

NORFOLK COUNTY

ENGINEERS DEPT.

NO. 233

233

FB 233
COUNTY OF NORFOLK
ENGINEERING DEPT.
649 HIGH STREET
DEDHAM, MA 02026

1-781-461-6128

1
233

2/ Page St. Avon Sections for

Proposed Sidewalk Aug 22, 1957 3

233

See N.B. 25 for 1931 Layout

" " 117 " Restaking & Benches

Note: Sta. on & Layout from scaled dist beg. @ Stoughton Avon line and are used for this job only. See old plan. H. Emery White in Vault

Freeman St. to

Pratt St.

39+52 Rt 45 201 279.72 ✓ 277.71

B.M. L.O.C. Bot. conc step Ho. 292 N.B. 117 P. 158

38+85 ± = 0+0 & Present T.W. Freeman St. Rt.

0+0 = 5.8 273.9

0+50 = 55 274.2

1- = 4.9 274.8

1+ = 4.7 275.0

2- = 4.1 275.6

	50	31	25	21	17	@	E	±WN.
39-	10.1	9.3	7.7	6.6	4.1	18	5.9	5.9
	269.6	270.4	271.8	273.1	275.6	274.4	273.8	273.8

E	15	25	40	48
5.9	6.0	5.9	5.9	5.8
273.8	273.7	273.8	273.8	273.9

39+09 Rt 135 Rim C.B. 6.18
273.54

39+50± Sill Ho #292 Rt 1.09
278.63

	50	40	27	25	20	18	@	E
39+	10.5	10.5	10.5	10.2	9.0	4.7	17	9
	269.2	269.2	269.2	269.5	270.7	275.0	273.3	273.5

±WN.	E	on walk	25	40	@ Ho.
5.9	5.9	5.3	4.5	3.2	2.5
273.8	273.8	274.4	275.3	276.5	277.2

39+52 & Bit walk Rt. ask. back. 273.9 273.8

Beg walk	15	25	@ Bot conc step	top 1st	on Plat
5.7	5.3	4.5	4.4	4.4	4.6
274.0	274.4	275.2	277.2	277.73	279.01

112 278.83 ✓ 277.71

39+81 Rt. 59 & Bit Drive 273.8 273.4 274.2

End	40	50	65
5.9	5.4	4.6	2.9
274.9	275.4	275.9	

✓ 9/12/57 A.T.

4/233 Page St.

278.83

Avon

Sections

5

40	50	40	25	15	14	13	7	0
9.8	9.0	8.1	7.2	5.4	5.7	5.2	5.0	
269.0	269.8	270.7	271.6	273.4	273.1	273.6	273.8	

27W.	E	25	40	50
2	11	4.9	4.8	3.5
4.9	5.2	273.9	274.0	275.3

40+	50	40	25	13	12	11	5	0
10.1	9.4	8.2	7.1	3.2	5.7	5.2	4.9	
268.7	269.4	270.6	271.7	275.6	273.1	273.6	273.9	

27W.	E	25	40	50
4	14	4.9	4.6	4.2
4.8	5.0	274.0	274.2	274.6

40+56 E Dirt Drive Rt. 89.

0	4
4.9	4.8
273.9	274.0

E	25	40	50	@ Barn
14	4.8	4.5	3.7	7.1
5.1	4.8	4.5	3.7	2.2
273.7	274.0	274.3	275.1	276.6

499 277.13 469 274.14

T.P. S.B. Rt.

40+76+ Sill Ho 274 Rt. 153

41	50	40	25	21	18	17	3	0
10.5	9.7	8.4	8.4	4.9	5.7	5.3	5.1	
268.6	269.4	270.7	270.7	274.2	273.4	273.8	274.0	

27W.	E	25	40	50
7	12	5.3	5.4	5.4
4.9	5.2	273.9	273.8	273.7

41+07 E Gravel Drive Rt. ask back

0	5
5.1	4.9
274.0	274.2

E	25	40	50	End
17	5.3	5.3	5.3	6.5
5.2	5.3	5.3	5.3	5.3
273.9	273.8	273.8	273.8	273.8

41+75 Lt 375 431 274.82 ✓

check B.M. (274.82)

41+	50	40	25	15	0
8.9	8.2	5.6	5.4	5.4	
270.2	270.9	273.5	273.7	273.7	

27W.	E	25	40	50
10	21	5.3	5.3	5.1
5.0	5.4	274.1	273.7	274.0

41+78 E Conc Walk Lt 89.

Piazza Fl.	top
39	37
310	4.38
276.03	274.75

@ 1st conc.	on	@ conc walk
37	7	9
5.05	5.26	5.4
274.08	273.87	273.77

41+78 Sill Ho 265 Lt 323 275.90

9/12/57 A.T.

42-

£ Conc walk

44	40	25
5.23	57	55
273.84	273.4	273.6

10	0	E	£ W.	E	23	25	34	50
48	49	49	45	47	47	47	45	45
274.3	274.2	274.2	274.6	274.4	274.4	274.6	274.6	274.6

42+03 £ Bit Drive Lt ask ahead.

100	50	40	25	10	0
85	65	61	53	47	49
270.6	272.6	273.0	273.8	274.4	274.2

42+08 £ Bit Drive Rt ask ahead.

0	E	£ W.	E	13	24	25	40	50	100
48	48	45	48	45	48	48	44	43	49
274.3	274.3	274.6	274.3	274.3	274.7	274.8	274.2		

42+40 Sill Ho Rt

1.88

277.19

42+48 £ Conc Walk Rt Rad.

0	£ W.
57	9
	49
274.0	274.2

E	@ walk	on				@ 1st top	Plot
<u>19</u>	<u>21</u>	<u>21</u>	<u>25</u>	<u>40</u>	<u>50</u>	<u>52</u> <u>52</u>	<u>53</u>
5.3	4.7	4.62	4.51	3.91	3.37	3.25 2.38	1.64
273.8	274.4	274.45	274.56	275.16	275.70	↓ 276.69	↓
down	E	on wall				275.82	277.43

42+

50	40	25	10	5	E	0
65	61	48	50	48	51	52
272.6	273.0	274.3	274.1	274.3	274.0	273.9

£ W.	E	on walk	40	50
9	19	25	3.9	3.5
49	53	4.55		
274.2	273.8	274.52	275.2	275.6

43-

50	40	25	15	12	E	0
55	52	47	55	61	59	57
273.6	273.9	274.4	273.6	273.0	273.2	273.4
	6.11	279.06	6.12	272.95		

£ W.	E	14	25	40	50
3	13	37	60	60	67
57	61	57			
273.4	273.0	273.4	273.1	273.1	272.4

43+45 £ Conc walk Lt rad.

49	48	48	@ 1st
298	358	418	
276.08	275.48	274.88	

40	25	22	@ walk	£ W.	0
447	531	545	22	13	3
			61	69	66
274.59	273.75	273.61	273.0	272.2	272.5

43+40 ± Sill Ho 253 Lt

318

275.88

43+

on walk	40	25	15	E	£ W.	0
44	45	55	73	70	67	67
45						
274.6	274.6	273.6	271.8	272.1	272.4	272.4

E	10	@	40	25	40	50
7	66	53	15	17	68	71
69			27	62		79
272.2	272.5	273.6	276.4	272.9	272.3	272.0
						271.2

7/12/57 A.T.

43+81 $\pm$ Bit Drive Lt Rad.
$$\begin{array}{r} 100 \\ 95 \\ \hline 269.6 \end{array}$$

$$\begin{array}{r} 50 \\ 82 \\ \hline 270.9 \end{array}$$

$$\begin{array}{r} 40 \\ 81 \\ \hline 271.0 \end{array}$$

$$\begin{array}{r} 25 \\ 80 \\ \hline 271.1 \end{array}$$

$$\begin{array}{r} E \\ 15 \\ \hline 82 \\ \hline 270.9 \end{array}$$

$$\begin{array}{r} \Delta W \\ 5 \\ \hline 7.8 \\ \hline 271.3 \end{array}$$

$$\begin{array}{r} 0 \\ 7.9 \\ \hline 271.2 \end{array}$$

43+63 36 Lt Rim well Lt 5.24

273.82

548 273.58

check old T.P. on walk (273.59)

$$\begin{array}{r} 102 \\ 274.61 \\ \hline 273.59 \end{array}$$

T.P. above

44-

$$\begin{array}{r} 50 \\ 48 \\ \hline 269.8 \end{array}$$

$$\begin{array}{r} 40 \\ 46 \\ \hline 270.0 \end{array}$$

$$\begin{array}{r} 25 \\ 43 \\ \hline 270.3 \end{array}$$

$$\begin{array}{r} E \\ 15 \\ \hline 45 \\ \hline 270.1 \end{array}$$

$$\begin{array}{r} \Delta W \\ 6 \\ \hline 4.2 \\ \hline 270.4 \end{array}$$

$$\begin{array}{r} 0 \\ 4.2 \\ \hline 270.4 \end{array}$$

$$\begin{array}{r} E \\ 4 \\ \hline 44 \\ \hline 270.2 \end{array}$$

$$\begin{array}{r} @ \\ 13 \\ \hline 45 \\ \hline 270.1 \end{array}$$

$$\begin{array}{r} top \\ 14 \\ \hline 20 \\ \hline 272.6 \end{array}$$

$$\begin{array}{r} 16 \\ 4.8 \\ \hline 269.8 \end{array}$$

$$\begin{array}{r} 25 \\ 5.4 \\ \hline 269.2 \end{array}$$

$$\begin{array}{r} 40 \\ 5.0 \\ \hline 269.6 \end{array}$$

$$\begin{array}{r} 50 \\ 5.2 \\ \hline 269.4 \end{array}$$

44+37

 $\pm$ Dirt Drive Lt Rad.
$$\begin{array}{r} 100 \\ 88 \\ \hline 265.8 \end{array}$$

$$\begin{array}{r} 50 \\ 66 \\ \hline 268.0 \end{array}$$

$$\begin{array}{r} 40 \\ 64 \\ \hline 268.2 \end{array}$$

$$\begin{array}{r} 25 \\ 63 \\ \hline 268.3 \end{array}$$

$$\begin{array}{r} 18 \\ 62 \\ \hline 268.4 \end{array}$$

$$\begin{array}{r} E \\ 17 \\ \hline 57 \\ \hline 268.9 \end{array}$$

$$\begin{array}{r} 40 \\ 5.5 \\ \hline 269.1 \end{array}$$

$$\begin{array}{r} 50 \\ 5.6 \\ \hline 269.0 \end{array}$$

44+37

 $\pm$ Dirt Drive Rt Rad
$$\begin{array}{r} 0 \\ 5.6 \\ \hline 269.0 \end{array}$$

$$\begin{array}{r} E \\ 3 \\ \hline 58 \\ \hline 268.8 \end{array}$$

$$\begin{array}{r} 10 \\ 55 \\ \hline 269.1 \end{array}$$

$$\begin{array}{r} 25 \\ 4.5 \\ \hline 270.1 \end{array}$$

$$\begin{array}{r} 40 \\ 3.9 \\ \hline 270.7 \end{array}$$

$$\begin{array}{r} End \\ 55 \\ \hline 4.2 \\ \hline 270.4 \end{array}$$

44+

$$\begin{array}{r} 50 \\ 9.7 \\ \hline 264.9 \end{array}$$

$$\begin{array}{r} 40 \\ 9.3 \\ \hline 265.3 \end{array}$$

$$\begin{array}{r} 25 \\ 74 \\ \hline 267.2 \end{array}$$

$$\begin{array}{r} E \\ 17 \\ \hline 14 \\ \hline 268.2 \end{array}$$

$$\begin{array}{r} \Delta W \\ 7 \\ \hline 5.9 \\ \hline 268.7 \end{array}$$

$$\begin{array}{r} 0 \\ 6.0 \\ \hline 268.6 \end{array}$$

$$\begin{array}{r} E \\ 4 \\ \hline 63 \\ \hline 268.3 \end{array}$$

$$\begin{array}{r} 7 \\ 6.1 \\ \hline 268.5 \end{array}$$

$$\begin{array}{r} 12 \\ 4.7 \\ \hline 269.9 \end{array}$$

$$\begin{array}{r} 25 \\ 4.0 \\ \hline 270.6 \end{array}$$

$$\begin{array}{r} 33 \\ 3.3 \\ \hline 271.3 \end{array}$$
44+60 $\pm$

Sill Ho. 244 Rt.

$$\begin{array}{r} 296 \\ \hline 271.65 \end{array}$$

45-

$$\begin{array}{r} 50 \\ 13.3 \\ \hline 261.3 \end{array}$$

$$\begin{array}{r} 32 \\ 11.4 \\ \hline 263.2 \end{array}$$

$$\begin{array}{r} top \\ 28 \\ 10.7 \\ \hline 263.9 \end{array}$$

$$\begin{array}{r} @ \\ 23 \\ 7.1 \\ \hline 267.5 \end{array}$$

$$\begin{array}{r} E \\ 22 \\ 7.7 \\ \hline 266.9 \end{array}$$

$$\begin{array}{r} \Delta W \\ 8 \\ 7.7 \\ \hline 266.7 \end{array}$$

$$\begin{array}{r} 0 \\ 8.0 \\ \hline 266.9 \end{array}$$

$$\begin{array}{r} 0 \\ 8.0 \\ \hline 266.6 \end{array}$$

$$\begin{array}{r} E \\ 2 \\ 8.1 \\ \hline 266.5 \end{array}$$

$$\begin{array}{r} @ \\ 10 \\ 6.1 \\ \hline 268.5 \end{array}$$

$$\begin{array}{r} top \\ 11 \\ 4.7 \\ \hline 269.9 \end{array}$$

$$\begin{array}{r} 12 \\ 5.7 \\ \hline 268.9 \end{array}$$

$$\begin{array}{r} 25 \\ 6.5 \\ \hline 268.1 \end{array}$$

$$\begin{array}{r} 33 \\ 6.3 \\ \hline 268.3 \end{array}$$

$$\begin{array}{r} 40 \\ 4.8 \\ \hline 269.8 \end{array}$$

$$\begin{array}{r} 50 \\ 4.2 \\ \hline 270.4 \end{array}$$

T.P. stone

45+

$$\begin{array}{r} 50 \\ 9.8 \\ \hline 259.9 \end{array}$$

$$\begin{array}{r} 40 \\ 9.7 \\ \hline 260.0 \end{array}$$

$$\begin{array}{r} Bot \\ 33 \\ 9.7 \\ \hline 260.0 \end{array}$$

$$\begin{array}{r} Top \\ 31 \\ 5.6 \\ \hline 264.1 \end{array}$$

$$\begin{array}{r} 25 \\ 5.2 \\ \hline 264.5 \end{array}$$

$$\begin{array}{r} E \\ 19 \\ 4.7 \\ \hline 265.0 \end{array}$$

$$\begin{array}{r} \Delta W \\ 9 \\ 4.7 \\ \hline 265.0 \end{array}$$

$$\begin{array}{r} E \\ 0 \\ 5.2 \\ \hline 264.5 \end{array}$$

$$\begin{array}{r} 10 \\ 6.8 \\ \hline 262.9 \end{array}$$

$$\begin{array}{r} 25 \\ 6.3 \\ \hline 263.4 \end{array}$$

$$\begin{array}{r} 40 \\ 5.7 \\ \hline 264.0 \end{array}$$

$$\begin{array}{r} 50 \\ 5.3 \\ \hline 264.4 \end{array}$$

$$\begin{array}{r} 50 \\ 5.3 \\ \hline 264.4 \end{array}$$

269.73
K

46	50	40	25	E	±VW	E	7	15	25	40	50
	<u>7.3</u>	<u>6.8</u>	<u>6.4</u>	<u>19</u>	<u>10</u>	<u>0</u>	<u>4.7</u>	<u>5.1</u>	<u>4.4</u>	<u>3.4</u>	<u>3.3</u>
	262.4	262.9	263.3	263.5	263.5	263.2	266.0	264.6	265.3	266.3	266.4

46+22 Sill Ho. Rt. 93' + 0.68

270.41

46+21	40	25	E	±VW	40	25	25	E	±VW
	<u>4.9</u>	<u>4.8</u>	<u>4.8</u>	<u>4.8</u>	<u>4.0</u>	<u>2.5</u>	<u>2.5</u>	<u>2.0</u>	<u>9</u>
	530	576	641	641	666	717	73	73	72
	264.43	263.97	263.32	263.32	263.07	262.56	262.4	262.4	262.5
46+21	530								
	264.43								

46+21 Sill Ho. #225 Lt

46+	50	40	25	E	±VW	E	15	25	40	50
	<u>8.0</u>	<u>7.8</u>	<u>8.2</u>	<u>8.2</u>	<u>8.0</u>	<u>8.4</u>	<u>7.5</u>	<u>8.0</u>	<u>7.8</u>	<u>7.5</u>
	261.73	261.9	261.5	261.5	261.7	261.3	262.2	261.7	261.9	262.2
				9.39	260.34	✓	check	old T.P.	stone	(260.35)

4.82 265.17 ✓
K260.35
conc fl. gar

T.P. above.

46+59 1/2 Gravel Drive Lt. sq.

88
44.9
260.68

50	40	25	E	±VW	E
<u>4.6</u>	<u>4.6</u>	<u>4.5</u>	<u>4.1</u>	<u>9</u>	<u>0</u>
260.5	260.6	260.7	261.1	261.4	261.1

46+70 Along top Ret Wall Lt. sq.

75
50
260.2

50	40	25	E	±VW	E
<u>4.8</u>	<u>3.5</u>	<u>3.5</u>	<u>3.0</u>	<u>10</u>	<u>0</u>
260.4	260.4	260.7	260.6	260.9	260.7

46+70 " Bot. " " " "

75
10.9
254.3

50	40	25	E	±VW	E
<u>7.3</u>	<u>5.7</u>	<u>4.5</u>	<u>4.6</u>	<u>10</u>	<u>0</u>
257.9	259.5	260.7	260.6	260.9	260.7

47- 60	52	50	40	25	E	±VW	E	15	25	40	50
<u>12.3</u>	<u>12.1</u>	<u>9.8</u>	<u>7.8</u>	<u>5.8</u>	<u>19</u>	<u>9</u>	<u>0</u>	<u>1</u>	<u>15</u>	<u>25</u>	<u>40</u>
252.9	253.1	255.4	257.4	259.4	259.6	260.0	259.7	259.6	259.9	260.3	261.2
											261.6

47+08 1/2 Gravel Road to Water Tower Rt. ask back

50	40	25	E	±VW	E
<u>5.7</u>	<u>6.0</u>	<u>5.6</u>	<u>5.0</u>	<u>4.4</u>	<u>3.6</u>
259.5	259.2	259.6	260.2	260.8	261.6
					263.2

9/12/57 A.T.

12
1233

Page

St.

26517

 π

Avon

Sections

13

R

	E	47W	
47+	$\frac{50}{12.1}$	$\frac{40}{10.8}$	$\frac{25}{7.9}$
	253.1	254.4	257.3
	$\frac{18}{7.1}$	$\frac{8}{6.8}$	$\frac{0}{7.1}$
	258.1	258.4	258.1

E	6	12	15	25	40	50
$\frac{1}{7.2}$	$\frac{6}{6.7}$	$\frac{12}{4.6}$	$\frac{15}{5.4}$	$\frac{25}{4.5}$	$\frac{40}{3.6}$	$\frac{50}{2.9}$
258.0	258.5	260.6	259.8	260.7	261.6	262.3

5.80

266.15

✓

260.35

T.P. above.

47+91 Bot. Slope Lt. Rad.

 $\frac{50}{13.5}$

252.7

 $\frac{40}{13.5}$

252.7

 $\frac{25}{13.3}$

252.9

Bot

 $\frac{23}{12.2}$

254.0

@

 $\frac{23}{9.7}$

256.3

E

 $\frac{17}{9.4}$

256.8

47W

 $\frac{8}{9.0}$

257.2

 $\frac{0}{9.2}$

257.0

48-

 $\frac{50}{10.7}$

255.5

 $\frac{40}{10.5}$

255.7

Also Top slope E

 $\frac{25}{9.8}$

256.4

47W

 $\frac{17}{9.7}$

256.5

 $\frac{8}{9.3}$

256.9

 $\frac{0}{9.4}$

256.8

E

 $\frac{3}{9.6}$

256.6

 $\frac{15}{7.8}$

258.4

@ ledge

 $\frac{22}{7.1}$

259.1

on

 $\frac{25}{4.2}$

262.0

Top

 $\frac{38}{2.2}$

264.0

Bot

 $\frac{30}{4.9}$

261.3

 $\frac{40}{4.2}$

262.0

 $\frac{50}{1.9}$

264.3

48+34 Lt 34.5

8.79

257.36

check B.M. (257.36) Ho. #209

48+24 Rt. 36.5

Rim Cesspool

3.46

262.69

48+40± Sill Ho #209 Lt

7.73

258.42

top Plat.

 $\frac{34}{7.44}$

258.71

top 1st

 $\frac{34}{8.78}$

257.37

Bot 1st

 $\frac{34}{9.42}$

256.73

 $\frac{25}{9.86}$

256.29

on

 $\frac{19}{10.22}$

255.93

@

 $\frac{19}{10.8}$

255.4

E

 $\frac{17}{10.5}$

255.7

47W

 $\frac{7}{10.1}$

256.1

 $\frac{0}{10.3}$

255.9

48+36 4 Conc Walk Lt. Rad.

48+

@ Bay Window.

 $\frac{35}{7.3}$

256.9

 $\frac{25}{9.9}$

256.3

E

 $\frac{15}{10.8}$

255.4

47W

 $\frac{5}{10.4}$

255.8

 $\frac{0}{10.4}$

255.8

E

 $\frac{5}{10.6}$

255.6

 $\frac{11}{10.4}$

255.8

 $\frac{15}{9.0}$

257.2

 $\frac{25}{8.3}$

257.9

 $\frac{36}{7.6}$

258.6

 $\frac{39}{6.3}$

259.9

@

 $\frac{43}{4.0}$

260.2

top

 $\frac{44}{2.1}$

264.1

48+75± Sill Ho #208 Rt. 6.00

260.15

7.50

264.86

✓

257.36

B.M. above

48+92 4 Bit. Drive Rt. Rad.

 $\frac{0}{10.0}$

254.9

E

 $\frac{8}{10.2}$

254.7

 $\frac{15}{9.9}$

255.0

 $\frac{25}{9.2}$

255.7

 $\frac{40}{7.7}$

257.2

 $\frac{50}{6.6}$

258.3

 $\frac{75}{3.7}$

261.2

 $\frac{100}{1.4}$

263.5

Conc fl. gar

 $\frac{106}{10.7}$

263.87

9/12/57 A.T

49-	50	40	25	14	3	0	8	12	20	25	40	50
	10.0	9.9	10.0	10.6	10.2	10.2	10.4	10.3	8.7	8.7	7.1	6.1
	254.9	255.0	254.9	254.3	254.7	254.7	254.5	254.6	256.2	256.2	257.8	258.8
			5.78	263.14	257.36		B.M. above					

49+27	Beg conc. ret. wall rt.	0	8	23	top	@ 2nd	39	39	50
		9.4	9.8	1	6.6	6.5	4.0	3.5	2.3
		253.7	253.3		256.5	256.6	259.1	259.6	260.8

49+50± Sill Ho. #192 Rt 0.70
262.44

49+	50	40	25	13	2	0	8	15	@ top	23	33	25	@	42	top	42	50
	12.0	11.4	10.8	11.0	10.4	10.4	10.8	9.8		7.2	7.0	6.9	4.4	2.9		2.3	2.3
	251.1	251.7	252.3	252.1	252.7	252.7	252.3	253.3		253.9	256.1	256.2	258.7	260.2		260.8	6.92
			2.76	256.89	✓	9.01	254.13	✓	T.P. Hyd Lt.							256.22	#191

50-	@ Ho.	40	E/F/39	E	Δ TN.	E	@	F	top	top	Well back	in drive		
	43	40	28	14	3	7	15	24	24	25	33	33	50	
	7.1	7.1	6.79	7.0	6.5	6.8	6.2	5.2	3.0	3.0	2.3	4.7	3.5	
	249.8	249.8	250.10	250.1	249.9	250.4	250.1	250.7	251.7	253.9	253.9	254.6	252.2	253.4

50+05	Top conc wall Rt ask back	0	8	24	24	25	40	50	73
		6.8	7.1	5.4	3.0	3.0	1.8	1.0	+ 0.2
		250.1	249.8	251.5	253.9	253.9	255.1	255.9	257.1

50+05	Bot " " " " "	0	8	24	24	25	40	50	73
		6.8	7.1	5.5	5.5	5.4	4.2	3.5	1.6
		250.1	249.8	251.4	251.4	251.5	252.7	253.4	255.3

50+11	4 Bit Drive Rt ask back	0	8	15	25	40	50	73	conc fl. gar.
		7.1	7.5	6.8	5.7	4.3	3.5	1.7	8.4
		249.8	249.4	250.1	251.2	252.6	253.4	255.2	255.86

50+16	top. conc. ret. wall Lt sq.	44	14	14	14	3	0
		7.2	7.0	7.3	7.8	7.8	7.3
		249.7	249.9	249.6	249.1	249.1	249.6

50+16 Bot. conc. ret. wall Lt. sq.

$$\begin{array}{r} 44 \\ 9.4 \\ \hline 247.5 \end{array}$$

$$\begin{array}{r} 40 \\ 9.0 \\ \hline 247.9 \end{array}$$

$$\begin{array}{r} 25 \\ 8.25 \\ \hline 248.64 \end{array}$$

$$\begin{array}{r} @ \\ 14 \\ 7.8 \\ \hline 249.1 \end{array}$$

$$\begin{array}{r} E \\ 14 \\ 7.8 \\ \hline 249.1 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 3 \\ 7.3 \\ \hline 249.6 \end{array}$$

$$\begin{array}{r} 0 \\ 7.3 \\ \hline 249.6 \end{array}$$
50+17 $\frac{1}{2}$ conc walk Lt. sq.
$$\begin{array}{r} 50 \\ 9.91 \\ \hline 246.98 \end{array}$$

$$\begin{array}{r} 40 \\ 9.27 \\ \hline 247.62 \end{array}$$

$$\begin{array}{r} 25 \\ 8.32 \\ \hline 248.57 \end{array}$$

$$\begin{array}{r} on \\ 23 \\ 8.20 \\ \hline 248.69 \end{array}$$

$$\begin{array}{r} @ \\ 23 \\ 8.2 \\ \hline 248.7 \end{array}$$

$$\begin{array}{r} E \\ 14 \\ 7.8 \\ \hline 249.1 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 3 \\ 7.4 \\ \hline 249.5 \end{array}$$

$$\begin{array}{r} 0 \\ 7.4 \\ \hline 249.5 \end{array}$$

50+33

Top slope rt. ask. back

$$\begin{array}{r} 0 \\ 8.3 \\ \hline 248.6 \end{array}$$

$$\begin{array}{r} E \\ 6 \\ 8.5 \\ \hline 248.4 \end{array}$$

$$\begin{array}{r} 15 \\ 8.0 \\ \hline 248.9 \end{array}$$

$$\begin{array}{r} 25 \\ 6.5 \\ \hline 250.4 \end{array}$$

$$\begin{array}{r} 40 \\ 4.8 \\ \hline 252.1 \end{array}$$

$$\begin{array}{r} 50 \\ 4.3 \\ \hline 252.6 \end{array}$$

50+36

Bot " " " "

$$\begin{array}{r} 0 \\ 8.5 \\ \hline 248.4 \end{array}$$

$$\begin{array}{r} E \\ 6 \\ 8.7 \\ \hline 248.2 \end{array}$$

$$\begin{array}{r} 15 \\ 8.9 \\ \hline 248.0 \end{array}$$

$$\begin{array}{r} 25 \\ 8.0 \\ \hline 248.9 \end{array}$$

$$\begin{array}{r} 40 \\ 8.1 \\ \hline 248.8 \end{array}$$

$$\begin{array}{r} 50 \\ 8.3 \\ \hline 248.6 \end{array}$$

0.93 255.06

254.13

TOP Hyd above

50+

$$\begin{array}{r} 100 \\ 13.5 \\ \hline 241.6 \end{array}$$

$$\begin{array}{r} 50 \\ 9.8 \\ \hline 245.3 \end{array}$$

$$\begin{array}{r} 40 \\ 9.0 \\ \hline 246.1 \end{array}$$

$$\begin{array}{r} 25 \\ 8.0 \\ \hline 247.1 \end{array}$$

$$\begin{array}{r} 22 \\ 8.0 \\ \hline 247.1 \end{array}$$

$$\begin{array}{r} 20 \\ 8.2 \\ \hline 246.9 \end{array}$$

$$\begin{array}{r} E \\ 15 \\ 7.8 \\ \hline 247.3 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 5 \\ 7.2 \\ \hline 247.9 \end{array}$$

$$\begin{array}{r} 0 \\ 7.4 \\ \hline 247.7 \end{array}$$

$$\begin{array}{r} E \\ 6 \\ 7.7 \\ \hline 247.4 \end{array}$$

$$\begin{array}{r} 14 \\ 7.7 \\ \hline 247.4 \end{array}$$

$$\begin{array}{r} 18 \\ 6.9 \\ \hline 248.2 \end{array}$$

$$\begin{array}{r} 25 \\ 7.0 \\ \hline 248.1 \end{array}$$

$$\begin{array}{r} 40 \\ 7.2 \\ \hline 247.9 \end{array}$$

$$\begin{array}{r} 50 \\ 7.7 \\ \hline 247.4 \end{array}$$

50+75+

Sill Ho Lt.

