

WILLIAM C. C. C. C.
INCORPORATED 1887

168

8336
5219
COUNTY ENGINEER
REG. DEEDS BLDG.
DEDHAM, MASS.

F.B. 168

COUNTY OF NORFOLK
ENGINEERING DEPT.
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O.U.7

Inst.

Tape

Wthr & Temp.

Date

Crew

1

168

2/168

LOVERING ST.

MEDWAY

Survey Traverse

16 Jan. 1951

3

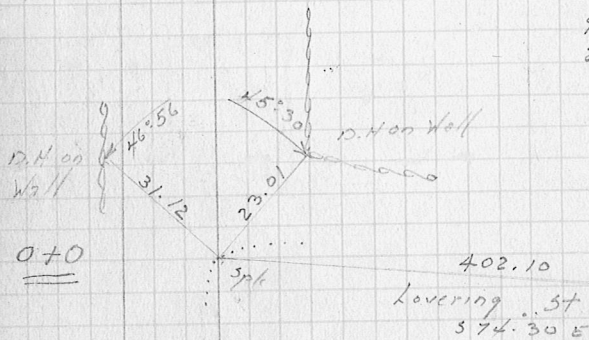
Cold Spring

(132-32)

S.B. 40.00 S.B.

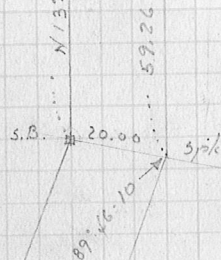
Summer St.

712.32 Plan



0+0

N 13:15 E

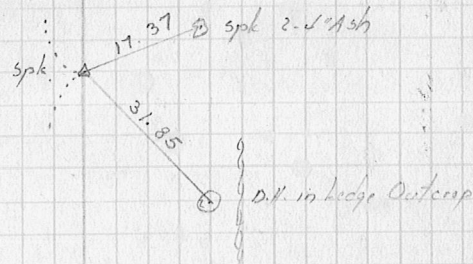


402.18
+ .08
402.10

737.62
- 0.12
737.50

737.50

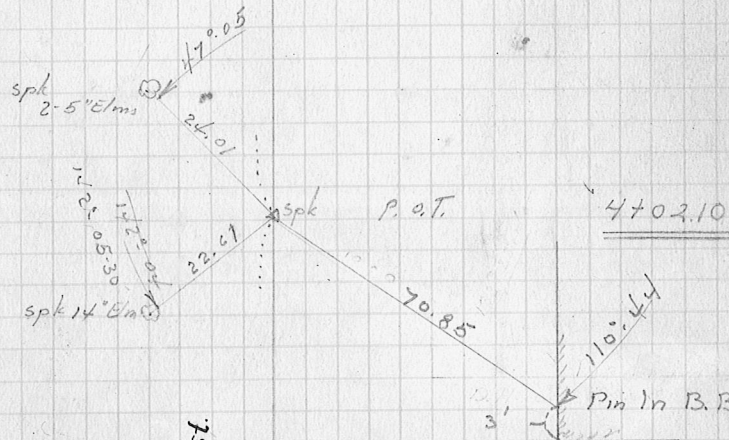
9+67.42 P.O.T.



565.43
- .11
565.32

565.32

402.10
565.32
967.42
737.50
1704.92



Lovering St.

402.10

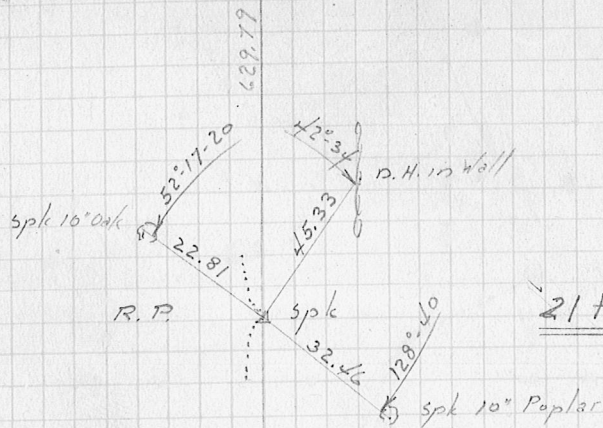
4/168 LOVERING ST.

MEDWAY

Survey B

Jan 1951 5

629.91
.12
629.79



21+64.96

460.13
.09
460.04

Lovering St.

460.04

spk 10" Willow

52°17'20"
52°17'20"
52°17'20"
52°17'20"

(SYN 1950)

spk. P.O.T.

17+04.92

D.H. in Conc. Header

22.42

-737.50

D.H. in Conc. Header

278.63
.03
278.60

31+58.88

D.H. in Wall

D.H. in Boulder

71°58'

162°05'

278.60
N 81°45'E

9.68

17.59

30.62

166°19'
138°57'30"
166°19'10"

364.20
.07
364.13

142°21'-40"
67°05'
142°21'-40"

D.H. in Wall

D.H. in Large Boulder in Wall

48°51'40"

121°11'

39.27

53.06

364.13
66°45'E

52°40'

32.14

34.1

spk 14" Oak

27+94.75

629.79
57°30'E

Lovering St.

Jan. 1951

Survey B

MEDWAY

LOVERING ST.

6/168

D.H. in
Stone Wall

126.89

27.56

spl. P.O.T.

40+17.09

23.60

25.15

spl 10" Birch

spl 16" M

689.34
1.13
689.21

Lovering St.

344.15

579.72
0.11
579.61

515.54
0.10
515.44 (1951)

515.46
0.07
515.39 (1953)

Lovering St.

354.30 E

515.37

579.61

D.H. in
Flat Boulder

34.54

31.79

D.H. in
Cone. Wall

138.23

15.79

spl

34+37.48

125° 34'-30
16° 43
125° 34'-20

(1964)

72.10

72.14

219° 35'-20

spl 20" Ash

278.50

spl 36" oak

170° 13'-20
150° 39'-40
170° 13'-13

13° 14'-40 spl 16" Ash

59.19

Winthrop St.

47+06.90

37.07

spl

89° 13'-40

spl 36" oak

Lovering St.

689.21

8/ LOVERING St

MEDWAY

Survey B

Jan. 1951 9

1/100

752.12
+ .11
752.01 (1951)

752.04
+ .09
751.95 (1953)

350.15 E
751.95

spl 36° oak 7.32 spl D.O.T. 57+68.10

D.H. ledge outcrop 23.18 22.02 D.H. ledge outcrop

546.44
+ .08
546.36 (1951)

96.60
449.76
546.36
+ .06
546.30 Apr 1953

Lovering St.
546.30

30° 09' 24" A

52+21.74

142° 21' 24" A 22.37 17.57 121° 02' 16" A 515.37

176° 11-10
168° 33-20
176° 11-07

Lovering St.

119° 15' 1089.70

67+57.99

R.P. spl N.B. 167 P. ✓

237.88

D.H. in Boulder

37° 54' 13.68

65+20.11

121° 01-20
3° 04'
121° 01-20

spl 36° oak 12.07 211° 38' 30" 8° 08' 151.95

10 LOVERING St

MEDWAY

Survey B

Jan. 1951 11

168

Pond St.

Lovering St.

454.52

696.50

Maple St.

144.48

spk N.B. 167 P.3

88768.03

95°01

N 9°15 E
1020.34

78747.69

P.O.T.

spk N.B. 147 P.3

1089.70

537.73

93722.55

P.O.T.

spk N.B. 