189

7.28

247.78

50+81

 $\frac{1}{2}$ Conc walk Lt. sq.
$$\begin{array}{r} \text{Top Plot} \\ 33 \\ 6.98 \\ \hline 248.08 \end{array}$$

$$\begin{array}{r} \text{Top} \\ 31 \\ 8.30 \\ \hline 246.76 \end{array}$$

$$\begin{array}{r} @ \text{ 1st} \\ 31 \\ 9.05 \\ \hline 246.01 \end{array}$$

$$\begin{array}{r} 25 \\ 9.22 \\ \hline 245.84 \end{array}$$

$$\begin{array}{r} on \\ 23 \\ 9.28 \\ \hline 245.78 \end{array}$$

$$\begin{array}{r} @ \\ 23 \\ 9.3 \\ \hline 245.8 \end{array}$$

$$\begin{array}{r} 17 \\ 9.9 \\ \hline 245.2 \end{array}$$

$$\begin{array}{r} E \\ 16 \\ 9.6 \\ \hline 245.5 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 5 \\ 9.1 \\ \hline 246.0 \end{array}$$

$$\begin{array}{r} 0 \\ 9.2 \\ \hline 245.9 \end{array}$$

6.42

251.26

10.22

244.84

TOP stone Lt.

50+99

 $\frac{1}{2}$ 1' Conc walk Lt. sq.
$$\begin{array}{r} 50 \\ 7.47 \\ \hline 243.77 \end{array}$$

$$\begin{array}{r} 40 \\ 7.07 \\ \hline 244.17 \end{array}$$

$$\begin{array}{r} 35 \\ 6.64 \\ \hline 244.62 \end{array}$$

$$\begin{array}{r} on \\ 24 \\ 6.7 \\ \hline 244.64 \end{array}$$

$$\begin{array}{r} @ \\ 18 \\ 7.1 \\ \hline 244.6 \end{array}$$

$$\begin{array}{r} E \\ 17 \\ 6.9 \\ \hline 244.2 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 5 \\ 6.4 \\ \hline 244.9 \end{array}$$

$$\begin{array}{r} 0 \\ 6.5 \\ \hline 244.8 \end{array}$$

51-

$$\begin{array}{r} 50 \\ 7.3 \\ \hline 244.0 \end{array}$$

$$\begin{array}{r} 40 \\ 6.8 \\ \hline 244.5 \end{array}$$

$$\begin{array}{r} 25 \\ 6.7 \\ \hline 244.6 \end{array}$$

$$\begin{array}{r} 18 \\ 7.1 \\ \hline 244.2 \end{array}$$

$$\begin{array}{r} E \\ 17 \\ 6.9 \\ \hline 244.4 \end{array}$$

$$\begin{array}{r} \text{EWN} \\ 5 \\ 6.4 \\ \hline 244.9 \end{array}$$

$$\begin{array}{r} 0 \\ 6.5 \\ \hline 244.8 \end{array}$$

$$\begin{array}{r} E \\ 5 \\ 6.7 \\ \hline 244.6 \end{array}$$

$$\begin{array}{r} 12 \\ 6.1 \\ \hline 244.2 \end{array}$$

$$\begin{array}{r} 18 \\ 4.8 \\ \hline 246.5 \end{array}$$

$$\begin{array}{r} 25 \\ 4.0 \\ \hline 247.3 \end{array}$$

$$\begin{array}{r} 30 \\ 3.6 \\ \hline 247.7 \end{array}$$

$$\begin{array}{r} 37 \\ 1.8 \\ \hline 249.5 \end{array}$$

$$\begin{array}{r} 40 \\ 1.5 \\ \hline 249.8 \end{array}$$

@ Ho.

v 9/12/57 A.T.

233
51+15 ± Sill Ho *188 Rt.

0.95
250.31

51+09 ± Conc walk Rt.

$\frac{0}{7.0}$ $\frac{E}{5}$
244.3 244.0

51+35 ± Bit Drive Rt ask back

$\frac{0}{8.4}$ $\frac{E}{5}$
242.9 242.7

51+
 $\frac{50}{12.6}$ $\frac{40}{11.9}$ $\frac{25}{10.2}$ $\frac{E}{15}$ $\frac{4WN.}{5}$ $\frac{0}{9.1}$
238.7 239.4 241.1 242.0 242.4 242.2
2.98 244.39 ✓ 9.85 241.41

$\frac{8}{7.3}$ $\frac{13}{6.2}$ $\frac{on}{13}$ $\frac{25}{5.14}$ $\frac{1st}{36}$ $\frac{topst}{36}$ $\frac{top top}{41}$
244.0 245.1 245.10 246.12 247.00 247.66 250.37

$\frac{7}{8.7}$ $\frac{15}{7.8}$ $\frac{25}{7.0}$ $\frac{40}{6.1}$ $\frac{50}{5.6}$ $\frac{75}{4.6}$ $\frac{conc fl. gar}{9.3}$
242.6 243.5 244.3 245.2 245.7 246.7 247.30

$\frac{6}{9.5}$ $\frac{13}{9.0}$ $\frac{15}{8.2}$ $\frac{25}{8.3}$ $\frac{40}{8.1}$ $\frac{50}{7.4}$
241.8 242.3 243.1 243.0 243.2 243.9
T.P. Stone Lt.

51+97 ± Gravel Drive Lt. ask back

$\frac{75}{7.1}$
237.3

$\frac{50}{6.7}$ $\frac{40}{6.2}$ $\frac{25}{4.8}$ $\frac{16}{4.3}$ $\frac{15}{4.3}$ $\frac{E}{13}$ $\frac{4WN.}{3}$ $\frac{0}{4.2}$
237.7 238.2 239.6 240.1 240.1 240.2 240.3 240.2
240.4

52-
 $\frac{50}{7.1}$ $\frac{40}{6.5}$ $\frac{25}{5.1}$ $\frac{E}{13}$ $\frac{4WN.}{3}$
237.3 237.9 239.3 240.0 240.2

$\frac{0}{4.3}$ $\frac{7}{4.6}$ $\frac{15}{4.1}$ $\frac{25}{4.4}$ $\frac{40}{4.0}$ $\frac{50}{3.8}$
240.1 239.8 240.3 240.0 240.4 240.6

52+30 ± Dirt Drive Rt. ask back.

$\frac{0}{5.2}$ $\frac{E}{9}$
239.2 239.9

$\frac{15}{5.5}$ $\frac{25}{5.0}$ $\frac{40}{4.7}$ $\frac{50}{4.6}$ $\frac{75}{4.9}$
238.9 239.4 239.7 239.8 239.5

52+46 ± Conc. walk Rt. ask back

$\frac{0}{5.6}$ $\frac{E}{10}$
238.8 238.5

$\frac{17}{5.9}$ $\frac{on}{17}$ $\frac{25}{5.12}$ $\frac{1st}{42}$ $\frac{conc stop}{3.53}$ $\frac{top}{44}$
238.5 238.59 239.27 240.76 241.73

52+50 ± Sill Ho *180 Rt.

2.75
241.64

✓ 9/12/57 A.T.

20
233
52+

Page St.

24439

Avon

@ Ho.
38
5.3

239.0

25
5.5

238.9

10
5.8

238.6

52+60± Sill Ho #161 Lt.

350

240.89

52+69 ± Loose Flag walk Lt. @ Ho. 161

top Plat.

35
2.77

241.62

237.34

4.84 242.18 ✓ 7.05
K

End

62
5.2

237.0

53-

50
4.9

237.3

40
4.9

237.3

25
4.7

237.5

15
4.6

237.6

E

8
4.7

237.5

0
4.5

237.7

53+

50
5.8

236.4

40
5.3

236.9

25
5.3

236.9

15
5.2

237.0

5
5.2

237.0

0
5.1

237.1

±WN

5
5.0

237.2

53+25± Sill New Ho Lt.

234

239.84

53+85 ± Gravel Rd Rt. ask back.

0
5.4

236.8

54-

50
5.7

236.5

40
5.5

236.7

25
5.6

236.6

15
5.6

236.6

5
5.7

236.5

0
5.5

236.7

4.35

241.69 ✓
K

237.34

Sections

21

±WN.
0

5.7

238.7

E
11

6.1

238.3

25

5.2

239.2

@ Ho.
45

3.4

241.0

top

32
4.76

239.63

T.O. stone Rt

@ 1st

32
5.6

238.8

@

15
6.2

238.2

E

10
6.4

238.0

0
6.1

238.3

40
4.8

237.4

25
4.5

237.7

15
4.6

237.6

E
9

4.5

237.7

0
4.3

237.9

±WN.

1
4.5

237.7

E

11
4.6

237.6

20
3.8

238.4

25
3.6

238.6

40
3.8

238.4

50
3.7

237.5

E
14

237.1

25
5.4

236.8

40
4.9

237.3

50
5.4

236.8

±WN.

5
5.3

236.9

E

16
5.3

236.9

25
5.2

237.0

40
5.5

236.7

50
5.7

236.5

25
6.0

236.2

100
5.9

236.3

±WN.

5
5.4

236.8

E

14
5.4

236.8

25
5.2

237.0

26
5.9

236.3

26
7.3

234.9

40
6.3

235.9

50
6.3

235.9

T.O. above.

✓ 9/13/57 A.T.

22
1233

Page St.

241.69
K

Avon

Sections

23
R

53+93 Flow 18" Conc Pipe Lt 108' 12.67
229.02

54+42 Bot. slope Lt. askew back 75
115

230.2

54+35 Flow 18" Conc Pipe Rt. 25 974
231.95

54+	50	40	25	Bot. 18	@ 18	E 6	0
	10.2	9.8	9.6	9.4	7.8	5.5	5.2
	231.5	231.9	232.1	232.3	233.7	236.2	236.5

54+81 Bot. slope Lt. Rad. 50 40
9.0 9.0

232.7 232.7

55+82 Rt. 42' 235 239.34

242.77
K

342 239.35

55-	50	40	25	15	E 8	0
	7.3	7.6	6.8	6.3	6.3	5.9
	235.5	235.2	236.0	236.5	236.5	236.9

55+25[±] Sill Ho* 149 Lt. 2.70 240.07

55+	50	40	25	E 13	4TW 3	0
	5.6	5.9	5.8	5.8	5.5	5.4
	237.2	236.9	237.0	237.0	237.3	237.4

55+59 4 Gravel Drive Lt askew back 75
4.5
238.3

55+59 4 Dirt Drive Rt. Rad. 0 5
5.4 5.6
237.4 237.2

50	40	25	17	10	E 6	0
10.8	10.9	10.5	8.5	5.1	5.6	5.2
230.9	230.8	231.2	233.2	236.6	236.1	236.5

4TW 4	E 14	@ 24	Bot 24	25	40	50
5.1	5.2	5.8	7.9	7.9	9.2	9.2
236.6	236.5	235.9	233.8	233.8	232.5	232.5

32	25	22	15	E 6	0
8.8	6.5	6.0	5.5	5.4	5.1
232.9	235.2	235.7	236.2	236.3	236.6
check	B.M.	Ho 150	(239.35)		

B.M. above

4TW 2	E 12	23	23	25	40	50
5.9	6.1	5.7	7.9	7.9	9.7	9.7
236.9	236.7	237.1	234.9	234.9	233.1	233.1

E 7	15	25	40	50
5.7	5.6	6.0	5.9	5.8
237.1	237.2	236.8	236.9	237.0

50	40	25	E 15	4TW 5	0
5.7	6.0	5.8	5.7	5.4	5.4
237.1	236.8	237.0	237.1	237.4	237.4

15	25	40	50	End 75
5.6	5.9	5.6	5.4	5.1
237.2	236.9	237.2	237.4	237.7

v 9/2/57 AT.

24
233

Page

St.

242.77

Avon

Sections

25

155+90

Sill H^o #150 Rt.

1.98 240.79

	E	4TW.	E
56-	<u>50</u> 4.8	<u>40</u> 5.3	<u>25</u> 5.3
	<u>22</u> 5.2	<u>10</u> 4.8	<u>0</u> 5.0
	238.0	237.5	237.5
	237.6	238.0	238.8
	+ 8.12	248.52	- 2.37
			240.40

A

56+28[±] = 0+0 4 Present TW. High St.

0+0	=	10.5	238.0
0+50	=	9.1	239.4
1-	=	8.8	239.7
1+	=	8.9	239.6
2-	=	9.0	239.5

E TW. High St.

	E	4TW.	E
56+	<u>50</u> 9.5	<u>41</u> 9.9	<u>25</u> 9.4
	<u>22</u> 9.4	<u>7</u> 9.8	
	239.0	238.6	239.1
	239.1	238.7	

57- E TW. High

	E	4TW.	E
57-	<u>69</u> 8.8	<u>50</u> 8.6	<u>40</u> 8.6
	<u>25</u> 8.5	<u>18</u> 8.5	<u>11</u> 9.0
	<u>4</u> 8.4		
	239.7	239.9	239.9
	240.0	240.0	239.5
	240.1	240.1	

	E	4TW.	E
57+	<u>50</u> 8.4	<u>40</u> 7.8	<u>32</u> 7.8
	<u>25</u> 7.6	<u>19</u> 7.6	<u>10</u> 8.0
	<u>0</u> 7.5		
	240.1	240.7	240.7
	240.9	240.9	240.5
	241.0		

57+62 4 Conc walk Rt ask ahead.

0
7.357+62[±] Sill H^o #140 Rt.241.2
1.09 247.43

	E	4TW.	E
58-	<u>50</u> 7.0	<u>40</u> 7.1	<u>25</u> 6.7
	<u>15</u> 6.5	<u>5</u> 6.7	<u>0</u> 6.1
	241.5	241.4	241.8
	242.0	241.8	242.4

530

249.68

414

244.38

	15	25	40	50
	<u>4.6</u> 238.2	<u>4.6</u> 238.2	<u>4.2</u> 238.6	<u>4.3</u> 238.5
	7.0	pt on conc.	curd	

	0	15	25	40	50
	<u>9.8</u> 238.7	<u>11.4</u> 237.1	<u>10.9</u> 237.6	<u>10.8</u> 237.7	<u>10.8</u> 237.7

	0	15	25	40	50
	<u>9.0</u> 239.5	<u>9.0</u> 239.5	<u>9.3</u> 239.2	<u>9.6</u> 238.9	<u>9.8</u> 238.7

	15	25	40	50
	<u>5.5</u> 243.0	<u>4.6</u> 243.9	<u>3.7</u> 244.8	<u>2.9</u> 245.6

@ House

	10	15	on 15	25	40	@ 1st	top 1st	Brick top Plat
	<u>5.5</u> 243.0	<u>5.0</u> 243.5	<u>4.90</u> 243.62	<u>4.17</u> 244.25	<u>3.32</u> 245.20	<u>4.2</u> 245.26	<u>4.2</u> 245.89	<u>4.3</u> 247.96

	7	15	25	40	50
	<u>4.9</u> 243.6	<u>5.6</u> 242.9	<u>5.0</u> 243.5	<u>3.9</u> 244.6	<u>3.6</u> 244.9

V.R. Boulder

✓ 9/13/57 A.T.

58+25± Sill Ho Lt. cor High St. 575 243.73

58+33 = 0+0 & Present W. Granite Ave.

0+0	6.7	243.0
0+50	5.6	244.1
1-	4.3	245.7
1+	2.2	247.5
1+70	0.0	249.7

58+	50	40	35	E	2TW	E	0
	7.0	7.0	6.6	6.7	6.4	6.5	6.6
	242.7	242.7	243.1	243.0	243.3	243.2	243.1

58+ & Gravel Drive Lt. Rad.

End
72
71

242.6

58+94	& Conc Walk Lt. Rad.	top plot	top 1st	0 1st
		57	55	55
		303	442	512
		246.65	245.26	244.56

3	4	15	25	40	50
6.4	5.9	5.7	6.1	5.9	5.6
243.3	243.8	244.0	243.6	243.8	244.1

50	40	25	E	2TW	E	0
71	6.9	6.5	6.7	6.3	6.5	6.5
242.6	242.8	243.2	243.0	243.4	243.2	243.2

50	40	25	on	2	E	2TW	E
55.27	55.5	58.9	5.9	5.9	5.9	5.5	5.6
244.41	244.13	243.79	243.8	243.8	244.2	244.1	

59+0± Sill Ho 119 Lt.

348 246.20

59-	50	40	35	E	2TW
	5.3	5.5	5.8	6.0	5.5
	244.4	244.2	243.9	243.7	244.2

0	5	15	25	40	50
5.5	5.5	5.0	5.3	5.0	4.8
244.2	244.2	244.7	244.4	244.7	244.9

59+25 & Gravel Drive Lt ask ahead. 100 75

244.1 244.2

50	40	25	E	2TW	0
5.5	5.5	5.4	5.6	5.2	5.2
244.2	244.2	244.3	244.1	244.5	244.5

59+	50	40	25	E	2TW
	5.8	5.7	5.3	5.4	4.9
	243.9	244.0	244.4	244.3	244.8

0	2	15	25	40	50
5.0	5.0	4.3	4.2	3.7	3.2
244.7	244.7	245.4	245.5	246.0	246.5

330 246.38

check T.P. conc block (246.37)

v 9/13/57 O.T

28 Page 754 253.91 246.37
 233 St. Avon
 59+ Sill Ho *118 Rt. 287 251.07

59+77 ± Conc walk Rt. sq. @
 0 7 14
 9.0 8.9 8.7
 244.9 245.0 245.2

59+90 ± Gravel Drive Rt. sq. E
 0 2
 8.8 8.8
 245.1 245.1

60- @ 1st E ±TW
 48 40 25 17 9
 749 764 88 8.9 8.5
 246.42 246.27 245.1 245.0 245.4

60+01 ± Conc Walk Lt. sq. P1222 top 1st @ 1st
 52 48 48
 471 890 749
 249.20 249.01 246.42

853 254.90 246.37
 7

60+0 ± Sill Ho *115 Lt. 599 248.91

60+12 ± Gravel Drive Rt. sq. E
 0 2
 9.4 9.4
 245.5 245.5

60+23 ± Bit Drive Lt. sq. 75
 88
 246.1

60+ 50 40 25 E ±TW
 83 8.8 9.6 17 8 0
 9.4 8.9 9.0
 246.6 246.1 245.3 245.5 246.0 245.9

T.P. Sections 29
 12

on 25 40 50 End
 14 14 69
 8.64 8.23 7.67 7.33 6.67
 245.27 245.68 246.24 246.58 247.24

15 25 40 50 75 100
 8.7 8.4 7.8 7.3 6.2 4.9
 245.2 245.5 246.1 246.6 247.7 249.0

0 2 10 25 40 50
 8.6 8.6 8.0 7.8 7.3 6.8
 245.3 245.3 245.9 246.1 246.6 247.1

40 25 25 E ±TW
 7.64 8.41 8.8 8.9 8.5 8.6
 246.27 245.50 245.11 245.0 245.4 245.3

T.P. above

15 25 40 50 75 100
 9.0 8.3 7.5 7.2 6.2 6.0
 245.9 246.6 247.4 247.7 248.7 248.9

50 40 25 E ±TW
 9.1 9.3 9.5 9.5 9.2 9.3
 245.8 245.6 245.4 245.4 245.7 245.6

E 12 14 25 40 50
 2 9.0 8.3 7.7 5.7 4.1 3.3
 245.9 246.6 247.2 247.2 250.8 251.6

9/13/57 A.T.

833

60+60± Sill Ho *109 Lt.

6.74 298.16

60+60± Sill Ho *110 Rt.

2.21 252.69

60+59 1/2 Conc walk Rt. Rad.

0	2
8.9	8.9
296.0	296.0

6.17 252.54

246.37

60+67 1/2 Grano walk Lt. Rad. top P1222 top 1st @ 1st.

55	53	53
4.18	5.61	6.24
298.36	296.93	296.30

60+88 1/2 Gravel Drive Lt. Rad.

50	40	25	E	1/2 TW	0
8.9	8.3	6.9	16	7	6.4
293.6	294.2	295.6	6.7	6.4	6.4

61+07 Bot slope Rt. Rad.

0	2	10
6.5	6.5	6.3
296.0	296.0	296.2

61+13 1/2 Bit Drive Lt. Rad.

100	75	50
11.7	10.0	8.6
290.8	292.5	293.9

61+40 1/2 Cemented Flags Lt. Rad. top P161 top 1st @ 1st.

55	53	53	50	40
6.22	7.49	8.11	8.09	8.12
296.32	295.05	299.93	299.95	299.92

@	on				@ stop	top
13	13	25	40	50	64	64
8.2	7.79	5.64	4.26	3.42	2.24	1.72
296.7	297.11	299.26	250.69	251.98	252.66	253.18

T. P. above

50	40	25	24	@	E	1/2 TW	0
6.28	6.52	6.81	6.85	6.9	6.9	6.4	6.4
296.26	296.02	295.73	295.69	295.6	295.6	296.1	296.1

75	50	40	25	E	1/2 TW	0
9.5	9.2	8.6	7.1	6.7	6.3	6.4
293.0	293.3	293.9	295.9	295.8	296.2	296.1

E	1/2 TW	0
2	11	25
6.5	6.2	5.4
296.0	296.3	297.1

25	40	50
5.0	4.1	3.7
297.5	298.4	298.8

40	25	21	E	1/2 TW	0
6.0	6.8	6.6	17	8	6.5
299.5	295.7	295.9	6.8	6.3	6.5

on	@	E	1/2 TW	0	✓
38	38	25	16	7	9/12/57
8.67	8.09	7.5	7.2	6.8	AT.
299.95	299.95	295.0	295.3	295.7	295.6

233

60+40± Sill Ho. #103 Lt. 674 295.80

	50	40	25	E	4TW	0
61+	8.1	8.1	7.5	7.3	7.0	7.0
	299.4	299.4	295.0	295.2	295.5	295.5

	E	6	15	25	40	@ Piz 220
	7.1	7.0	6.0	5.1	4.2	4.8
	295.4	295.5	296.5	297.4	298.3	298.3

61+58± Sill Ho #102 Rt. 183 250.71

	0	E
61+58	7.2	7.2
	295.3	295.3

	6	@	on	25	40	@ 1st	top 1st	Piazza Fl.
	7.2	6.0	5.98	5.13	4.20	4.03	3.40	1.54
	295.3	296.5	296.56	297.41	298.39	298.51	299.14	251.0

61+61 Top Slope Lt. Rad. 5.64 252.01 246.37

	50	40	25	E	4TW	0
	8.1	8.1	7.7	7.5	7.2	7.2
	299.4	299.4	299.8	295.0	295.3	295.3

T.O. above

61+70 Bot slope Lt. Rad. 5.0 10.2 291.8

	40	27	top	@	E	4TW	0
	7.5	8.2	5.4	7.1	7.2	6.8	6.9
	292.5	293.8	296.6	299.9	299.8	295.2	295.1

61+75 4 Bit Drive Rt. Rad. 0 7.3 299.7

	15	25	40	50	75	conc fl. gar.
	6.7	6.0	5.0	4.6	4.1	9.8
	295.3	296.0	297.0	297.4	297.9	4.06
						297.95

	50	40	30	25	20	E	4TW	0
62-	10.1	9.7	8.9	8.1	7.6	7.7	7.3	7.4
	291.9	292.3	293.1	293.9	294.4	294.3	294.7	294.6

	E	15	25	40	50
	7.4	6.8	6.0	5.1	4.7
	294.6	295.2	296.0	296.9	297.3

62+04 4 Bit Drive Lt. Rad. 100 7.5 5.0 290.7 291.4 292.0

	30	35	20	E	4TW	0
	8.9	8.2	7.7	7.8	7.4	7.4
	293.1	293.8	294.3	294.2	294.6	294.6

9/17/57 345.40

233

62+16 Bot slope Rt. Rad. $\frac{0}{7.6}$ $\frac{1}{7.6}$ $\frac{5}{7.5}$
299.4 299.4 299.5

62+23 $\pm$ Conc. walk Lt. Rad. $\frac{53}{5.41}$ $\frac{51}{6.53}$ $\frac{51}{7.22}$
296.60 295.48 294.79

62+ 6.53 295.48

62+23 $\pm$ Sill Ho* 97 Lt. 5.61 296.40
339 $\frac{248.87}{\pi}$ 295.48

62+40 Top slope Lt. sq.

62+44 " " " $\frac{50}{6.5}$
292.4

62+ $\frac{50}{6.9}$ $\frac{40}{6.9}$ $\frac{28}{6.4}$ $\frac{25}{5.5}$ $\frac{17}{5.2}$ $\frac{9}{4.7}$ $\frac{0}{4.8}$
292.0 292.0 292.5 293.4 293.7 294.2 294.1

62+74 Bot. slope Lt. sq. $\frac{50}{6.6}$
292.3

62+84 Top " " " $\frac{50}{4.5}$
294.4

R

$\frac{15}{8.2}$ $\frac{25}{8.5}$ $\frac{40}{8.4}$ $\frac{50}{8.4}$
293.8 293.5 293.6 293.6

on @ E $\frac{17}{8.1}$ $\frac{17}{8.1}$ $\frac{17}{8.1}$ $\frac{17}{8.1}$
40 $\frac{26}{8.20}$ $\frac{26}{8.1}$ $\frac{25}{8.1}$ $\frac{25}{8.1}$ $\frac{25}{8.1}$ $\frac{25}{8.1}$
299.30 293.81 293.9 293.9 293.9 293.9 294.3 294.3

check B.M. Ho* 97 (295.48)

B.M. above

$\frac{50}{4.4}$ $\frac{40}{4.8}$ $\frac{25}{5.3}$ $\frac{17}{5.1}$ $\frac{17}{5.1}$ $\frac{17}{5.1}$ $\frac{17}{5.1}$
294.5 294.1 293.6 293.8 294.3 294.2

$\frac{40}{6.4}$ $\frac{28}{6.3}$ $\frac{25}{5.4}$ $\frac{18}{5.1}$ $\frac{18}{5.1}$ $\frac{18}{5.1}$ $\frac{18}{5.1}$
292.5 292.6 293.5 293.8 294.3 294.2

$\frac{1}{4.8}$ $\frac{4}{4.4}$ $\frac{12}{5.2}$ $\frac{13}{4.0}$ $\frac{14}{5.6}$ $\frac{25}{6.4}$ $\frac{40}{6.3}$ $\frac{50}{6.3}$
294.1 294.5 293.7 294.9 293.3 292.5 292.6 292.6

$\frac{40}{6.3}$ $\frac{28}{6.1}$ $\frac{25}{5.5}$ $\frac{17}{5.3}$ $\frac{17}{5.3}$ $\frac{17}{5.3}$ $\frac{17}{5.3}$
292.6 292.8 293.4 293.6 294.1 294.0

$\frac{40}{5.0}$ $\frac{25}{5.5}$ $\frac{17}{5.2}$ $\frac{17}{5.2}$ $\frac{17}{5.2}$ $\frac{17}{5.2}$ $\frac{17}{5.2}$
293.9 293.4 293.7 294.0 294.0

36 Page St.

24887 Avon

63-	$\frac{50}{4.7}$	$\frac{40}{5.2}$	$\frac{25}{5.4}$	$\frac{17}{5.6}$	$\frac{8}{5.0}$	$\frac{0}{5.1}$
	294.2	293.7	293.5	293.3	293.9	293.8

63+05± Sill Ho # 92 Rt. 0.91 297.96

63+00± " " # 91 Lt. 2.63 296.24
cor Pratt St.

3.39 245.48

Sections

37
R

E	$\frac{15}{5.1}$	$\frac{25}{4.4}$	$\frac{40}{3.4}$
	293.8	293.8	294.5

@ Piazza

check BM (245.48)

✓ 9/13/57 A.T.

38

233

39

40

233

41

42

233

43

44

233

45

46 Causeway St
1233

Medfield

Survey 4

22 Jan, 1959

47

S+N "7
McIntyre

19.33

S+N P.O.T.
5+35.10

29.60
66.47
78.65
86.33
50.20
330.59
104
330.55

75.79
47.50
54.98
78.98
257.25
103
257.22

380.00
21.31
401.31
0.05
401.26

10+20.08

P.O.T.

S+N

12.22

S+N "9

McIntyre

2+77.88

P.O.T. S+N

22.11

S+N "6
McIntyre

McIntyre

277.91
103
277.88

Causeway

N 53° 15' E

277.85

277.88

122° 41-30
8° 04-30
122° 41-30

Orchard St

45.35

N.B. 229 P. 76 spl

34.15

0+00 Causeway St.

N.B. 229 P. 76 spl

26.42

149° 26-40

747.77

spl 20' ord

78° 45

28.88

D.H. Bedstone

154.15

St

Causeway

154.41

154.43

N 19° 30' E

82° 21-20

144.14-20
72° 43
144.14-20
10

D.H. Bedstone

97° 35'

28.38

1.96

D.H. Bedstone

D.H. ledge

8+65.65

22.97

D.H. In Bedstone on line

330.52
330.55

9° 01

61.99

S+N "8

McIntyre

48 Causeway St

Medfield

Survey B

Jan 1959 49

233

Spk 12' oak

SEE P 106 for
connection to
HAMMOND STA.

157° 40-20

113° 01

18+21.40 157° 40-20

D.H. Bedstone

McIntyre 34N 11

D.H. Bedstone
on line

Spk 18' P.

169.15
231.03
400.18
.12
400.06

N 34° 30' E

400.06
400.02

D.H. Bedstone

14+21.34

D.H. Bedstone

165-19-50
135-59-30
165-19-50
165-20-00

Spk 10' Nut

10 34N
McIntyre

86° 33' 30" E

Spk 8' oak

156° 15

108° 45 22+37.76

156° 15

Spk 18' oak

78.96
129.41
208.37
.06
208.31

208.31

20+29.45

Spk

18.38

89° 12'

34N 12
McIntyre

208.11
.06
208.05

208.05

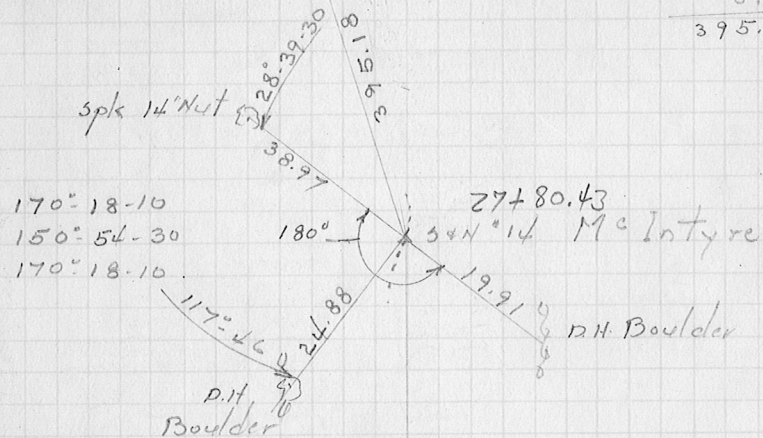
50 Causeway St,
1233

Medfield

Survey

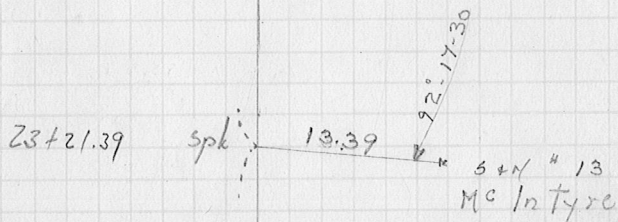
Jan. 1959

51



459.17
.13
459.04

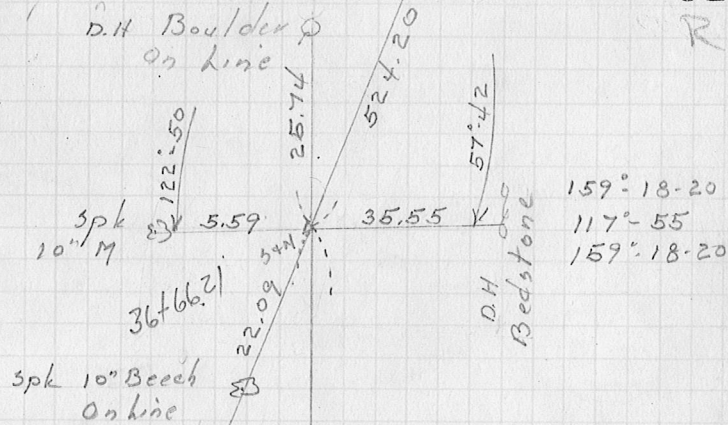
459.04



83.63

395.29
0.11
395.18

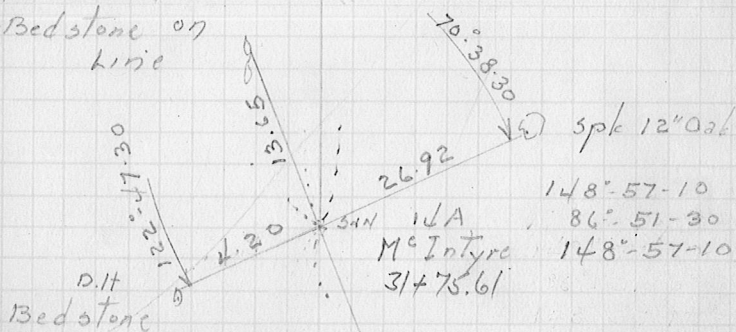
83.32
441.00
524.32
.12
524.20



59.98
72.78
71.90
71.61
71.90
71.22
71.34
490.73
.13
490.60

N 53° 30' E 490.60

D.H. Bedstone on line



395.18
0.11
395.07

52 Causeway St.

233

73.96

46+19.59

spt
1st oak
GONE

156-40

N 85° 10' 128

EDM 1991

355.09

355.24

N 21° E

Medfield

Noon Hill St

OK 1991

143° 54' 20

131° 43

143° 54' 20

spt 12" oak

T 48°

88.31

97.76

98.04

75.98

355.09

126° 25' 10

19° 15' 40

126° 25' 10

spt 8" P

91° 17

44.76

41+90.41

P.H. ledge

40.37

92° 13

spt 12" P

11.97

OK 1991

FND 1991

spt 8" oak on line

Survey B

387.42

.11

387.31

Jan. 1959

53

R

OK 1983

387.31

140° 1991

140° 1991

OK 1991

20.52

spt 18" M

OK 1991

175° 55' 40

167° 45' 40

175° 55' 30

OK 1991

107° 32

OK

P.H. Boulder

368.58

.07

368.51

368.51

N 37° E

$$\begin{array}{r} 61.39 \\ 224.65 \\ \hline 286.04 \end{array}$$
$$\begin{array}{r} 12.63 \\ 398.31 \\ 3.97 \\ \hline 414.91 \\ 09 \\ \hline 414.82 \end{array}$$

214.82
OK 1982

 $65 + 48.37$

D.H.
OFF Line

ok
41.63

D.H. FND
0.118 Boulder ~~Da Line~~

new vert SPK 20" Beech
SPK 16" Beech

spk R.P. 69+63.19
100.00
36.81

$$\tau = 90^\circ$$

100.00
100.00
~~100.00~~
100.00
6.81

406.81 T
.06
.04 Tape

406.91

166-14-40
138-44-00
166-14-40

$$\begin{array}{r} 69 + 63.19 \\ 2 + 24.71 \\ \hline 71 + 87.90 \end{array}$$

71 + 87.90

71 + 87.90

D.H. Wing But.

BRIDGE

S & N.

$$76 + 84.72$$

503 spk 18" m
18.58
Spk in Bridge 75

75 + 94.81

69463.19

224.71

7 1:87.90

4 + 6.97

75494.81

89.91

$$76 + 84.72$$

59-02-00
20.90

~~Spk
Th 6" E.~~

153-14-30

S + N. 71 + 87.90 ✓

1800
19.41-10

171-45-00
155-15-00
171-45-00

△.

224.71

~~Ch. 11.~~
Top conc.
Post

417.60 sec. 99

58 Additional Survey Traverse Causeway
x233 St. @ Dwight St.

1233 St. @ Dwight St.

Temp 90° @ 1 P.M.

70° @ 2 P.M.

D. H. Granite Bridge Abut.

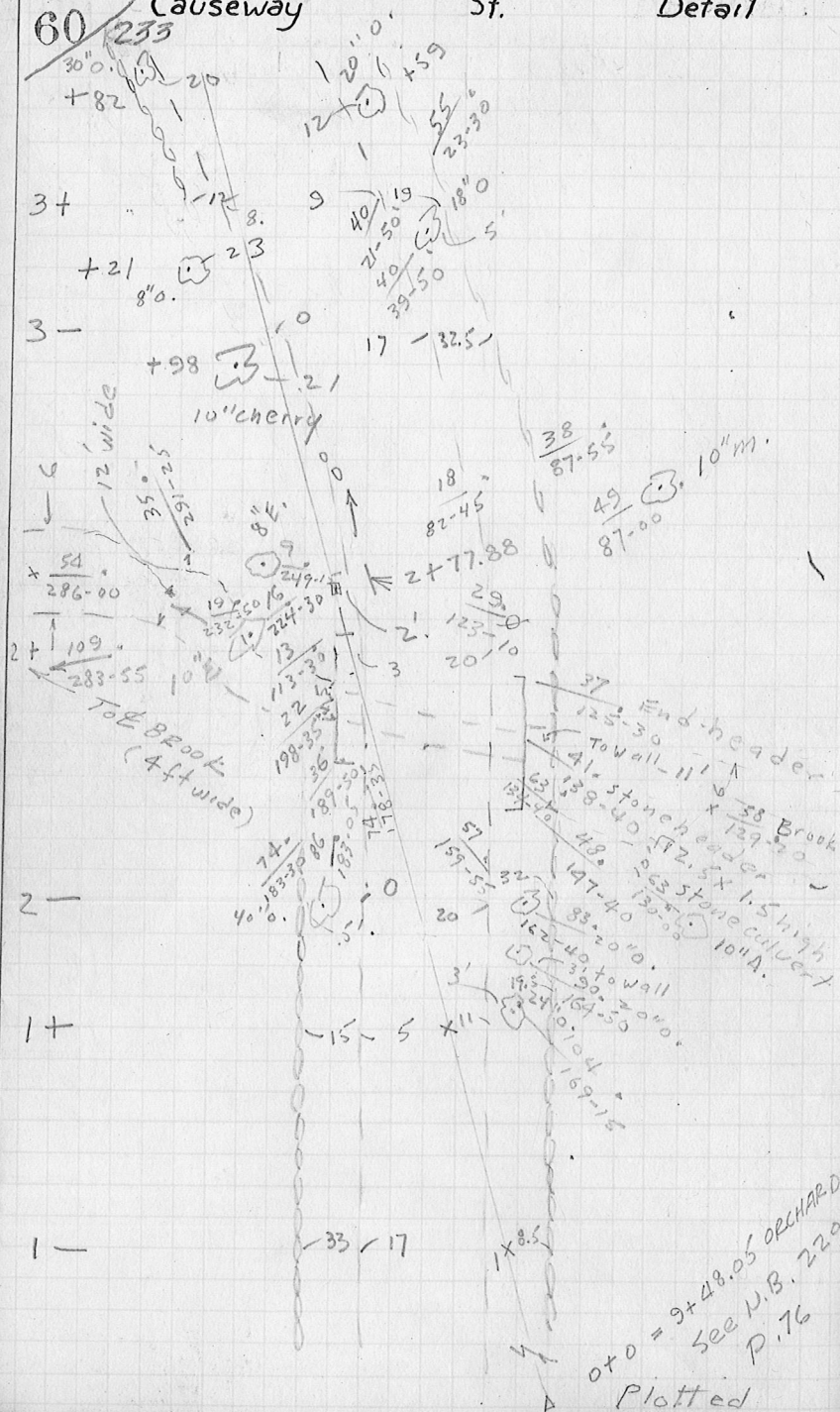
See Page 96 for Survey

60/233

Causeway

St.

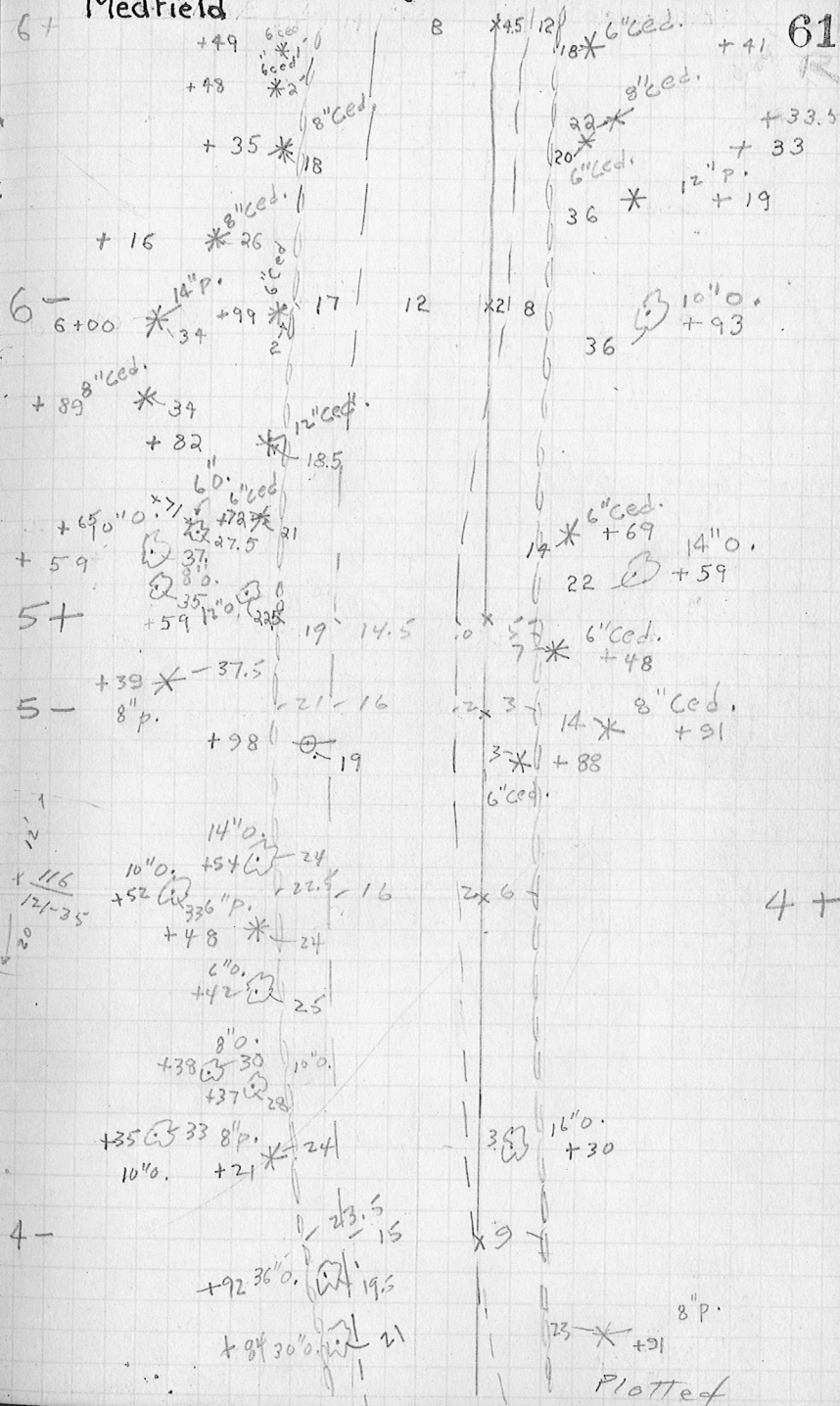
Detail



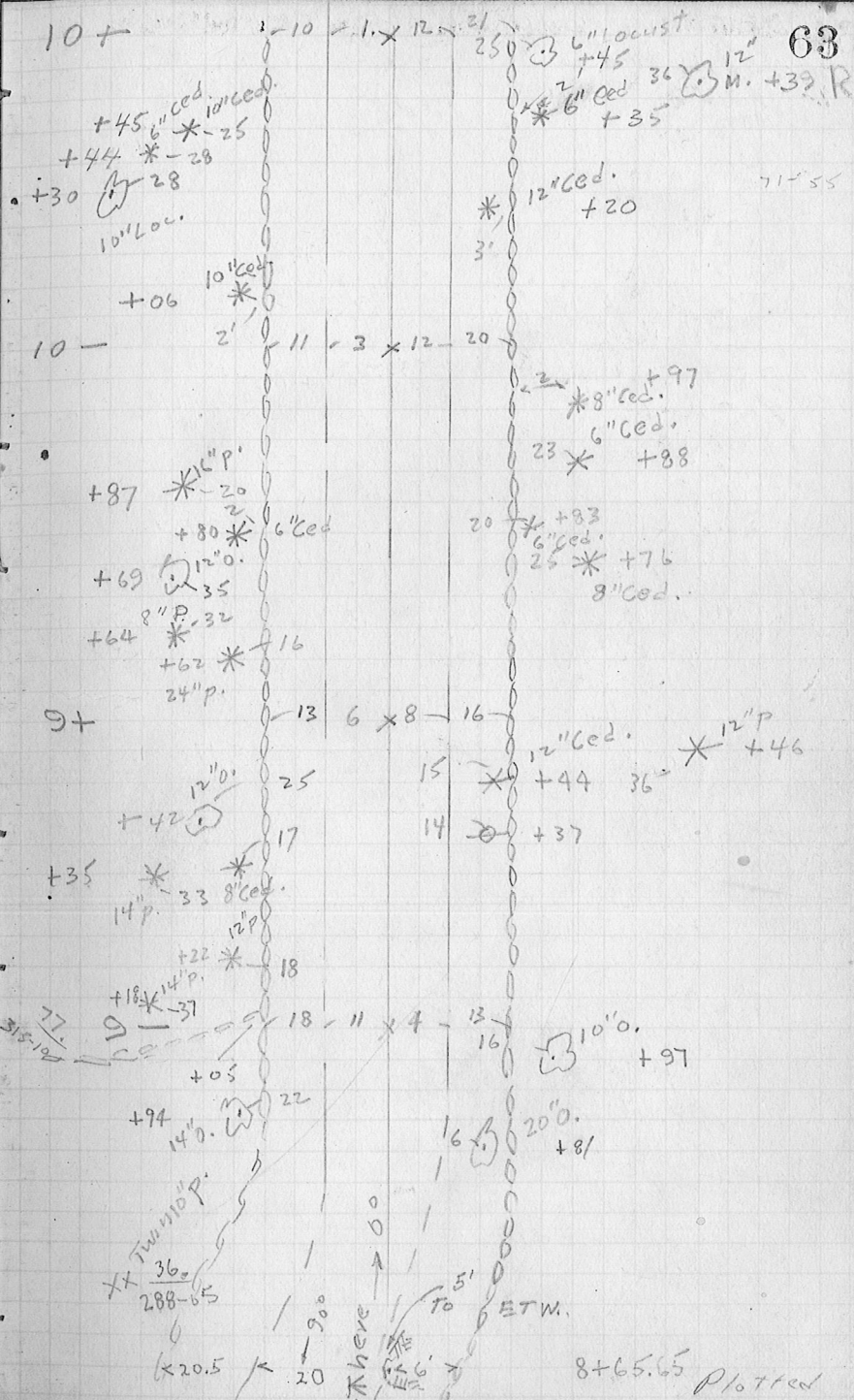
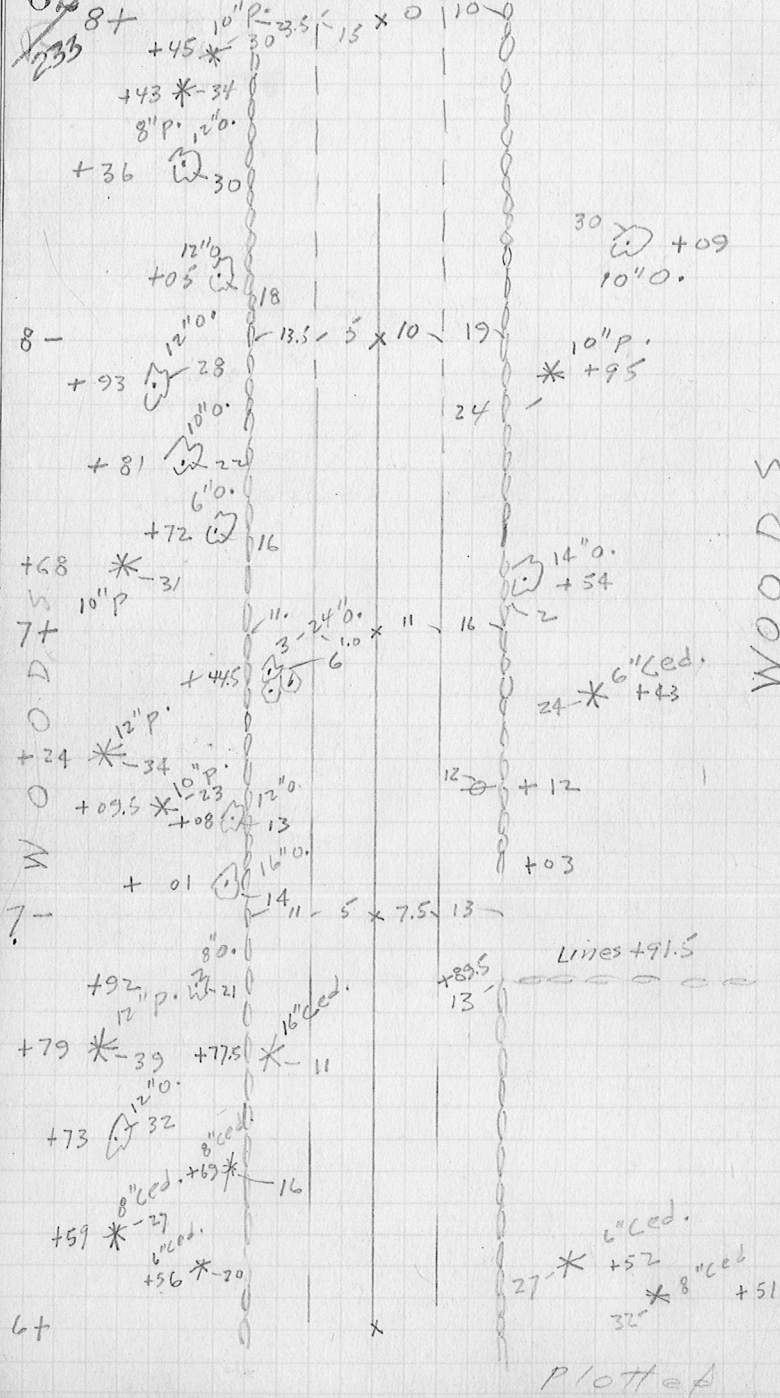
$0 + 0 = 9 + 48.05$ ORCHARD ST.
 see N.B. 229.
 P. 76
 Plotted

Medfield

61



62 Detail Causeway St. Medfield



64 Detail Causeway St. Medfield

233
 +82 * 20
 +80 8" M. 26
 +68 * 20
 +62 12" M. 43
 +59 8" ced 20
 12+ 18 11.5 x 3
 +49
 1
 +40
 +21 8" O. 26
 +05 8" ced.
 +03 18" O. 22.6 k
 12- 15.5 10.5 x 5.5 13
 +98 * 24
 +84.5 15.5
 10" M.
 0
 11+ 10.5 5 x 10 17
 +21 4' 10" Loc.
 +84 3
 +58.5 8" ced.
 4'
 23 26 22 6" M. 52
 12" A. 50+
 12" M. 43
 6" E. 22 8" P. 17
 30.5 * 14
 27 10" O. 17
 30" P. * 94
 2 12" M. 70
 32
 + 15 16 23 10" P. 55
 7' 10" E. 30.5
 39 14" P. 11
 12" ced. 21
 14" O. 47 70
 plotted

NOTE - This E/CU. 15
Approx. 15' above E.T.W.

V
 A
 O

M

[illegible]

NOTE
This

13-

-E D G E

2/7

+60 6" hem. * - 20'

 $20' \rightarrow$

40 -  100. + 55

~~Plotted~~
(done)

+91.5 } 12" M
(.) — 23

$$37.0 - (\cdot) + 62$$

Plotted ~~on~~

21 +

70
#233

+49 30"0.

+35 10"4"0.
+34 18"m. 7

+09 12"0. 7

Twin 12"0.
+02 7

25 - 10.5' x 14

+92 14"0.
4

+61 20"p. 11.5

24 + 20"p. 10 0 x 14

+48 * -22
6"nut +45 6'

8"nut +25 8

15"p.
+12.5 * -30

24 - 11' x 11.5

+98 -11.5

LINES +01 +97 14"nut
Twin 12"0.

+84 24"0.

+79 10

+64 8"p. * -14.5

23 + +52 8" * -22 12 23 x 11

+32 8"p. * 16.5

+24 * -20.5

19.5 +33 10"m
34 - +31

33 - 10"0. +17

35 12"0.
+99 +93

29 8"0. +87 6"0.
24 +64

26 10"0.
+41

27.5 6"0.
+32

28 6"0.
+16

31 10"0.
+35

25 8"0.
+87

12"0. 10"0.
36 - +75

24 * 6"p. +67

26 * 6"p. +53

25 * 6"p. +51

28 - 6"0. +37

27+50

+47 * 8"ced. 20
+40 * 8"ced. 20
12"p. 10"0.
+35 19.5

10"0. +29 * 19.5
+150

27 -

+04 -17.5

16 - 11 x 6
19 8"ced. 16

+30 * 18
+87 * 8"ced. 13

+84 * -42 12"p. +74 13
+68 16"0. 13

+41 12"p.
8"nut

26 + +50 * 27 14 - 6 x 11

+34 * -43 12"0. 11

12"p. +20 * -22 14"nut. 10

+16 * -36 16"p. 6"ced.
+11 * -14.5

26 - +89 * -28 18"p.

+85 24"0. 27.5

+74 * 13 16"p.

25 + +60 * -28 16"p.

21 - 0 x 14

17 * 6"p. +48

20 16"0. +35

22 6"0. +08

16 - 11 x 6
19 8"ced. 16

+30 * 18
+87 * 8"ced. 13

+84 * -42 12"p. +74 13
+68 16"0. 13

+41 12"p.
8"nut

26 + +50 * 27 14 - 6 x 11

+34 * -43 12"0. 11

12"p. +20 * -22 14"nut. 10

+16 * -36 16"p. 6"ced.
+11 * -14.5

26 - +89 * -28 18"p.

+85 24"0. 27.5

+74 * 13 16"p.

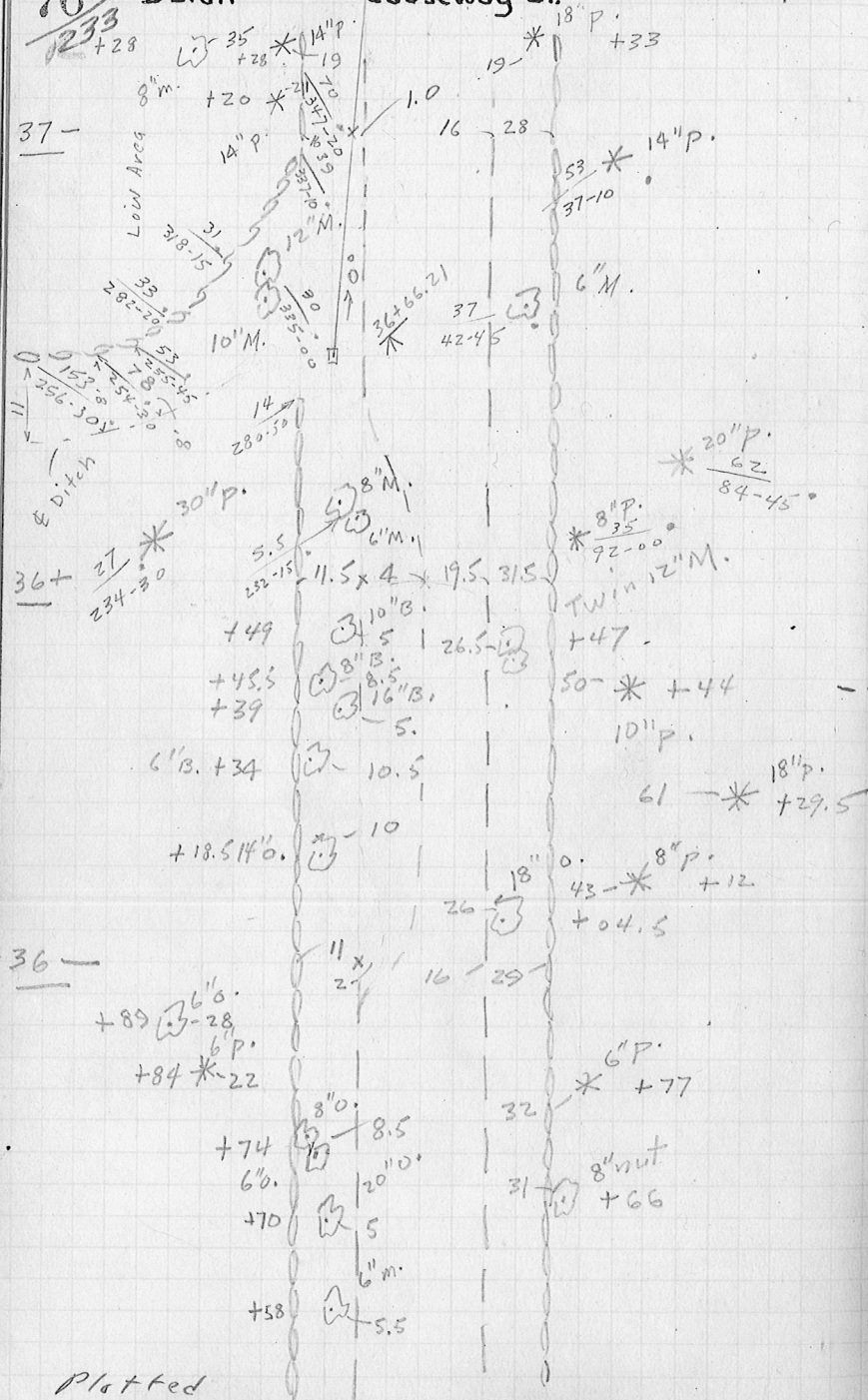
25 + +60 * -28 16"p.

WOODS

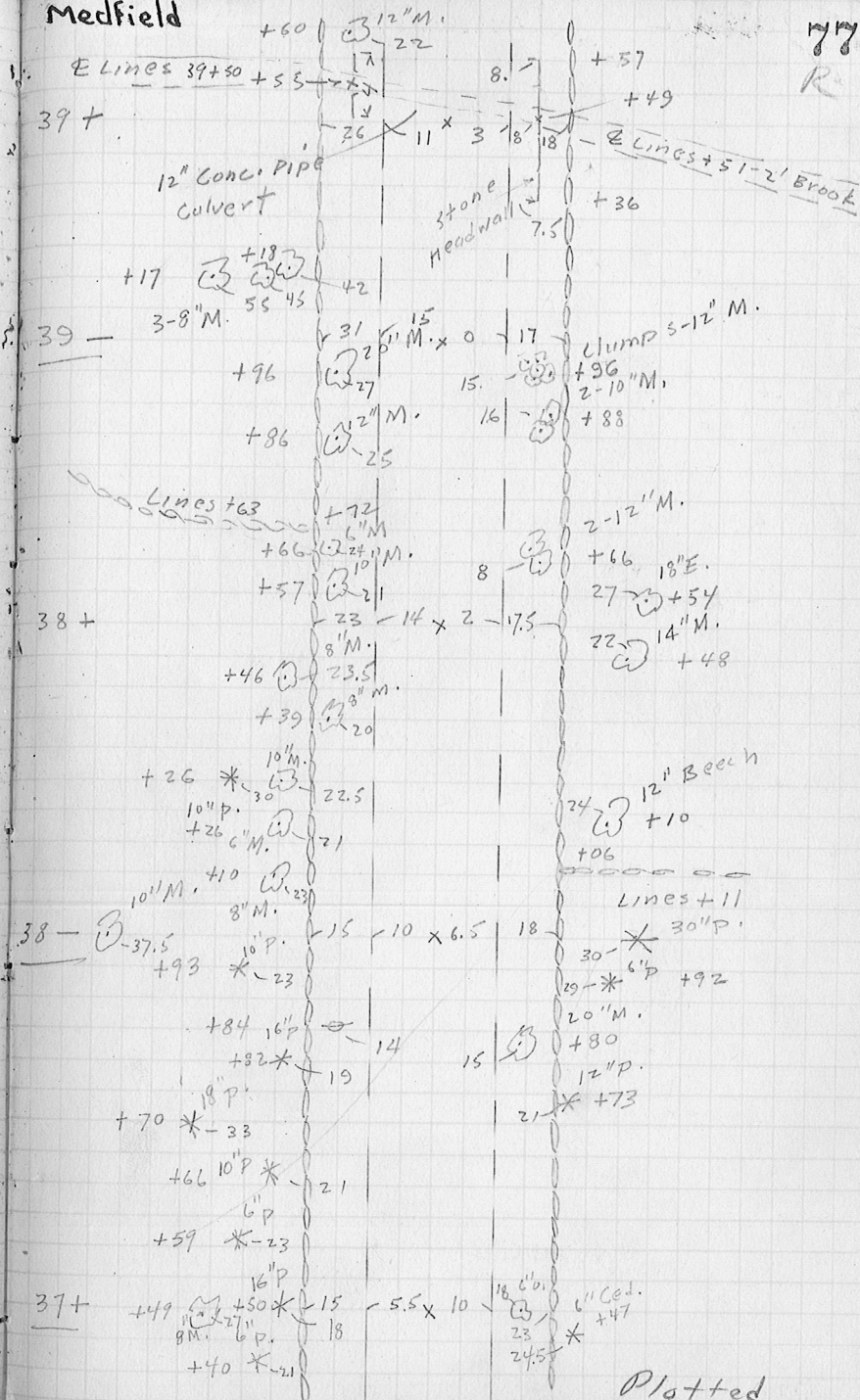
71
R

76 Detail

Causeway St.



Medfield



41+

WOODS (PINES)

Plotted

Medfield

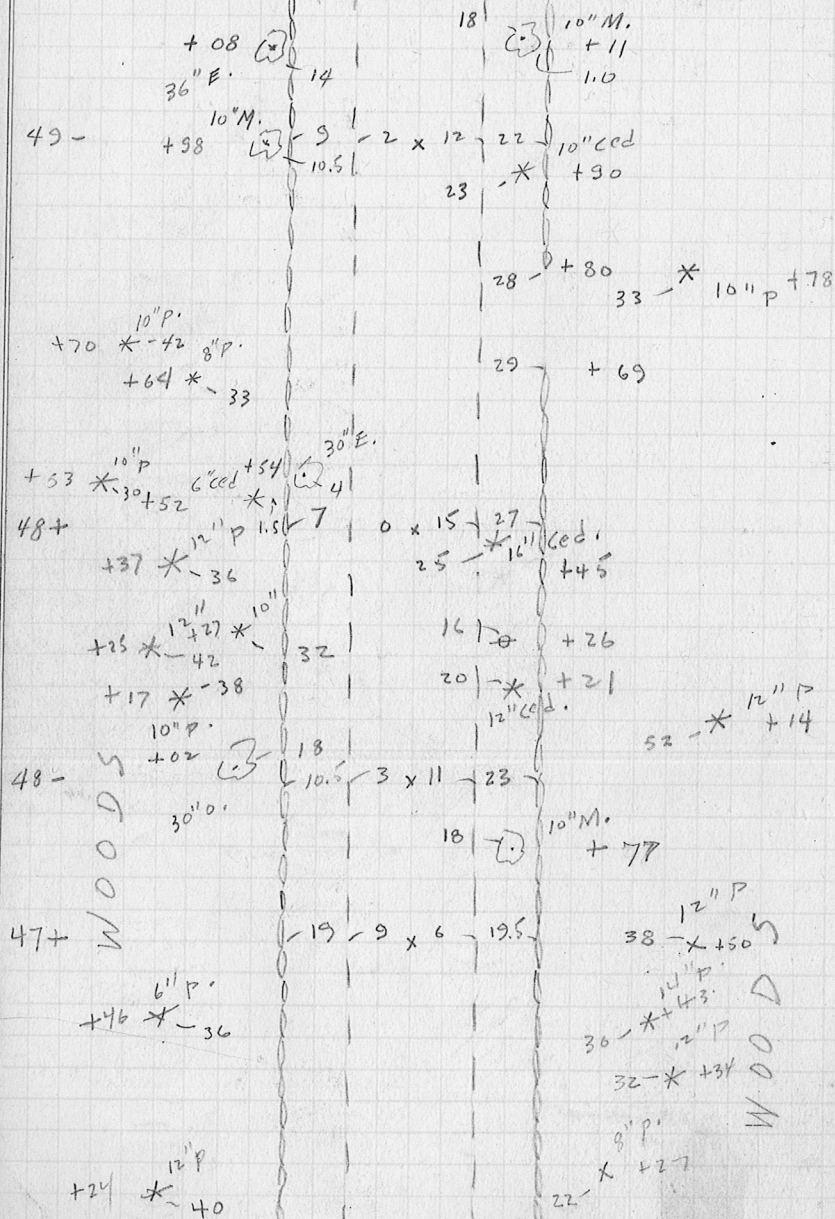
79

233

Woods

Plotted

233



PLOTTED

51-

50+

50-

49+

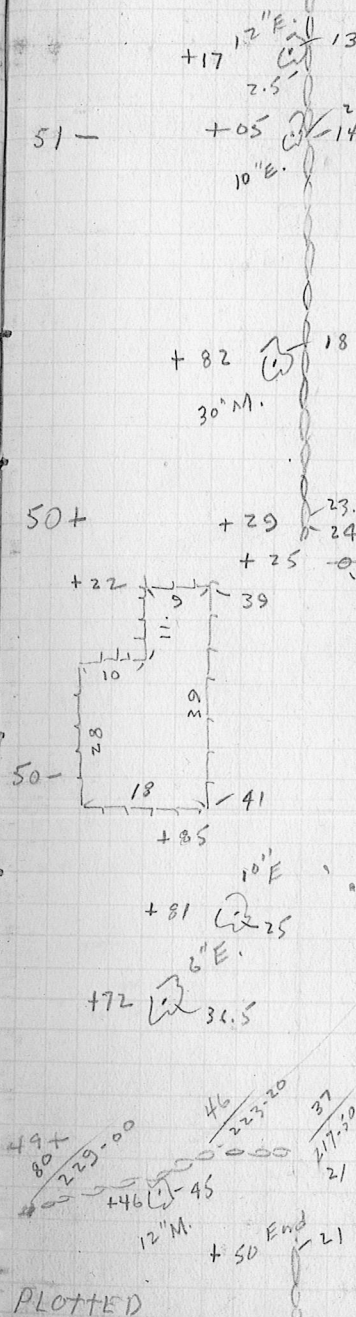
46

44

42

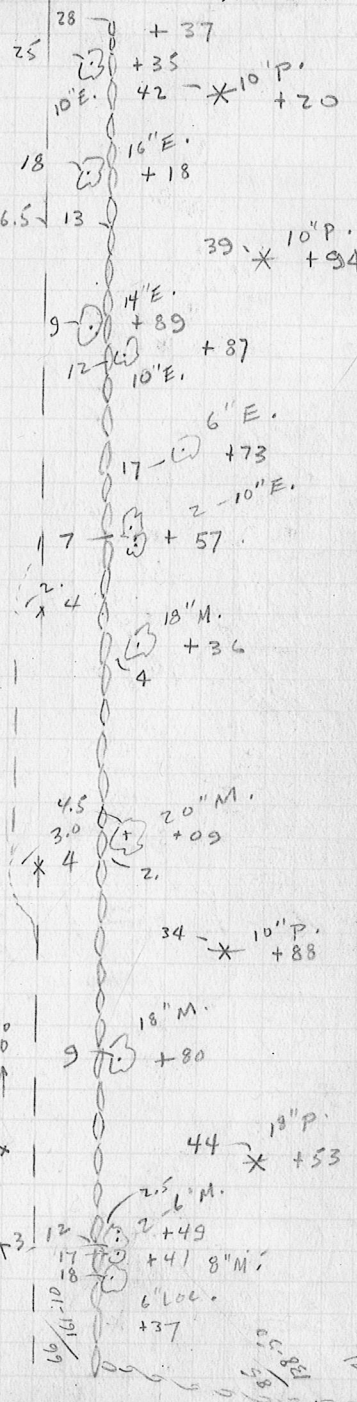
40

38



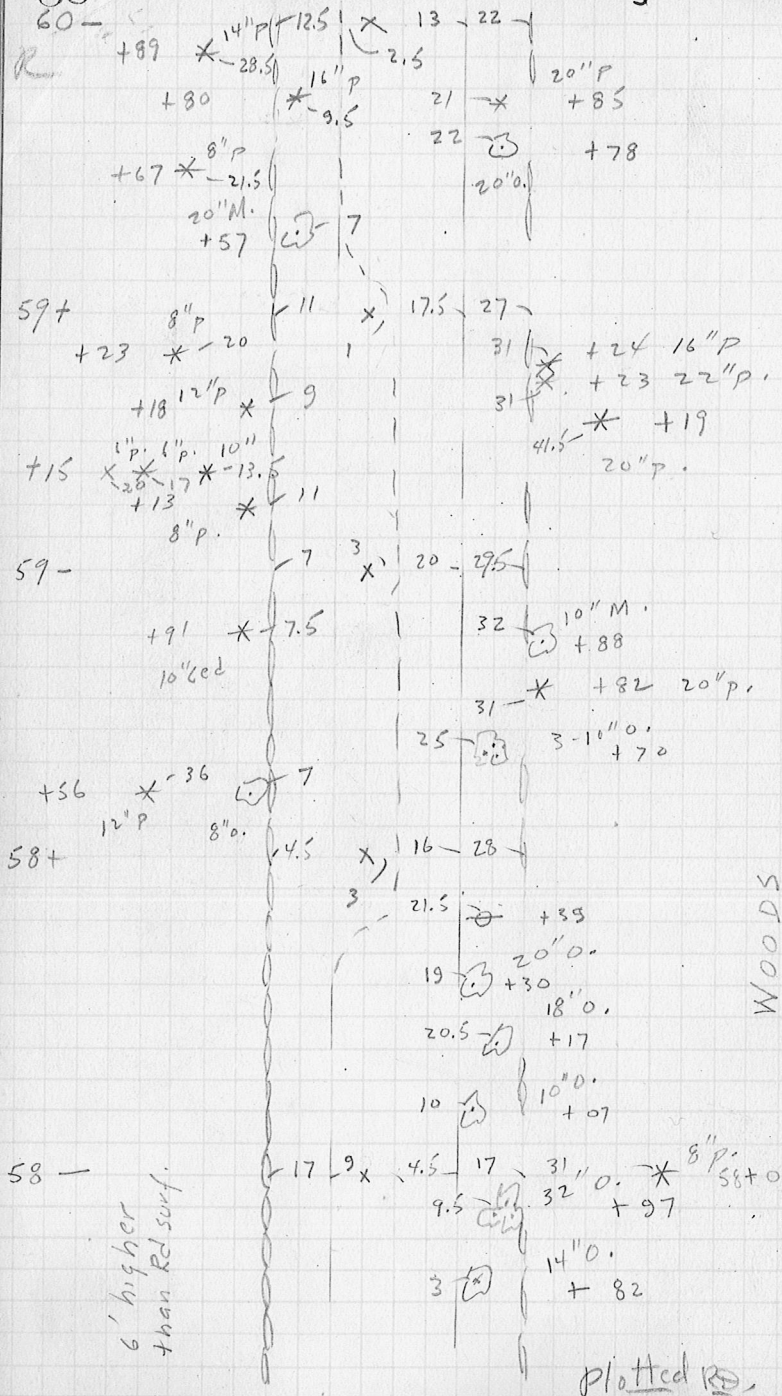
PLOTTED

WOODS (PINES)



88 Detail

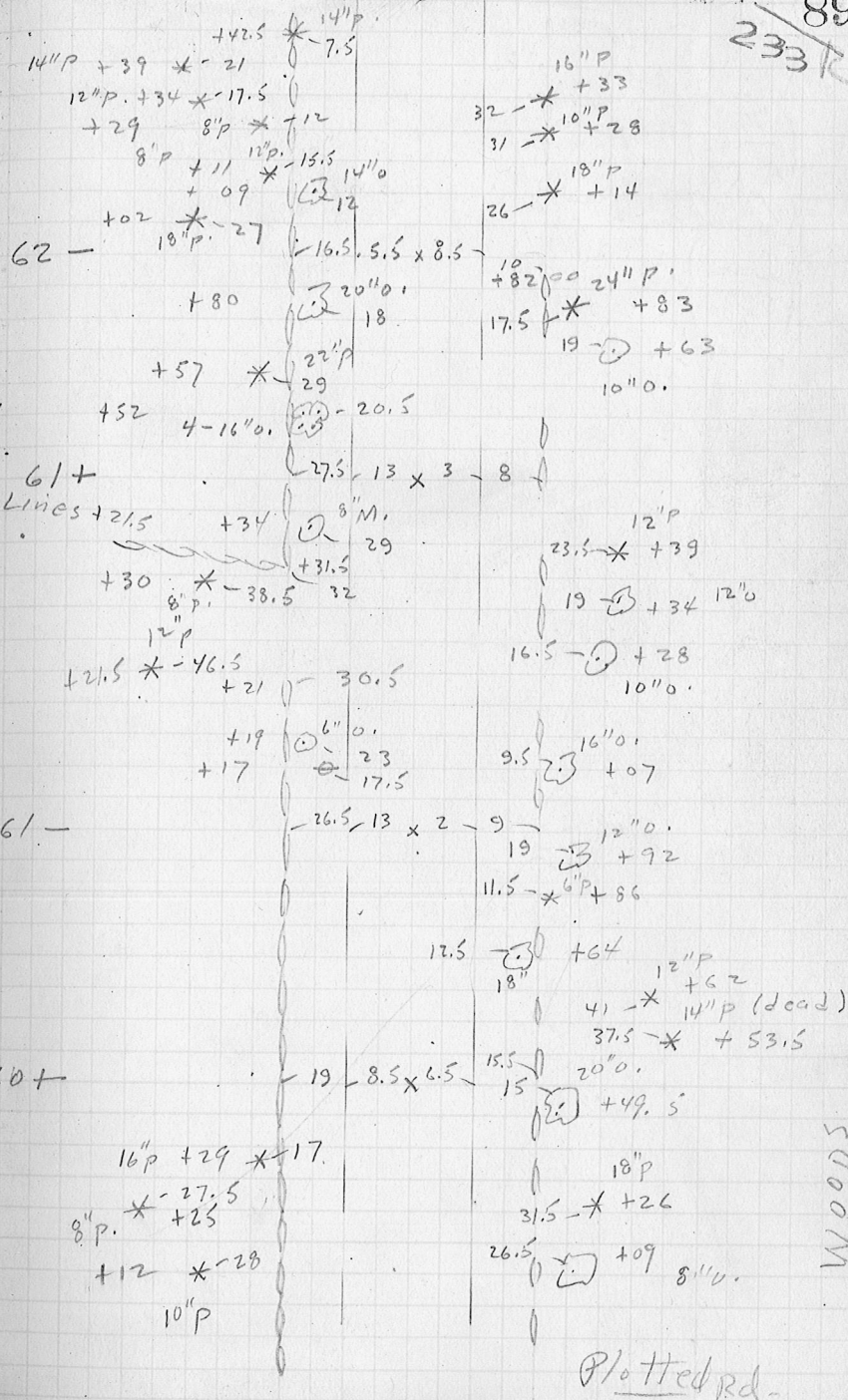
Causeway St.



Medfield

89

233R



233

64 +

+61 -12

+41 * 14" 13 - 0 x
+38 * 27.5
10" P. 27.5

3-12" M. +28 14

+19 15.5

+08 * 22

+06 * 10" P. 40

64 - 18 P. 20 12 x 5

+78 6" O. 16.5

+77 * 20" P. 39

+75 * 12" P. 17

10" P. +67 * 25

63 +

+57.5 * 14" P. 19 22 16 x 0

+47 * 20.5

10" P. 22

+28 * 27

+21 * 22

10" O. 22

+03 * 16

12" O. 17 12 x 4.5

+92 * 18

+88 * 32

+72 * 25

20" P. 16" O. 9.5

62 +

12" P. * 25.5
104-55

20" P. 16.5 * +27 12" O.
41 - 1 +22

20 - 16 14" O.

30.5 +05 12" O.
41.5 +01 16" O.
Twin 10" O.

23.5 +94

19.5 +86 18" O.

18" O. +85

12.5 +84 +84 T

19 +83

4 - 14" O.

14" O.

34 +58

24" P. 36.5 * +22
24" P. 12 * +13

26 * 14" P. +03

42 * 14" P. +99

10" P. +91

37.5 * 16" O. 40 * +85

17 +80 8" P.

62 + 43.17

2.0

* 264-05

19

8.5

14" P.

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

14

92 Detail

Causeway St.

Medfield

20-93

68-

67+

67-

66 +

PINES and few small OAKS
6 ft. higher than

 $71 + 87.9$

71 +

71+

71-

704

70-

69 +

69-

766 * -35.3

1. $\times 17.5$

$$0 \times 16.5$$

6 15.5

$$15 = 3 \times 12$$

20, 8 x 7

7) $\times 10'' p. + 89$

14.5 * +73
12"p.

2233

75-

15-45-85-19

11-20

12" M + 87

74+

17-5-9-18

12.5

10" M + 41

14"E + 37

(2) 10.5

2-6"E + 21

(2) 13

74-

16-7-8-15

10-0

+ 43

14"E + 21

(2) 15

8"E + 17

(2) 17

13-0

8" Will + 02

Swampy

73+

Edge of swamp

19-8-6-12

Edge of Swamp

73-

21-10-4-11

14"E + 83

(2) 22

72+

24-14-3-7

72-

26-13-2-7

2-6"E + 99

(2) 19

Swampy

Charles River

wood rail

wood
plantingset up
75+94.81

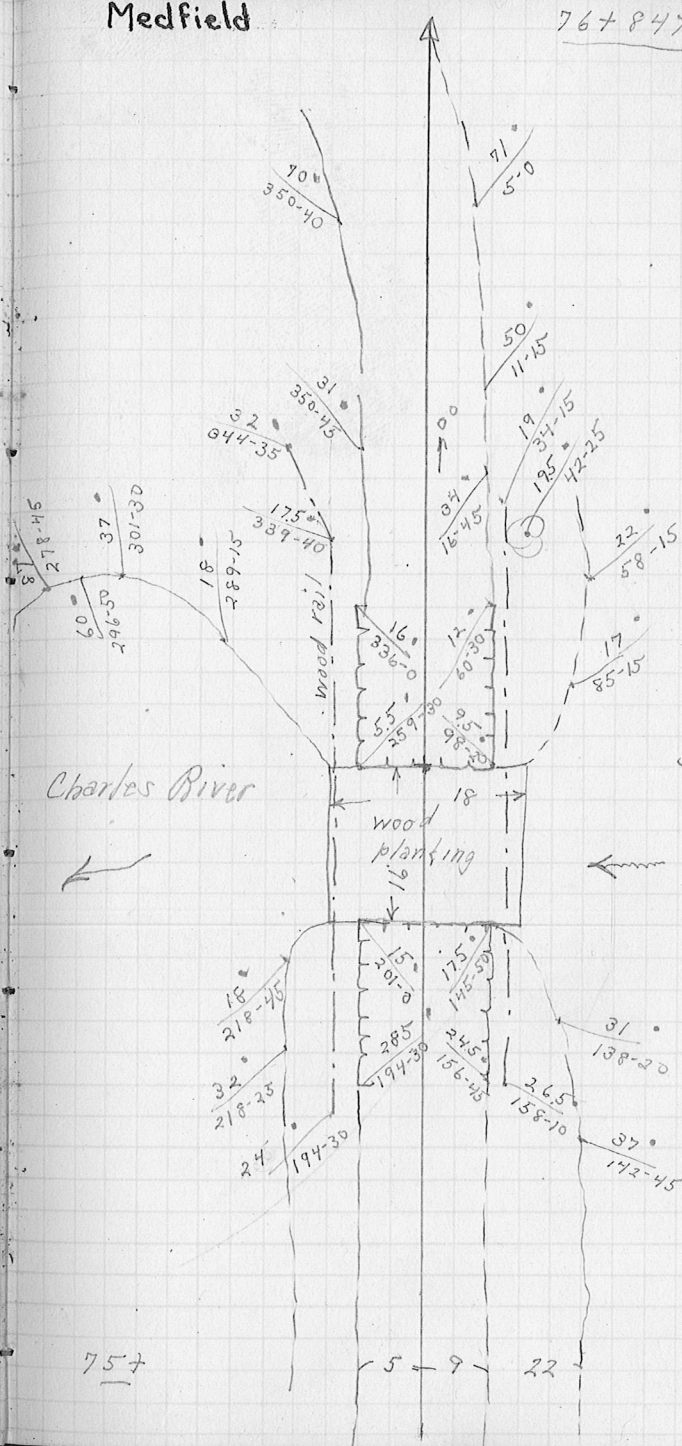
Charles River

swampy

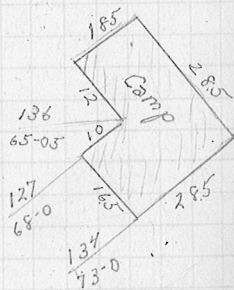
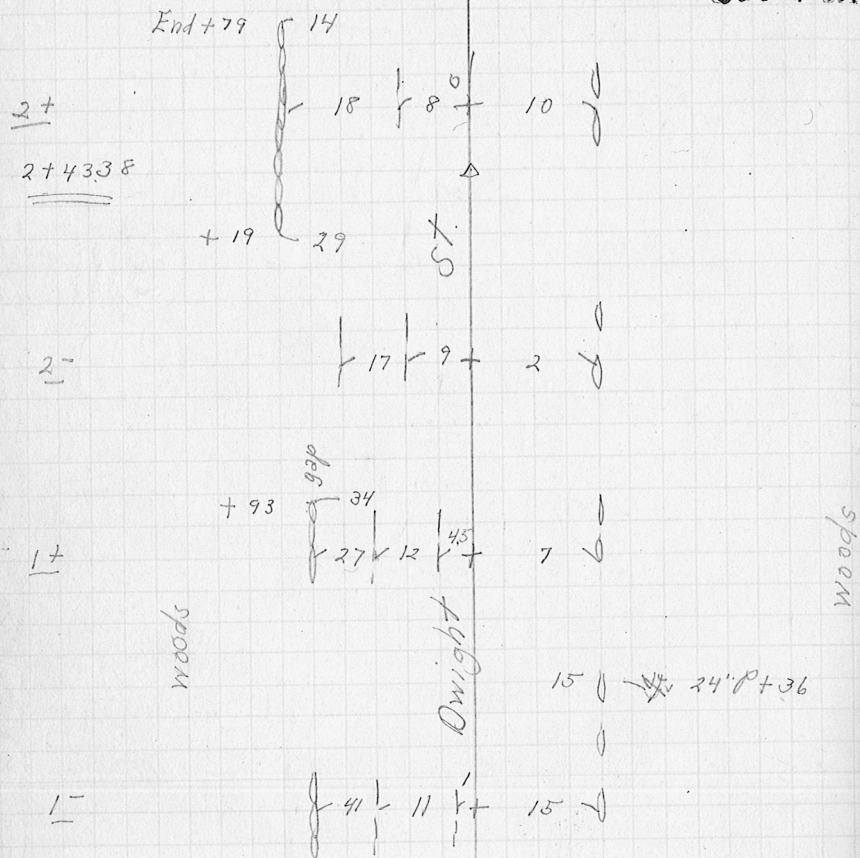
75+

5-9-22

flowing

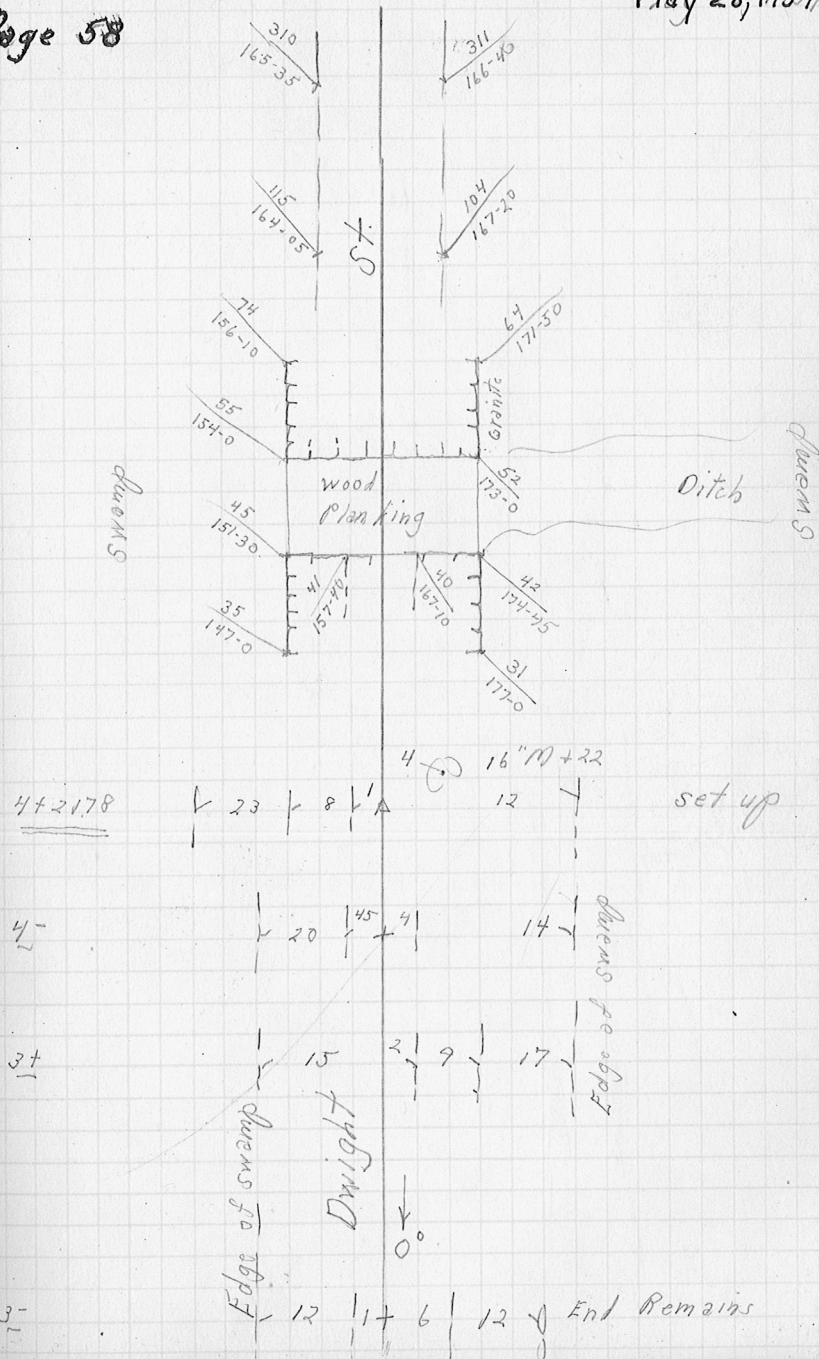


96 Additional Survey @ Dwight St.
233 See trav.



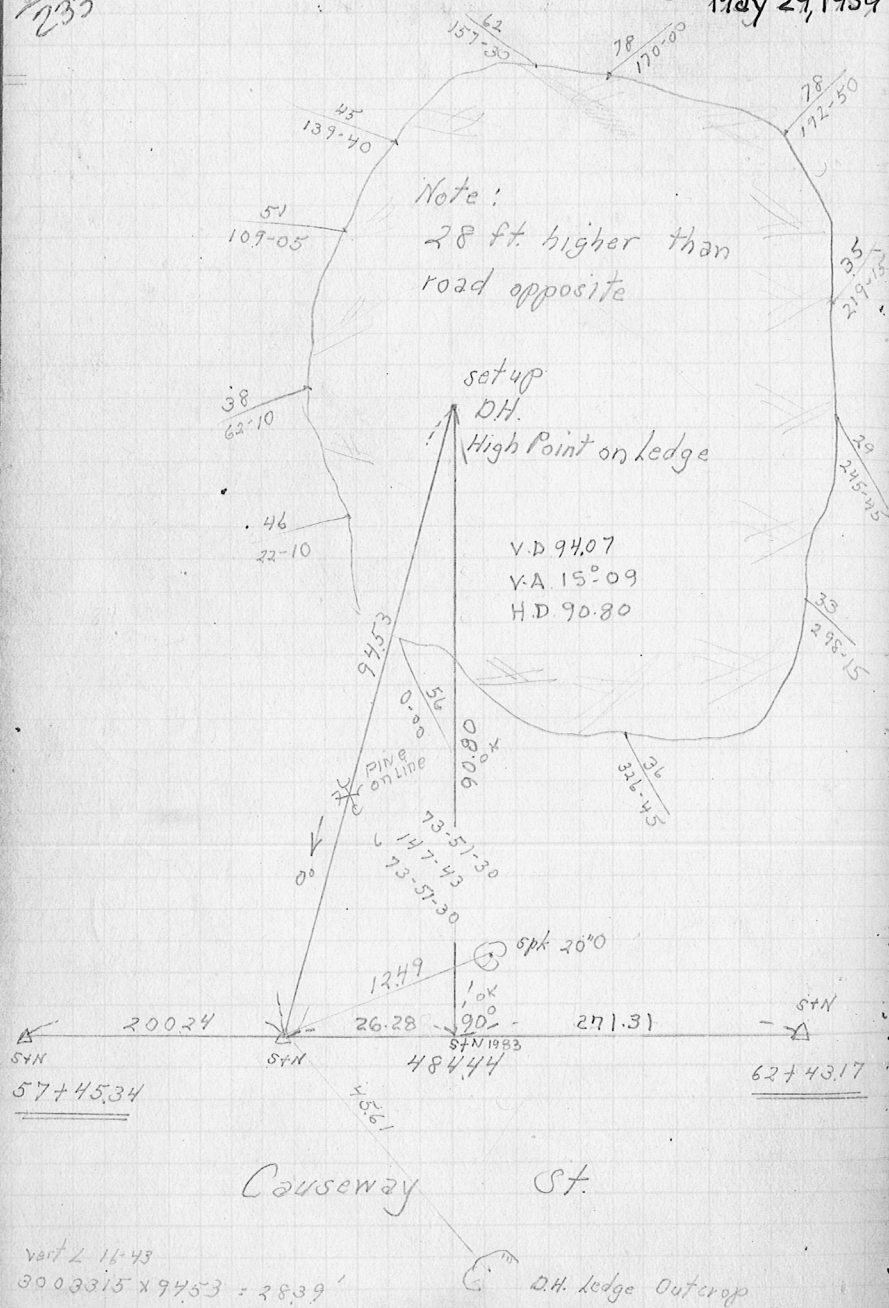
for Causeway St. Medfield
Page 58

R97
May 28, 1959



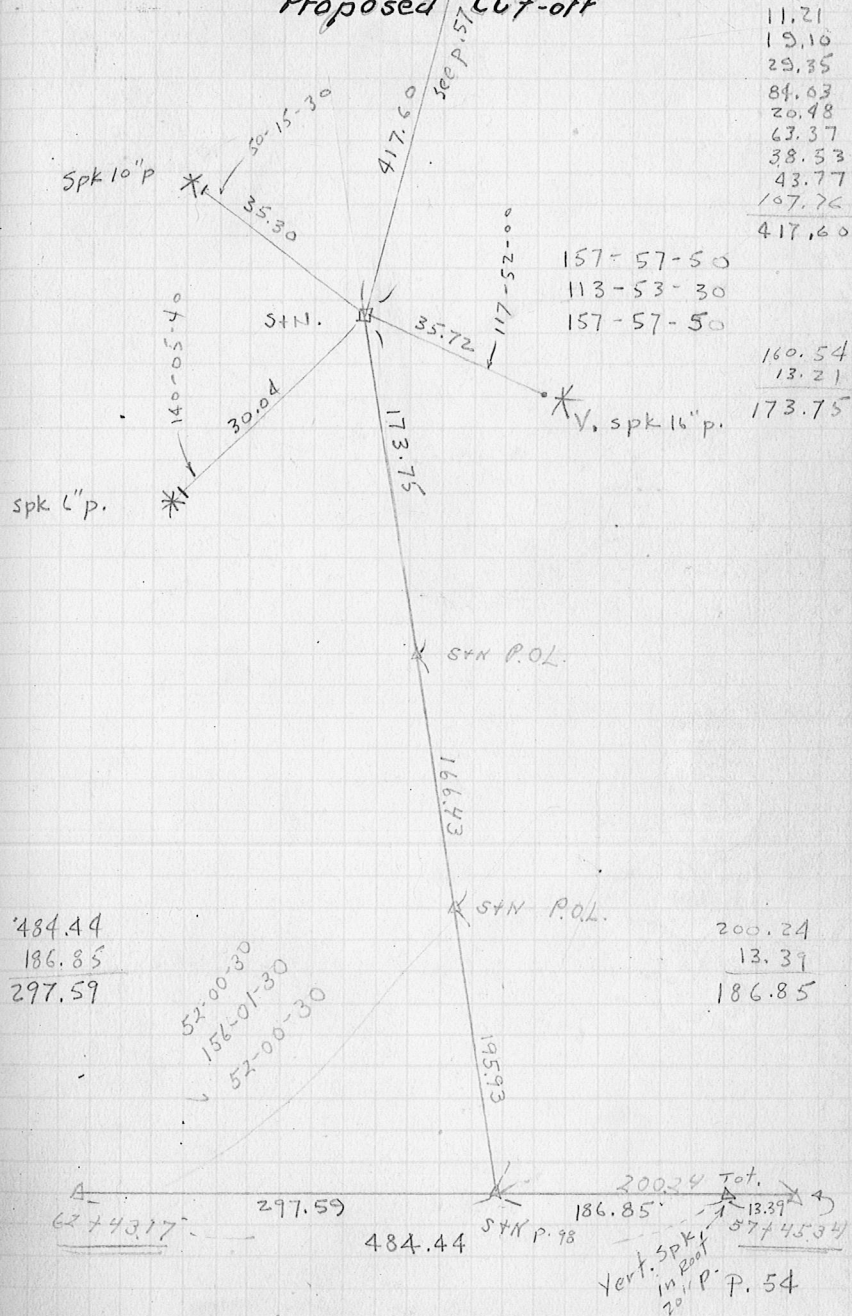
233

May 29, 1959



Traverse for Location	Slope on Proposed Cut-off
1	1:1
2	1:1
3	1:1
4	1:1
5	1:1
6	1:1
7	1:1
8	1:1
9	1:1
10	1:1
11	1:1
12	1:1
13	1:1
14	1:1
15	1:1
16	1:1
17	1:1
18	1:1
19	1:1
20	1:1
21	1:1
22	1:1
23	1:1
24	1:1
25	1:1
26	1:1
27	1:1
28	1:1
29	1:1
30	1:1
31	1:1
32	1:1
33	1:1
34	1:1
35	1:1
36	1:1
37	1:1
38	1:1
39	1:1
40	1:1
41	1:1
42	1:1
43	1:1
44	1:1
45	1:1
46	1:1
47	1:1
48	1:1
49	1:1
50	1:1
51	1:1
52	1:1
53	1:1
54	1:1
55	1:1
56	1:1
57	1:1
58	1:1
59	1:1
60	1:1
61	1:1
62	1:1
63	1:1
64	1:1
65	1:1
66	1:1
67	1:1
68	1:1
69	1:1
70	1:1
71	1:1
72	1:1
73	1:1
74	1:1
75	1:1
76	1:1
77	1:1
78	1:1
79	1:1
80	1:1
81	1:1
82	1:1
83	1:1
84	1:1
85	1:1
86	1:1
87	1:1
88	1:1
89	1:1
90	1:1
91	1:1
92	1:1
93	1:1
94	1:1
95	1:1
96	1:1
97	1:1
98	1:1
99	1:1
100	1:1

99



~~100~~
233

101

Causeway St. Medfield
 Prelim. Elevations on Proposed Cutoff
 Call Sta. 2+0 opposite Survey spk. 53+75.41

Sta.	Rod	Elev.	T	HI	—	Remarks
		100.00				Vert. spk 14" Elm Assumed Elev. 100.00
			2.37	102.37		
		96.61	4.56	101.17	5.76	T.P. Stone
0+0	5.4	95.8				
	4.5	96.7				LT 16.0 & T.W
0+50	7.1	94.1				
	4.6	96.6				LT 17.5 & T.W
1+0	7.6	93.6				
	4.6	96.6				LT 20.0 & T.W
1+50	7.5	93.7				
	4.5	96.7				LT 23.0 & T.W
2+0	4.7	96.5				
	4.5	96.7				LT 21.0 & T.W
		97.16	8.09	105.25	4.01	T.P. Stone
2+50	9.3	96.0				
2+63	8.0	97.3				& T.W
3+0	5.7	99.6				
3+50	4.3	101.0				
4+0	+0.4	105.7				4+0 ± = & P.I. and Intersection of 5-foot offset P.I.
		105.24	10.95	116.19	0.01	T.P. Stk
4+50	+0.4	116.6				
		115.75	9.28	125.03	0.44	
5+0	1.5	123.5				
	0.5	124.5				LT 5.0
	6.0	119.0				RT. 25.0
5+50	6.3	118.7				
	5.7	119.3				LT 5.0
	11.9	113.1				RT. 25.0
6+0	15.5	109.5				
		113.42	0.17	113.59	11.61	T.P. Hor. Spk 18" P.I. = 6+34 ± = 59+45.58
6+34	4.6	109.0				Survey Base Line
6+45	4.5	109.1				& T.W
6+50	4.5	109.1				

✓ Z.B. 7/20/59

July 1959

Sta.	Rod	Elev.	T	HI	—	Remarks
7+0	5.6	108.0				
7+50	7.5	106.1				
		110.91			2.68	110.91 = Vert Spk Root 24 P.I. = 59+85.5 Survey Base Line LT 21.0
			39	111.30		B.M. 110.91
8+0	5.0	106.3				
8+50	3.2	108.1				
		110.81	10.41	121.22	.49	T.P. Stk
9+0	7.7	113.5				
	7.1	114.1				LT 5.0
	0.4	120.8				LT 35
	13.3	107.9				RT. 30
9+50	+2.2	123.4				
	+3.2	124.4				LT 5.0
	6.5	114.7				RT. 30
		121.14	11.23	132.37	.08	T.P. Stk
9+50	4.2	128.2				LT 35.0
10+0	2.5	129.9				
	2.4	130.0				LT 5.0
	1.4	131.0				LT 3.5
	7.5	124.9				RT. 30.0
10+50	1.9	130.5				
	2.0	130.4				LT 5.0
	1.7	130.7				LT 35.0
	3.7	128.7				RT. 25.0
11+0	4.1	128.3				
	3.9	128.5				LT 5.0
	2.3	130.1				LT 35
	6.2	126.2				RT. 25
11+50	6.8	125.6				
	6.7	125.7				LT 5.0
	5.5	126.9				LT 30
	5.1	127.3				LT 50
	7.4	125.0				RT 24
		126.72	1.07	127.79	5.65	
11+70 ±	5.0	122.8				Angle Pt.
	3.9	123.9				LT 25
	3.6	124.2				LT 40

✓ Z.B. 7/20/59

Sta.	Rod	Elev.	+	H.I.	-	Remarks
11+70±	3.6	124.2		127.79		Rt. 35
	3.7	124.1				Rt. 40
12+0	8.7	119.1				Lt. 30
	9.5	118.3				Rt. 30
	6.0	121.8				Rt. 50
	4.1	123.7				Lt. 40
12+50	11.4	116.4				RT. 20
	12.1	115.7				RT. 35
	11.2	116.6				T.P. Top of Stk
	11.2	116.6				
		117.41	1.09	118.50	10.38	
13+0	4.0	114.5				Lt. 30
	5.1	113.4				Lt. 50
	5.8	112.7				RT. 10
	4.8	113.7				RT. 30
	5.0	113.5				T.P. Stk
		108.80, 39		109.19	9.70	
13+50	3.7	105.5				Lt. 30.0
	3.0	106.2				Rt. 25.00
	4.3	104.9				Rt. 45.00
	7.8	101.4				Lt. 30
14+0	5.6	103.6				Lt. 66 E.T.W.
	7.0	102.2				Rt. 20.0
	13.7	95.5				Rt. 35.0
	6.2	103.0				Lt. 20.00
	9.5	99.7				Lt. 14 E.T.W.
14+50	9.3	99.9				Rt. 32 on ledge
	17.6	91.6				
	17.6	91.6				
	10.3	98.9				
		97.59	.95	98.54	11.60	
14+18	1.6	96.9				Lt. 18
	7.0	91.5				Lt. 36 E.T.W.
	7.2	91.3				Rt. 32 Edge Cart Path
	7.9	90.6				Cart Path
14+91	8.3	90.2				Rt. 30.0
	8.2	90.3				
15+0	8.5	90.0				Rt. 25.0
	11.5	87.0				Lt. 26.0 E.T.W.
	8.3	90.2				
		92.56	1.71	94.27	5.98	

Sta.	Rod	Elev.	+	H.I.	-	Remarks
15+50	7.1	87.2		94.27		
16+0	6.5	87.8				T.W
16+50	6.9	87.4				T.W
17+0	7.1	87.2				T.W
17+50	7.2	87.1				T.W
18+0	7.1	87.2				T.W
18+50	6.8	87.5				T.W
19+0	7.0	87.3				T.W
19+50	6.5	87.8				T.W
19+79±	5.0	89.3				on Bridge
		93.68	11.28	104.96	.59	T.P. stone
		104.38	8.19	112.57	.58	T.P. stone
				109.06	3.51	SPK Root 20" Pipe
				Survey	→	65+88.5 - RT. 32
						B.M. = 107.16
		109.06	3.42	112.48		
		107.69	7.40	115.09	4.79	T.P. stone
		110.93			4.16	B.M. Vert Spk (110.91)
		106.39	1.34	107.73	8.70	T.P. stone
		100.08			7.65	Assumed B.M. (100.00)
						Vert Spk

$$\begin{array}{r} 66.01 \\ 43.87 \\ 40.45 \\ 40.96 \\ 29.12 \\ 22.82 \\ \hline 243.23 \\ .07 \\ \hline 243.16 \end{array}$$

243.16

243.16

d.h. top hill Fo
St N on π Line
CAUSEWAY ST.

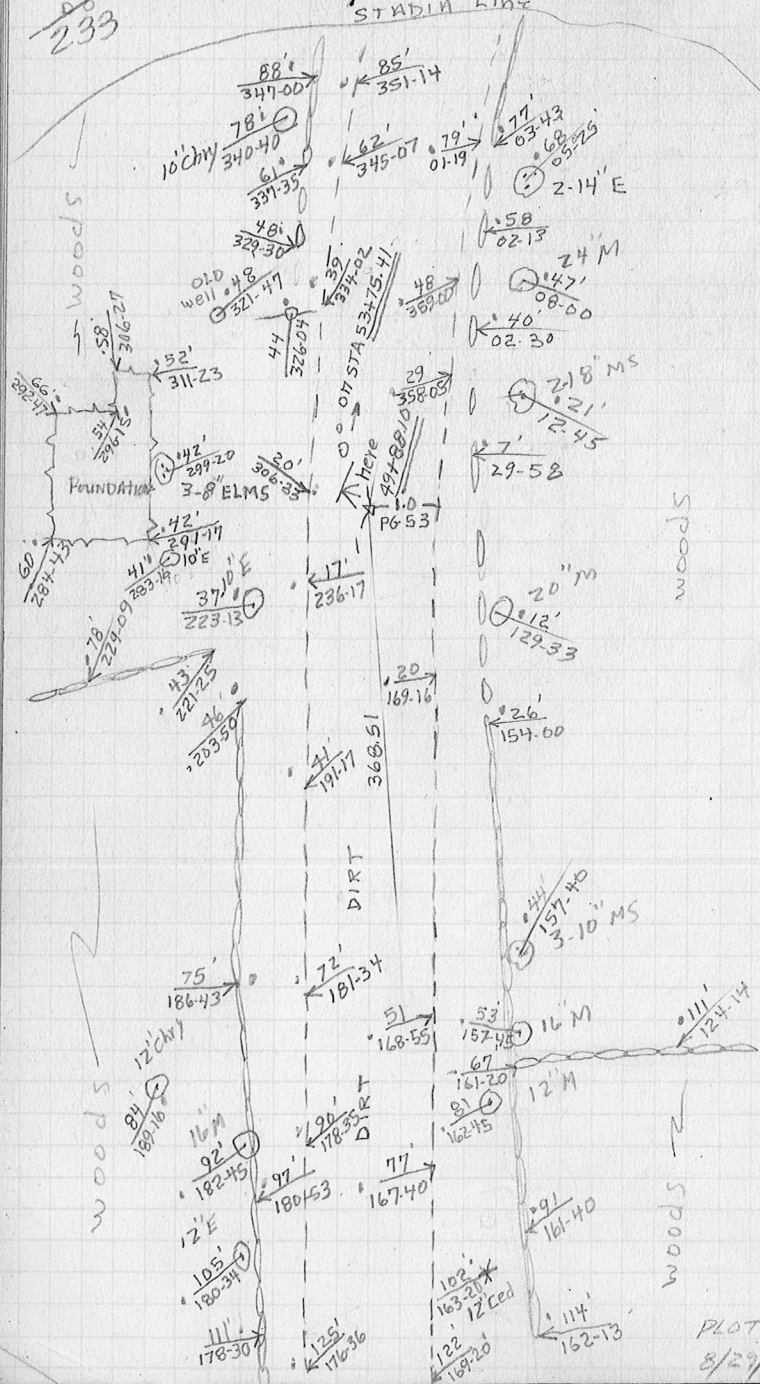
5+N on line

108
233

109

110 CAUSEWAY STREET

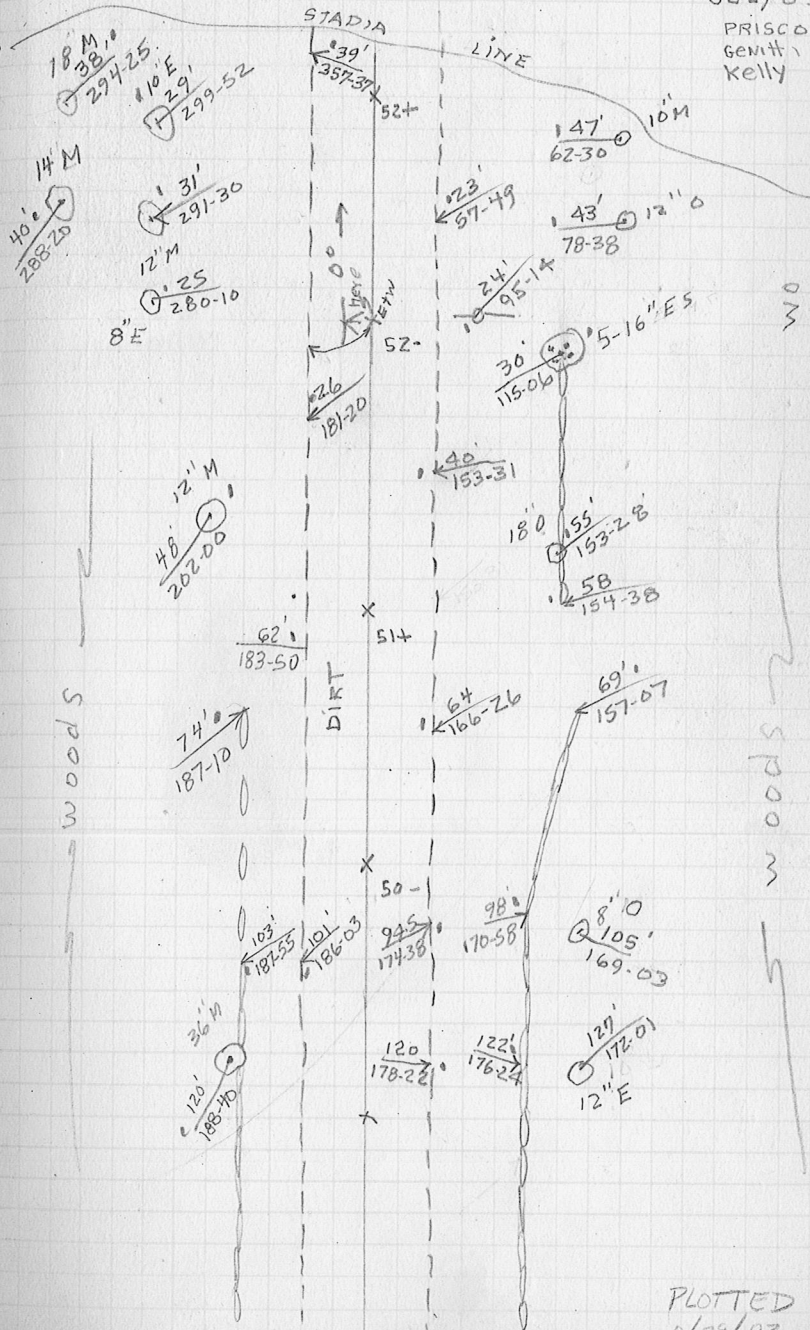
STADIA LINE



PLOTTED
8/29/83 ES

Inst.	Tape	Wthr & Temp.	Date	Crew
MEDFIELD			DETAIL	111

JULY 83
PRISCO
GENITH
Kelly



PLOTTED
8/29/83 ES

STREET

5003

Spooe

STADIA LINE

woods-

Plotted ES.
Aug 83

Inst. Tape
MEDFIELD

DETAIL

JULY 83

55+0

spoon

Ø 12" E +95
17

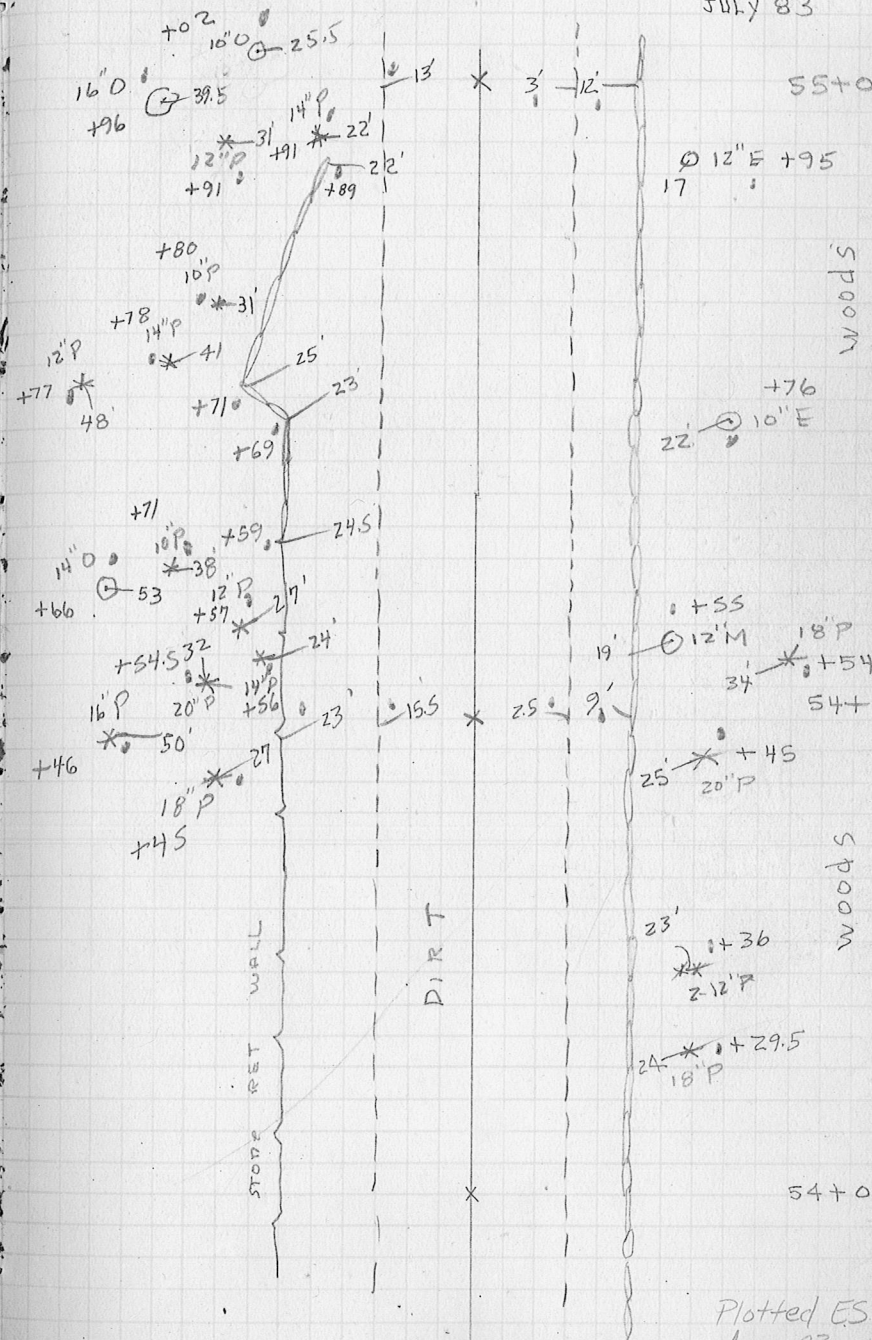
+76
10" E

18'P
* + 54
54+

woods

 $54 + C$

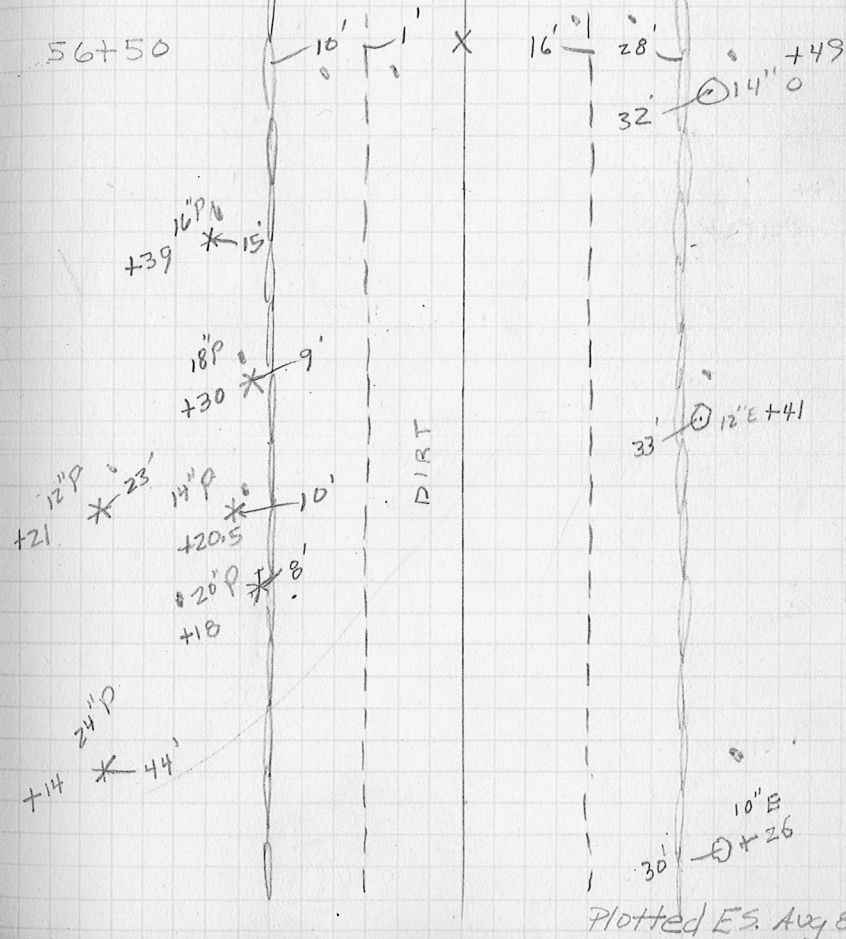
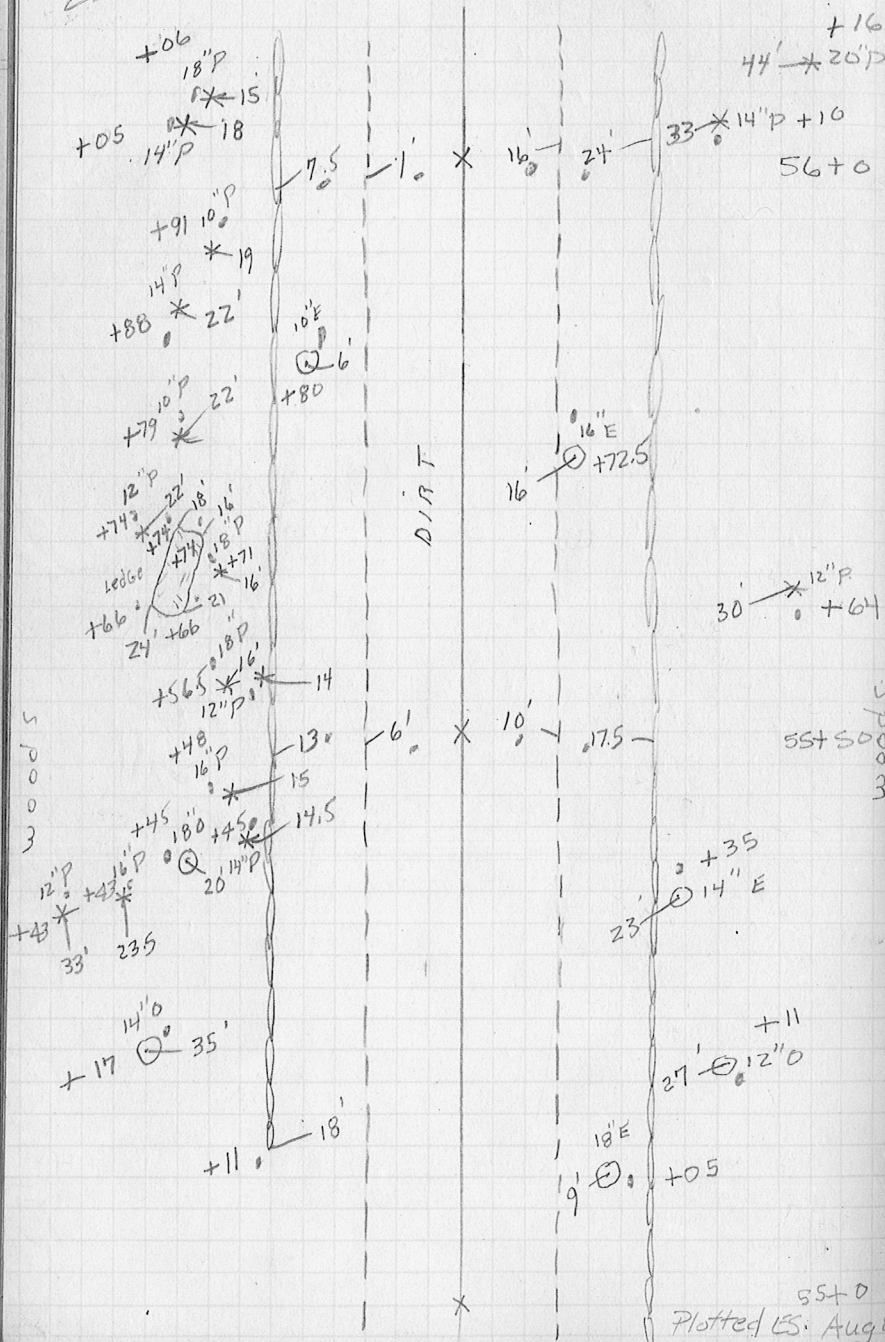
Plotted ES
Aug 83



114 Inst. Tape Wthr & Temp. Date Crew
CAUSE WAY STREET

Inst. Tape Wthr & Temp. Date Crew
MEDFIELD DETAIL

July 83



116

Inst.

Tape

Wthr & Temp.

Date

Crew

CAUSEWAY

STREET

MED FIELD

DETAIL

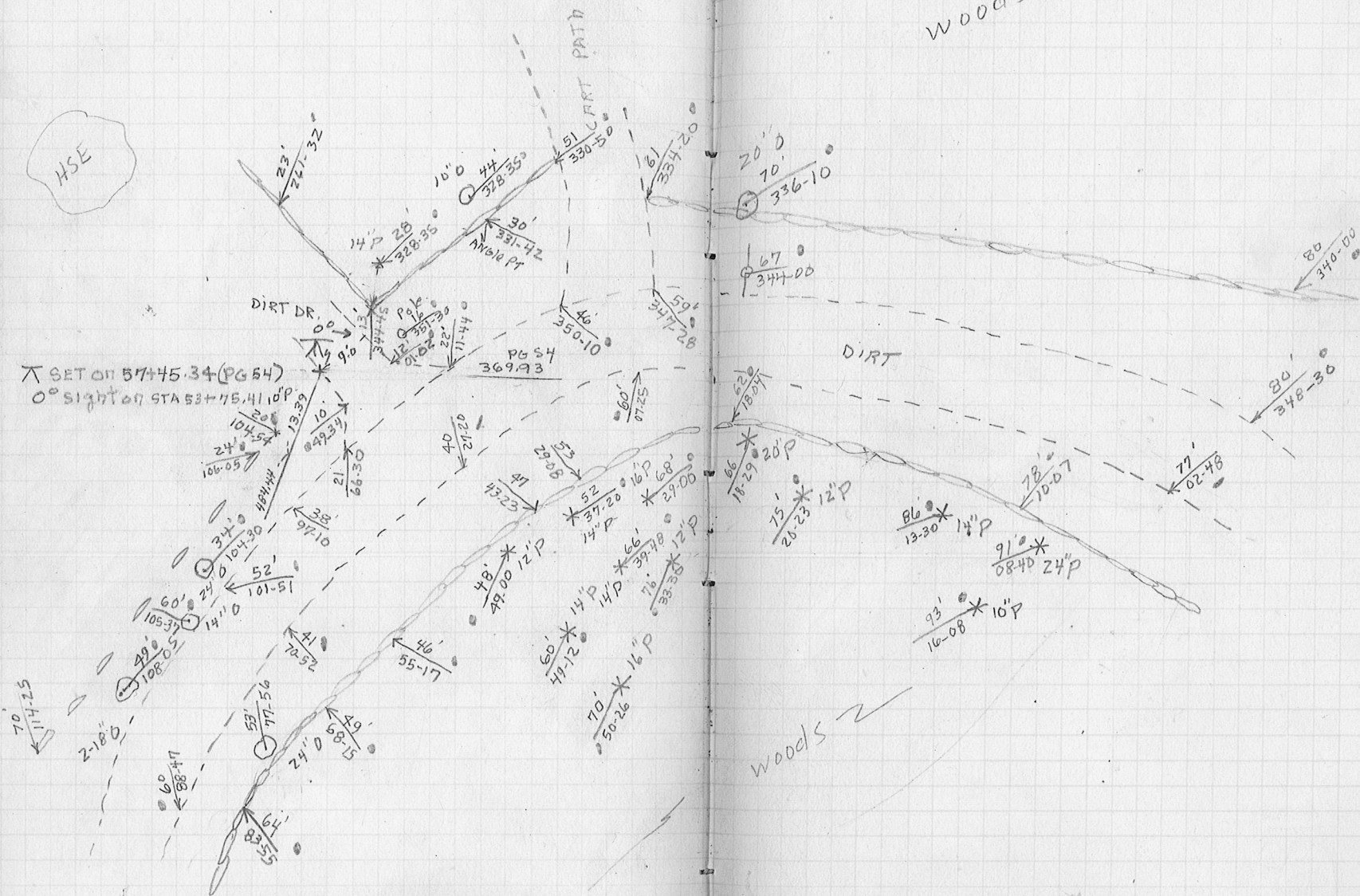
117

JULY 83

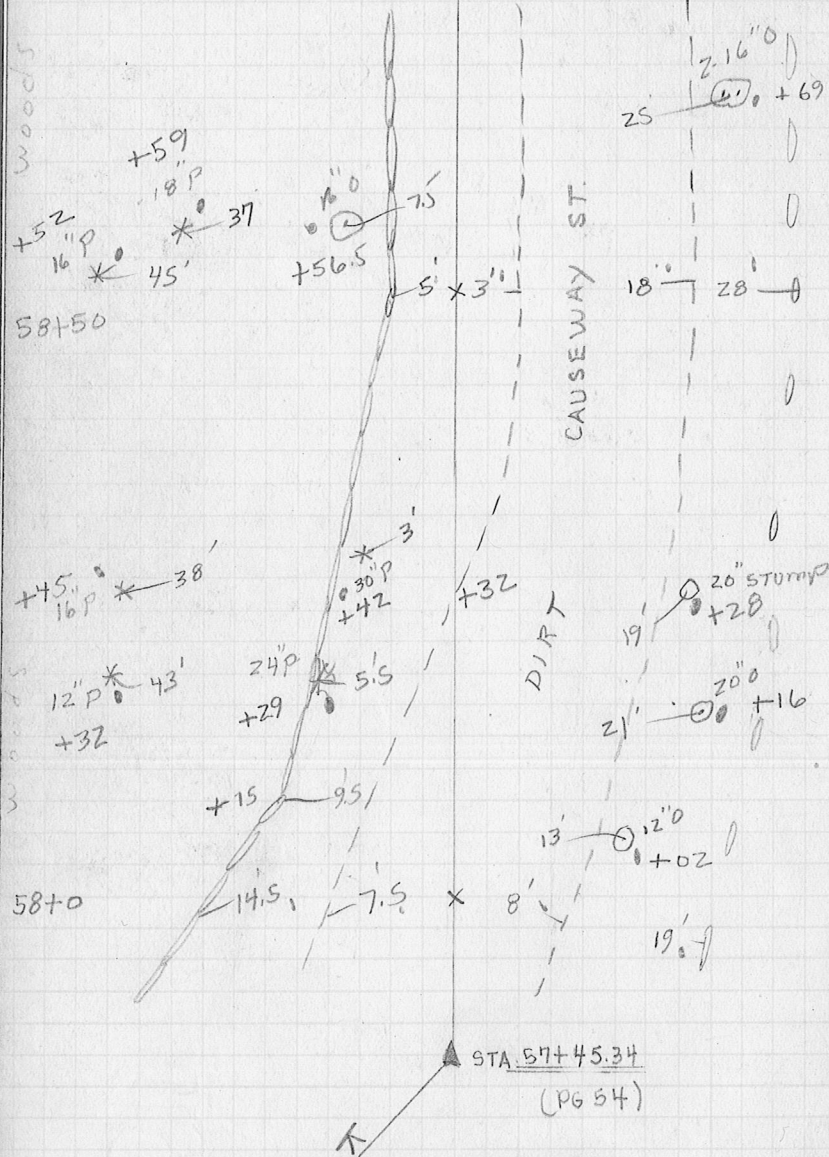
HSE

X SET ON 57+45.34 (PG 54)

0° SIGHT ON STA 53+75.41 10°

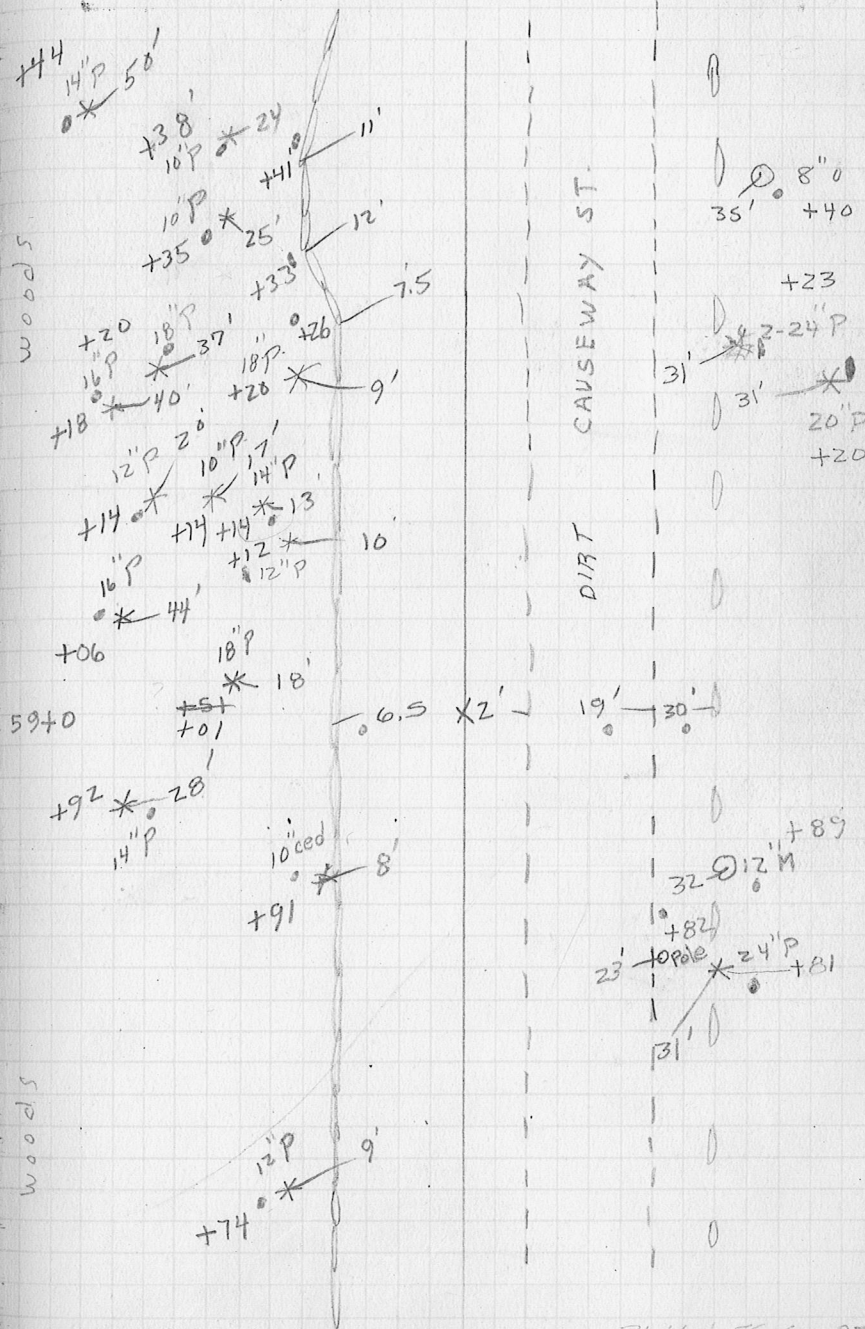


118 Inst. Tape Wthr & Temp. Date Crew
CAUSEWAY STREET



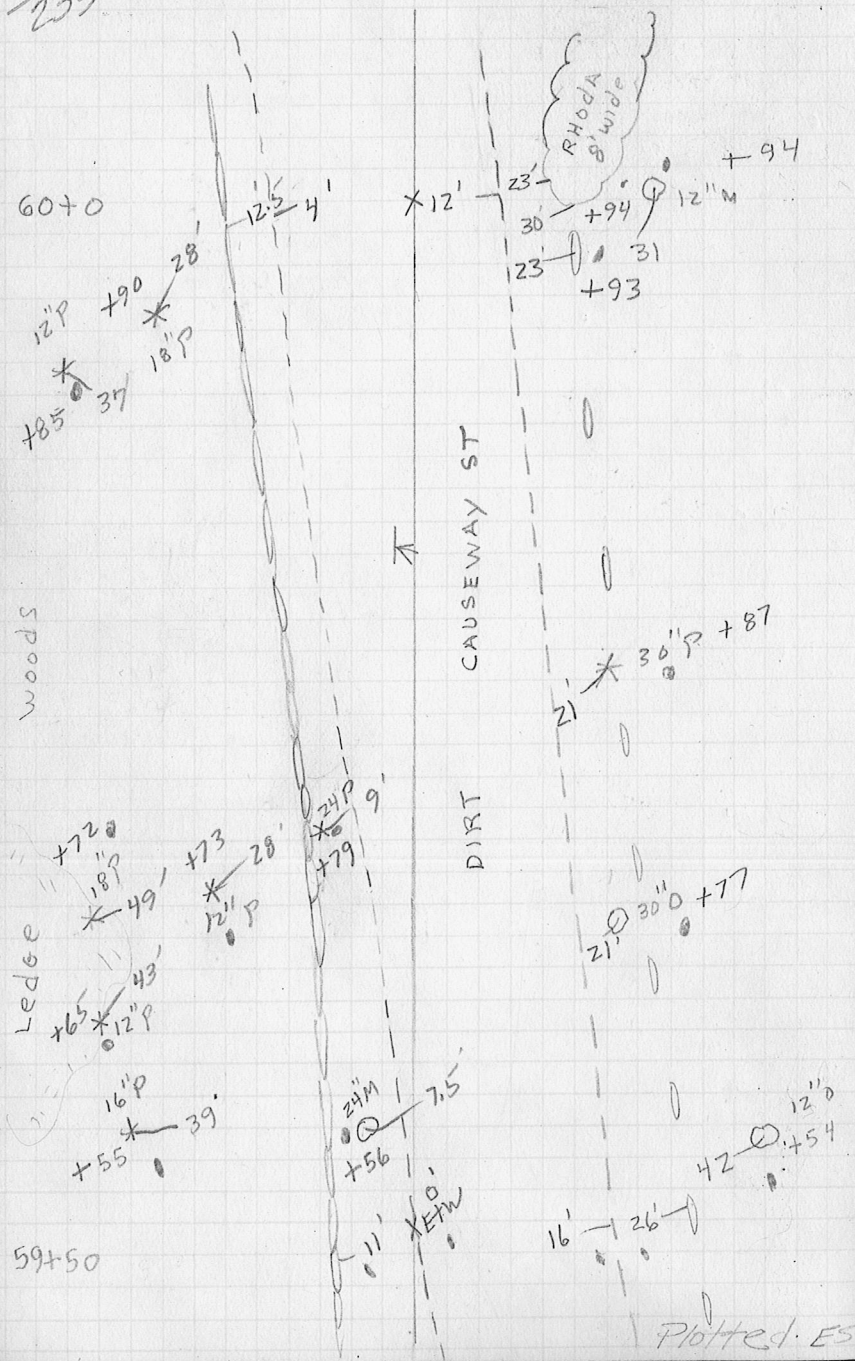
Plotted ES Sep 83

Inst. Tape Wthr & Temp. Date Crew
MEDFIELD DETAIL JULY 83 119
PRISCO

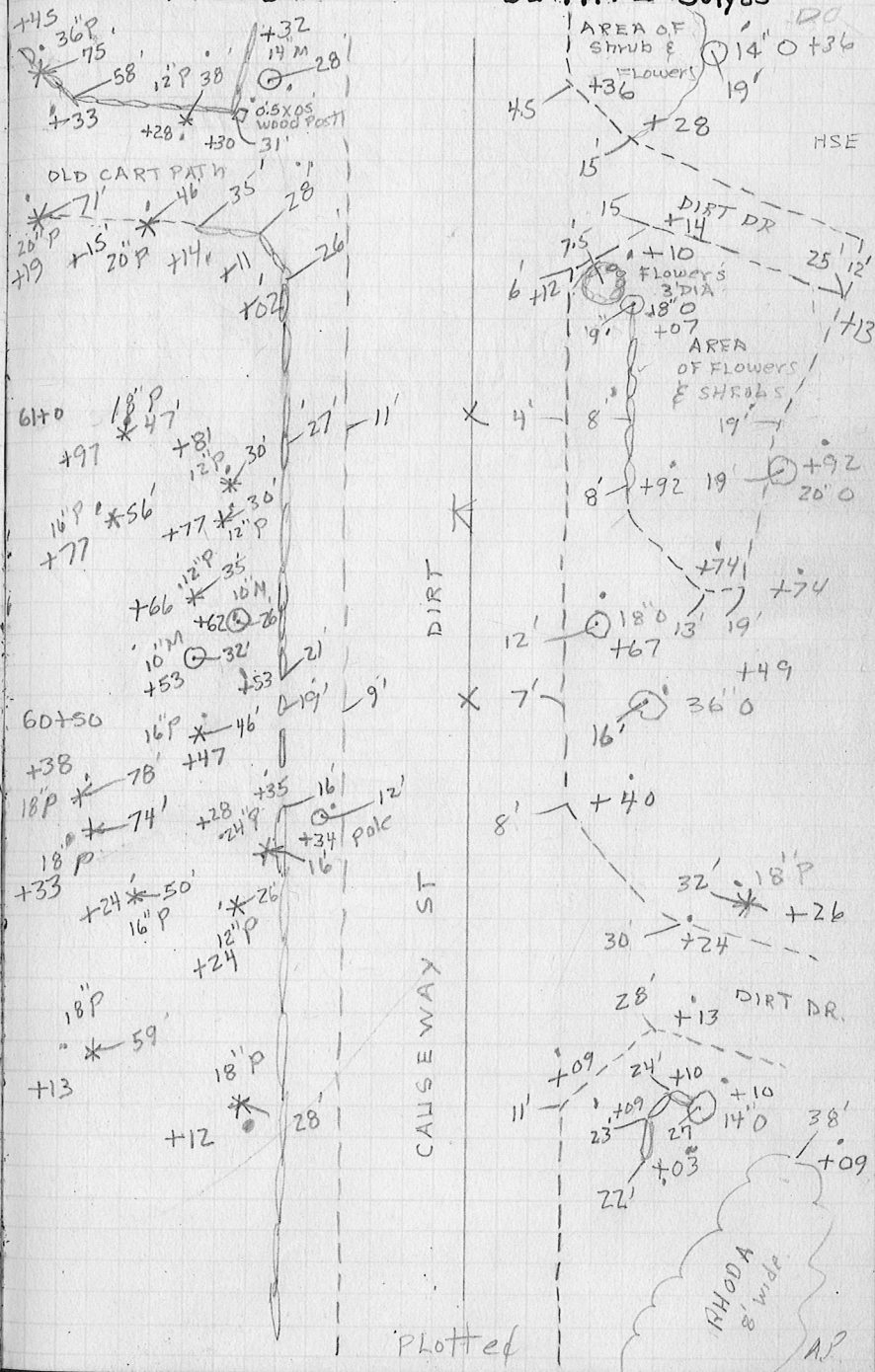


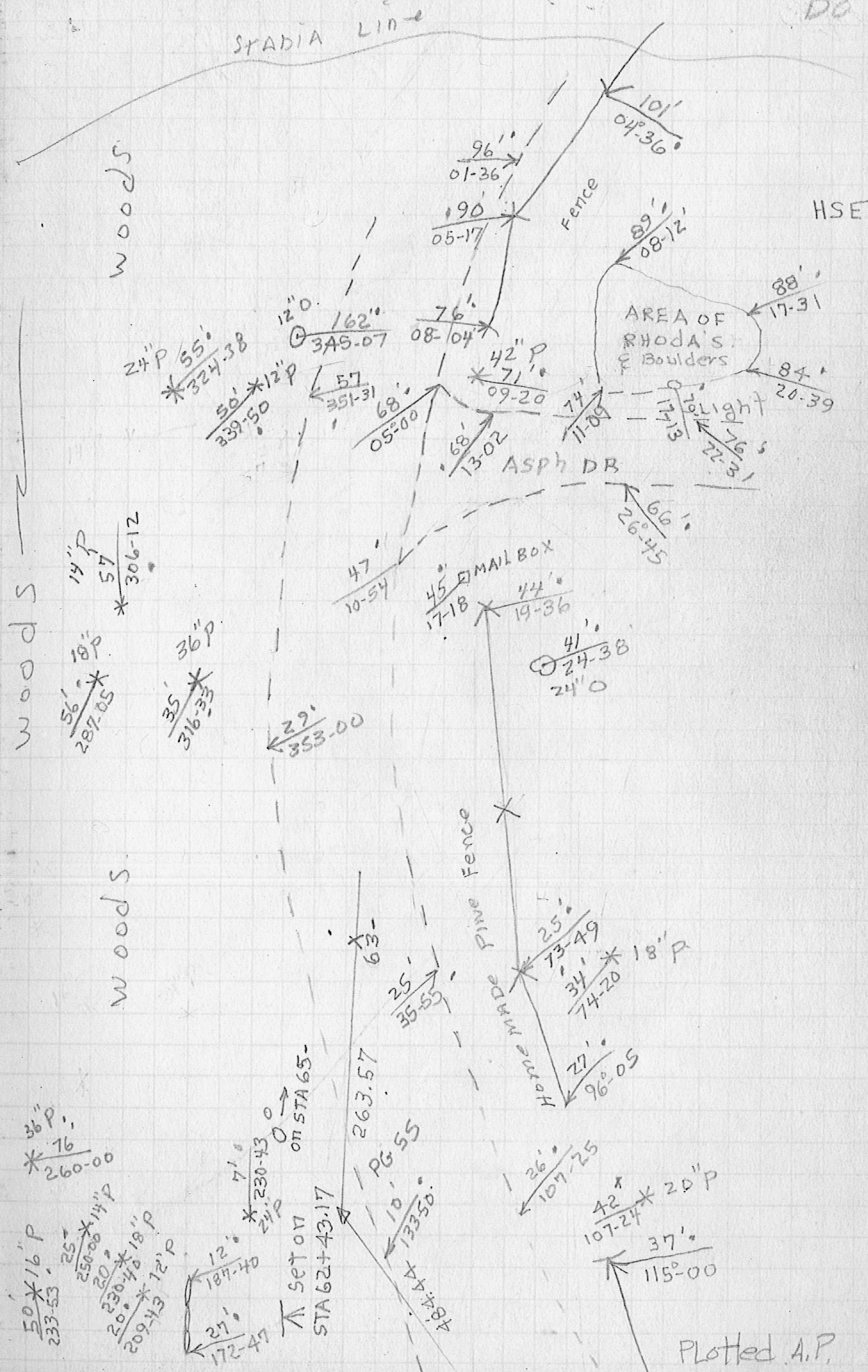
Plotted ES Sep 83

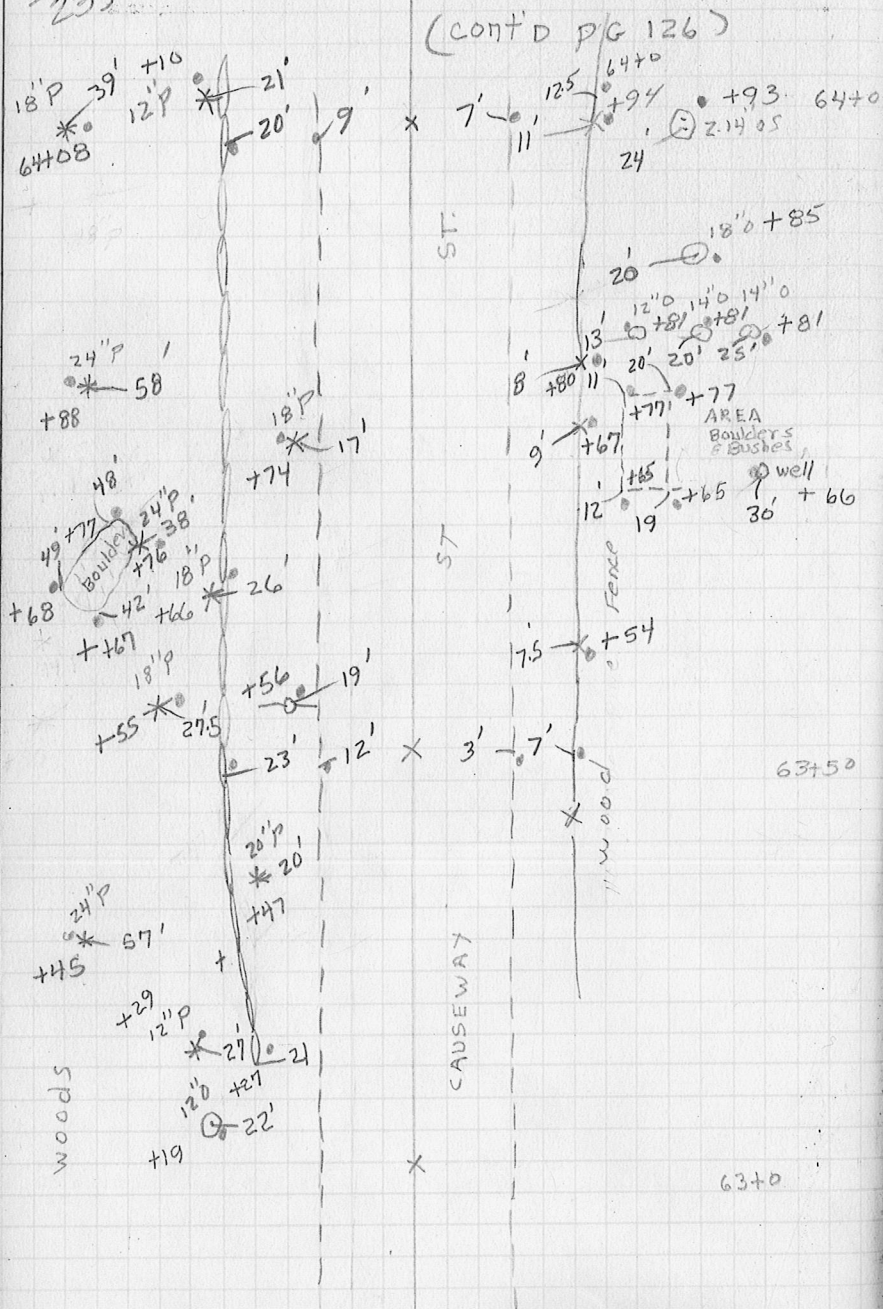
Inst.	Tape	Wthr & Temp.	Date	Crew
120	CAUSEWAY	STREET		



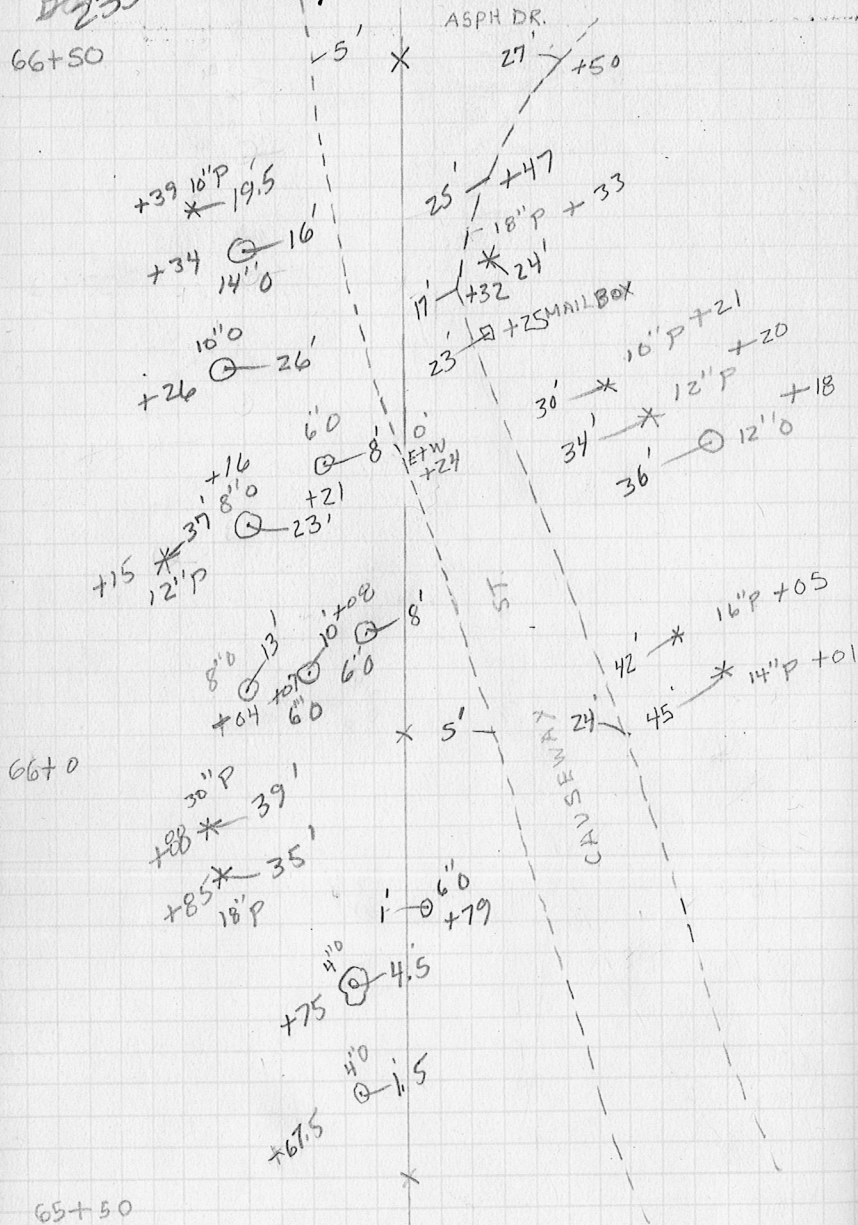
Inst. Tape Wthr & Temp. Date Crew
MEDFIELD DETAIL July 83 121



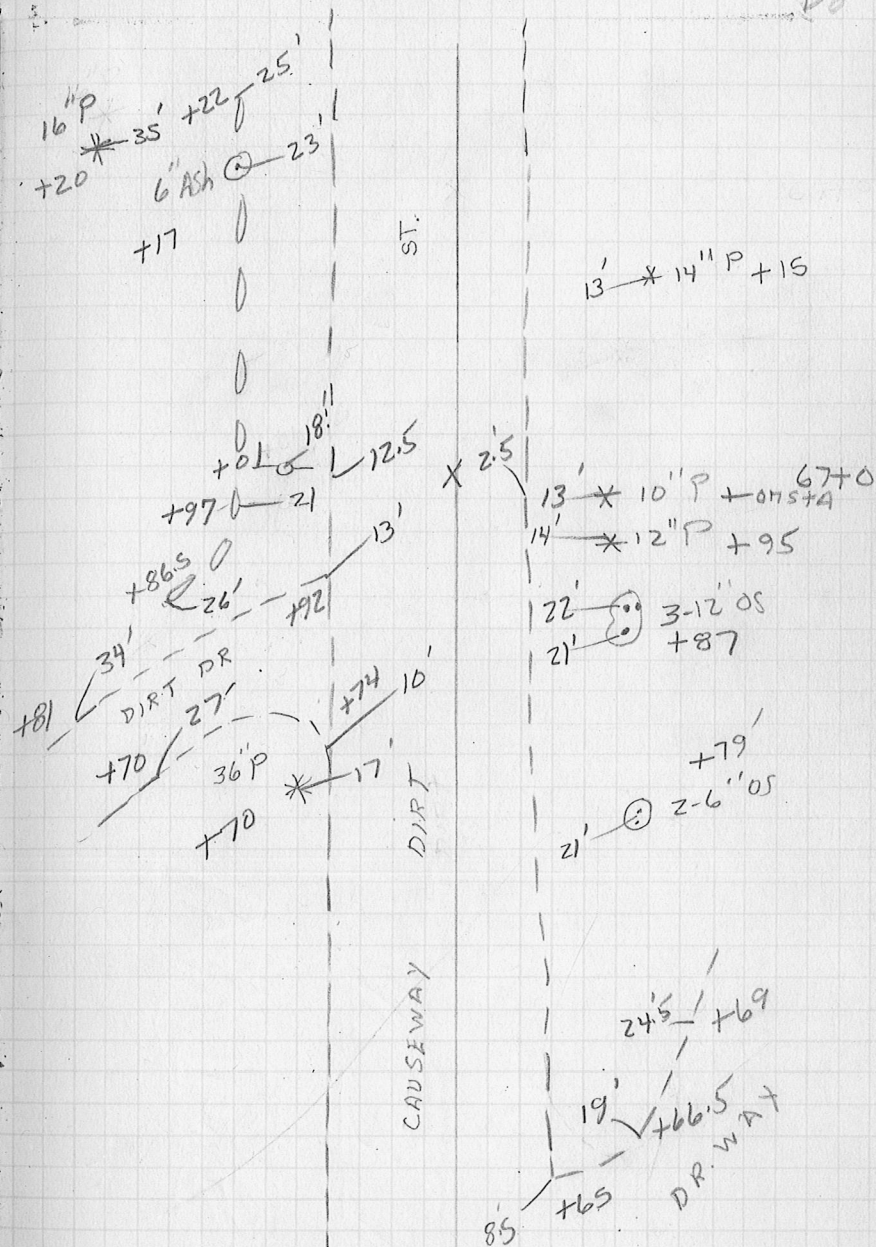




Plotted A.P.



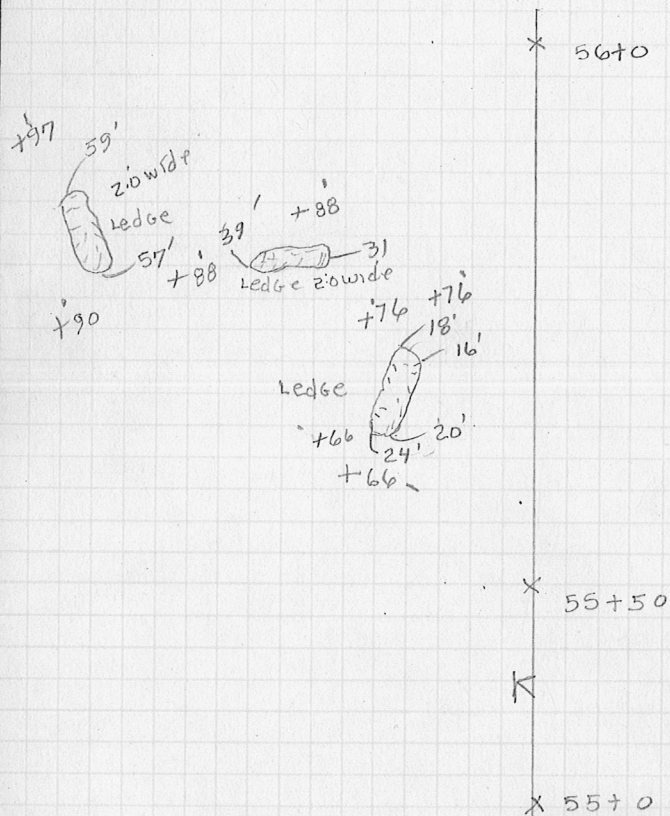
Plotted A.P.



Plotted A.P.

132	Inst.	Tape	Wthr & Temp.	Date	Crew
-----	-------	------	--------------	------	------

233 CAUSEWAY ST. MEDFIELD

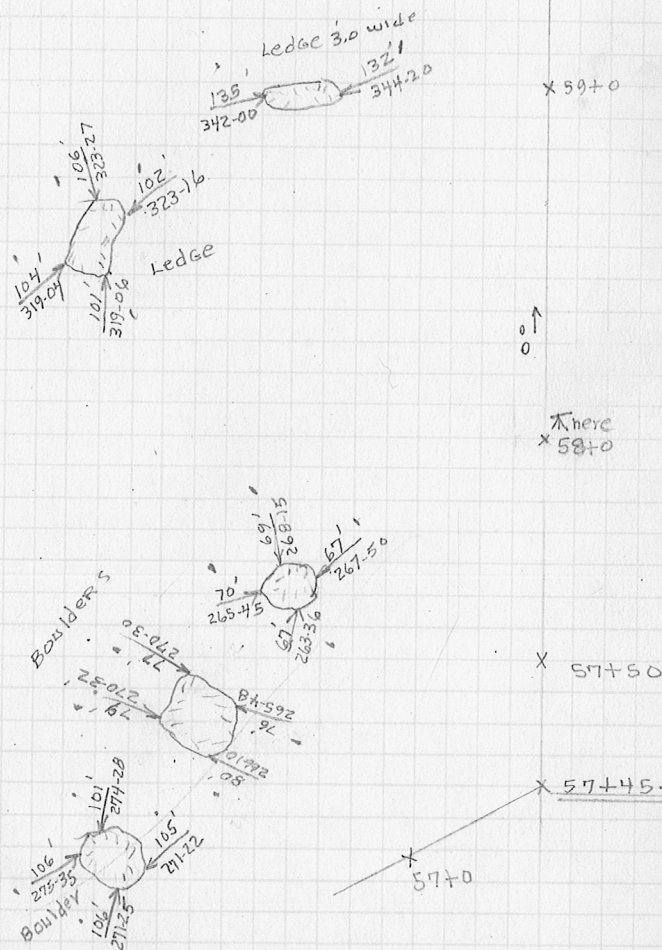


Plotted A.P.

Inst.	Tape	Wthr & Temp.	Date	Crew
				133

LOCATING LEDGE & BOULDERS

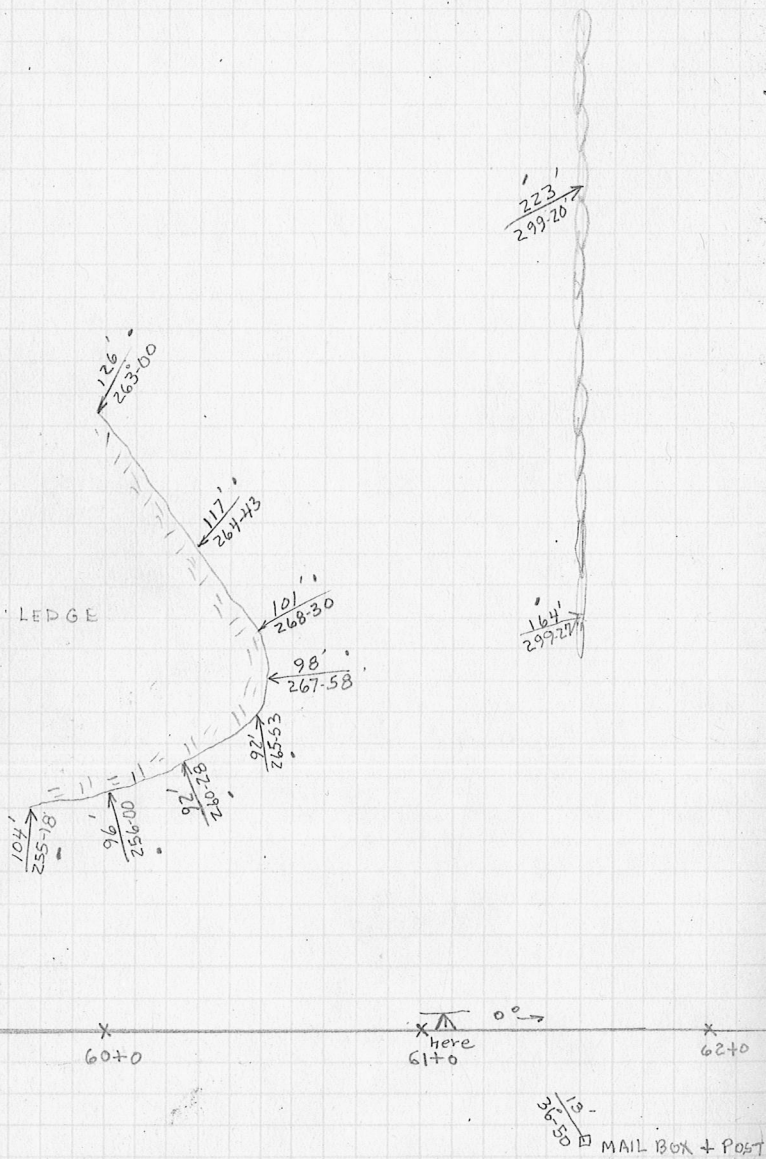
Nov 83



Plotted A.P.

134 Inst. Tape Wthr & Temp. Date Crew
 CAUSEWAY STREET

Inst. Tape Wthr & Temp. Date Crew
 MED FIELD 135



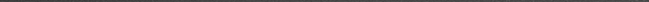
Plotted A.P.

Inst. 138 Tape Wthr & Temp. Date Crew
BENCHMARKS
233

STA & OFFSET	+	H. I.	-	ELEV	ADJ
	9.74	132.75		123.01	
	8.00	139.86	0.89	131.86	
4+08 LT 40'	8.62	145.24	3.24	136.62	
	9.37	154.42	0.19	145.05	
7+43 RT 83'	7.80	155.67	6.56	147.86	147.87
	6.01	159.71	1.97	153.70	
	9.50	169.09	0.16	159.55	159.56
	11.65	179.66	1.04	168.01	
	11.83	190.81	0.68	178.98	
	11.58	201.77	0.62	190.19	190.20
	3.00	198.56	6.21	195.56	195.57
	7.38	199.63	6.31	192.25	192.26
	8.37	207.50	0.50	199.13	
	10.81	215.66	2.65	204.85	204.86
	1.58	205.93	11.31	204.35	
	7.77	206.16	7.54	198.39	
	1.13	202.07	5.22	200.94	200.95
	3.15	195.98	9.24	192.83	
	3.76	194.54	5.20	190.78	190.79
	1.54	186.27	9.81	184.73	184.74
	0.57	175.32	11.52	174.75	
	1.00	164.64	11.68	163.64	
	0.42	161.36	3.70	160.94	160.96
	0.51	150.09	11.78	149.58	
	0.80	142.07	8.82	141.27	141.29
	6.05	142.13	5.99	136.08	
	1.58	139.10	4.61	137.52	137.54
	8.55	145.35	2.30	136.80	136.82
	2.95	138.03	10.27	135.08	
	2.58	133.23	7.38	130.65	130.67
51+14 RT 49.5	6.67	132.58	7.32	125.91	125.93
53+72.5 LT 28'	5.70	133.71	4.57	128.01	128.03
	11.36	141.37	3.70	130.01	
57+55.5 RT 6'	5.43	144.21	2.59	138.78	138.80
60+72.5 RT 183'	5.28	144.83	4.66	139.55	139.57
	3.40	142.06	6.17	138.66	
	5.04	137.96	9.14	132.92	132.95
67+85 LT 74'	9.53	138.66	8.83	129.13	132.16
	0.78	129.24	10.20	128.46	
cont'd (PG 138)			8.46	120.78	120.81

Inst. 137 Tape Wthr & Temp. Date Crew
CAUSEWAY ST. MEDFIELD
PRISCO O'BRIEN
OCT 83

REMARKS
T.B.M. C.S.R. #51 CHIS SQ CONC ABUT. BRIDGE (123.01) NB 229/133
T.P. Stone
B.M. CHIS SQ Ledge (136.62) NB 229/133 (ORCHARD ST)
T.P. Stone
B.M. CHIS SQ BEDSTONE stone wall (147.87) ORCHARD ST NB 229/133
T.P. SELV COR S.B.
B.M. ROC BOT BRICK STEP HSE #252 (CAUSEWAY ST)
T.P. HIGH PT. Stone
T.P. Stone IN STREET
B.M. LOC. BOT BRICK STEP HSE #242
B.M. HORIZ. R.R. SPK 24" Pine (opposite HSE #234)
B.M. CHIS SQ Boulder opposite HSE #222
T.P. Spk Pole #69
B.M. CHIS SQ Ledge outcrop opposite HSE #218
T.P. Stone IN STREET
T.P. Stone IN STREET
B.M. ROC BOT BRICK STEP HSE #200
T.P. Stone IN STREET
B.M. HORIZ. R.R. SPK 18" O APPROX. STA 28+60 RT 25' 99% NLY FROM pole 24" RT 17' OFF WALL
B.M. CHIS SQ Ledge outcrop APPROX. STA 31+55 LT EDGE CANTER
T.P. Stone
T.P. Stone
B.M. CHIS SQ Ledge outcrop APPROX. STA 35+50 LT 17' FROM wall
T.P. Stone
B.M. VERT. R.R. SPK 42" Pine APPROX. STA 38+0 30' RT.
T.P. Stone
B.M. CHIS SQ Boulder APPROX. STA 42+35 RT 20' SWLY Pole 24" RT 25.5' NLY
B.M. HORIZ. R.R. SPK 16" OAK APPROX. STA 44+73 17' RT opposite WALL
T.P. Stone
B.M. CHIS SQ Boulder APPROX. STA 48+10 LT 25.5' FROM wall
B.M. CHIS SQ Boulder
B.M. CHIS SQ Ledge outcrop
T.P. Stone
T.P. CHIS SQ Boulder
B.M. LOC. BOT CONC. STEP HSE #134
T.P. Stone
B.M. CHIS SQ BEDSTONE IN stone wall @ APPROX. STA 65+06 LT.
B.M. VERT. R.R. SPK 24" Pine
T.P. Stone
B.M. VERT. R.R. SPK 24" O APPROX. STA 70+60 RT 25' @ Oak #37



140

ELEVATIONS

Inst.

Tape

CAUSEWAY

Wthr & Temp.

Date

Crew

+6.49

132.42

USE
TRAVERSE STA.

	21	18.5	ETW 18	7	ETW 1	0
50+0	4.3	5.1	4.6	4.2	4.3	4.2
	128.1	127.3	127.8	128.2	128.1	128.2

	21	18	ETW 14	7	ETW 0	0
50+50	4.4	5.2	4.8	4.4	4.6	4.6
	128.0	127.2	127.6	128.0	127.8	

	20	15	8.5	ETW 15	0	0
51+0	6.3	6.0	5.1	4.7	4.7	4.7
	126.1	126.4	127.3	127.7	127.7	

	20	55	ETW 2	0	0	0
51+50	7.6	6.3	5.3	5.2	5.2	5.2
	124.8	126.1	127.1	127.2		

	20	10	6	0	0	0
52+0	7.8	7.8	7.6	5.5	5.5	5.5
	124.6	124.6	124.8	126.9		

	20	15	6	ETW 0	0	0
52+50	8.8	8.4	8.0	5.4	5.4	5.4
	123.6	124.0	124.4	127.0		

+7.65

135.73

STREET

Inst.

Tape

Wthr & Temp.

MEDFIELD

Date

Crew

OCT 83 141

PRISCO
Gen 141

✓ B.M.
125.93 CH19 S9
Boulder
(P6137)
STA 51+14 RT 49.5

	2	5.5	20
	3.8	4.9	6.0
	128.6	127.5	126.4

	2	4.5	15
	4.2	6.1	6.7
	128.2	126.3	125.7

	ETW 6	20
	5.0	5.8
	127.4	126.6

	ETW 6	ETW 14	20
	5.0	5.2	5.6
	127.4	127.2	126.8

	ETW 1	8	16	20
	5.5	5.0	5.3	5.8
	126.9	127.4	127.1	126.6

	ETW 6	ETW 16	20
	4.9	5.3	6.0
	127.5	127.1	126.4

T.P. SPK Pole #34
45

- 4.34 128.08

EK

142

ELEVATIONS CAUSEWAY

233 Inst.

Tape

Wthr & Temp.

Date

Crew

135.73

53+0

20

12'

ETW

0

10.7

9.9

8.4

8.3

125.0

125.8

127.3

127.4

53+50

20

10

ETW

0

9.5

8.3

8.0

8.0

126.2

127.4

127.7

127.7

53+89LT

0 28
0 5.820
6.5

129.9

129.2

Stone Ret wall

STREET

Inst.

Tape

Wthr & Temp.

Date

Crew

MEDFIELD

OCT 83

143

PRISCO
GENITT

ETW

ETW

20

6

14

9.5

8.1

8.6

126.2

ETW

ETW

TOP BNK

BOT

6

14

16

20

8.0

8.5

8.4

10.3

127.7

127.2

127.3

125.4

on

@ wall

ETW

0

15

15

3.5

0

6.6

8.0

8.0

7.9

129.1

127.7

127.7

127.8

54+0

30

20

on

@ wall
16

12

ETW

ETW

ETW

5.5

6.0

6.8

7.2

8.3

7.9

7.8

8.1

130.2

129.7

128.9

128.5

127.4

127.8

127.9

127.6

54+50

75

50

30

on @
22

22

ETW

ETW

ETW

3.3

4.6

4.7

4.6

6.2

7.5

7.3

7.3

132.4

131.1

131.0

131.1

129.5

128.2

128.4

128.4

54+59 LT

30

on @
22.5

22.5

ETW

ETW

ETW

4.8

4.4

6.1

7.3

7.2

7.5

130.9

131.3

129.6

128.4

128.5

128.5

55+0

75

50

20

3.3

5.2

6.0

132.4

130.5

135.11

129.7

ETW

ETW

ETW

12

5

3.5

6.9

6.6

6.9

128.8

129.1

129.0

-7.70

128.03

BM. CH15 59 Ledge

(128.03) PG 137

-2.37

133.34

T.P. STONE STA 53+72.5 LT 28

VEK

+7.68

+9.11

142.45

144

ELEVATIONS

CAUSEWAY

233 Inst. Tape Wthr & Temp. Date Crew

142.45

	75	50	30	Top	10	ETW	0
55+50	6.9	10.3	10.7	10.9	12.4	12.8	12.7
	135.6	132.2	131.8	131.6	130.1	129.7	129.8

	75	50	30
56+0	2.9	7.0	10.3
	139.6	135.5	132.2

	75	50	30	Top	10	ETW	0
56+50	+2.3	2.6	6.6	8.1			
	144.8	139.9	135.9	133.7			

	75	50	Top	Bot BNK	ETW	0
57+0	+1.0	1.7	3.8	9.2	9.3	9.1
	143.5	140.8	138.7	133.3	133.2	133.4

57+39.5 LT

	Inter DR	Inter DR @ ETW
	14.5	18
	7.5	7.5
	135.0	135.0

	DIRT DR
	0
	8.1
	134.4

+10.03

148.83

SKIP 57+50

	50	Top	Bot BNK	ETW
58+0	7.3	9.0	12.1	
	141.5	139.8	136.7	

STREET

MEDFIELD

145

Inst. Tape Wthr & Temp. Date Crew

	ETW	ETW
	2	8
	12.6	12.8
	129.9	129.7

	Top BNK	ETW	ETW	ETW
	10	0	7.5	15
	10.6	12.2	11.9	12.2
	131.9	130.3	130.6	130.3

	Bot BNK	ETW	ETW	ETW
	4.5	0	0.5	15
	10.6	11.1	11.1	10.6
	131.9	131.4	131.4	131.9

	ETW
	4
	9.1
	132.9

- 3.65

138.80

T.R. Chis Sq Boulder
(128.80) PG 137

✓ EK

146

233

ELEVATIONS

Inst.	Tape	Wthr & Temp.	CAUSEWAY Date	STREET Crow
-------	------	--------------	---------------	-------------

148.83

58+50

100	75	50	30	5
+2.5	2.0	7.0	9.2	9.3
151.3	146.8	141.8	139.6	139.5

59+0

75	50	34	8
+2.0	5.1	8.8	9.6
150.8	143.7	140.0	139.2

Bot Slope

59+50

@ ledge

69.5	50	30	10
+1.6	3.9	7.5	8.9
150.5	144.9	141.3	139.4

+4.77

145.33

+9.71

149.28

60+0

50	30	13	7	3.5
0.1	4.5	5.7	8.1	8.1
149.2	144.8	143.6	141.2	141.2

Top

BOT BNK

ETW

147

MEDFIELD

Inst.	Tape	Wthr & Temp.	Date	Crow
-------	------	--------------	------	------

0	ETW	ETW	ETW
10.3	3	9	18
138.5	10.8	10.6	10.8
	138.0	138.2	138.0

0	ETW	ETW	ETW
10.8	2	10	18
138.0	10.4	10.0	10.3
	138.4	138.8	138.5

0	ETW	ETW	ETW
9.4	2	7.5	18
139.4	9.3	8.9	9.0
	139.5	139.9	139.8

- 8.27 140.56 T.P. HIGH PT. STONE

- 5.76 139.57

B.M. LOC. BOT CONC STEP
HSE #134 (139.57) PG 137

EK

ELEVATIONS
233 Inst. Tape Wthr & Temp. Date Causeway Crew

149.28

^

60+27 RT

E EDGE DR.

O ETW

0
8.1
141.2

ETW
8
8.7
140.6

ETW
2
8.2
141.1

60+50

75 50 36 12
4.9 9.3 9.9 9.2
144.4 140.0 139.4 140.1

ETW
8
8.7
140.6

ETW
0
8.4
140.9

61+0 @ Edge

100 75 50 30 16
8.0 8.6 10.1 9.9 9.9
141.3 140.7 139.2 139.4 139.4

ETW
12
9.3
140.0

ETW
3
9.0
140.3

61+22.5 RT

E EDGE DR.

O ETW

0
9.4
139.9

@ DR.
ETW
4.5
9.7
139.6

61+50

100 75 50 30 16
8.9 9.3 11.1 10.2 10.3
140.4 140.0 138.2 139.1 139.0

ETW
13
9.8
139.5

ETW
3
9.6
139.7

62+0

100 75 50 30 9
9.4 10.4 10.4 10.5 10.6
139.9 138.9 138.9 138.8 138.7

ETW
5.5
10.2
139.3

ETW
3.5
10.2
139.1

Inst. Tape Wthr & Temp. Date Crew

O DR.

ETW

10

8.6

140.7

ETW

8

8.9

140.4

ETW

5

9.2

140.1 139.8

ETW

5.5

9.6

139.7 139.4

ETW

3.5

10.0

139.3 139.3

ETW

12.5

10.2

139.1

233 ELEVATIONS
Inst. Tape Wthr & Temp.

CAUSEWAY
Date Crew

149.28

+3.66

143.90

62+50

75	50	30	8
7.5	6.7	6.4	5.0
136.4	137.2	137.5	138.9

0	ETW	ETW	ETW
2.5	2.5	10	18
6.0	5.6	5.2	5.1
137.9	138.3	138.7	138.8

- 9.04 140.24 T.P. Stone

63+0

75	50	30	23	18	11	8	ETW
12.0	10.5	8.8	7.9	5.3	6.3	6.0	6.0
131.9	133.4	135.1	136.0	138.6	137.6	137.9	137.9

ETW	ETW	ETW
0	0	7
5.4	5.30	5.30
138.5	138.6	138.6

63+50

50	30	27	13	15	11.5	4	ETW
13.1	10.6	7.6	5.6	6.6	6.2	5.5	5.5
130.8	133.3	136.3	138.3	137.3	137.7	138.4	138.4

0	ETW	ETW
5.3	3.5	5.1
138.6	138.6	138.8

64+0

50	30	20	13	9	7	1	0	ETW
11.6	8.6	7.3	5.6	6.2	5.9	5.2	5.2	4.9
132.3	135.3	136.6	138.3	137.7	138.0	138.7	138.7	139.0

64+50

50	30	13	0	ETW	ETW	ETW
7.0	5.7	4.0	6.3	5.8	5.3	5.2
136.9	138.2	139.9	137.6	138.1	138.6	138.7

STREET
Inst. Tape Wthr & Temp. MEDFIELD
Date Crew

152

233

ELEVATIONS

Inst.

Tape

Wthr & Temp.

CAUSEWAY

Date

Crew

143.90

X

65+0 LT side only

50
9.830
5.723
3.9

134.1

138.2

140.0

Slope

BOT

13
6.8

137.1

0
7.2

136.7

+1.84

139.66

X

+9.73

142.68

X

-6.68 137.22 T.P. Stone

-6.11

132.95

B.M. Chissg
Bedstone
PG-137
(132.95)65+20 LT
ASK BACK
C D WIGHT ST50
10.830
8.920
8.210
7.40
6.710
6.120
5.630
5.040
4.450
4.4

65+50 RT

BOT
Slope
0
6.810
5.819
5.430
4.7

BOT BANK

40
4.8

66+0 RT

0
5.13
5.17
5.515
5.1

BOT BANK

24
5.166+31 RT
ASK AHEAD
C ASPH DR.0
5.810
5.521
5.726
5.8540
4.6550
3.18

153

NOV 83
Crew SEP
1984

EK

154 ELEVATIONS CAUSEWAY

Inst. - Tape Wthr & Temp. Date Crew

233

142.68

66+50

woods

ETW
5 0
6.2 5.9

66+89 LT 0.7 DR.
ASK BACK 40 20 15 14 ETW 11 ETW 4 0
DIRT DR. 9.1 7.6 6.9 7.1 6.7 6.4 6.4

67+0

ETW ETW BOT BANK ETW
13 5 0 3
7.1 6.6 6.7 6.7

67+50

ETW ETW BOT BANK ETW
16 8 1.5 0
7.9 7.5 7.5 7.2

+1.73

138.56

68+0

ET.W. ET.W. ETW.
16 8 0.5 0
4.5 4.1 4.0 4.0

PROFILE

68+50

ETW
5 0
4.9

69+0

STREET

Inst. Tape Wthr & Temp. Date Crew

#3

ROD

CLEAR 70°

SEPT 84

PRISCO
GENITH
SLY

155

ETW ETW on ASPH BACK EDGE
5 12 16 27
5.6 5.8 6.75 5.64

- 5.85 136.83 T.P. HIGH PT STONE

ETW
0
7.1

69+50

0

ETW
4
10.2

156

ELEVATIONS CAUSEWAY

Inst.

Tape

Wthr & Temp.

Date

Crew

233

+ 1.19

138.56

128.62

STREET

Inst.

Tape

Wthr & Temp.

Date

Crew

#3

ROD

CLEAR 70°

SEPT 84

157

PRISCO
GENITTI
SLY

- 11.13

127.43

T. P. STONE

- 7.81

120.81

B.M. VERT R.R. SPK 24" O
(PG 137) APPROX STA 70+60

(120.81)

158 WALL LOCATIONS

Inst. Tape Wthr & Temp. Date Crew

233

D.H.
SET

112.84
10-48-40

97.46
14-13-00

D.H.
SET

86.77
15-22-25

D.H.
SET

20.62
46-30-30

359.10
369.93

387.31

SPK
PG 54

53+75.41

T 28°

96.41
16.46
112.87
.03
112.84

10-48-40
21-37-20
10-48-40

13-16-00
26-32-00
13-16-06

CAUSEWAY ST. MED FIELD

Inst. Tape VI Wthr & Temp. Date

FLURRIES 28° JAN 29

Crew 159

PRISCO
LEONE
CAREW
CROWLEY

57+45.34

SPK
PG 98

57.84
15-21-50

T 28°

97.46
56.89
154.35
.04
154.31

46-21-00
92-42-00

30.51
46-21-00

271.31

0
0

SPK

154.31

SPK PG 55

62+43.17

31.97
122-31-10

122-31-20
245-03-20
122-31-10

END OF

F.B. 233

52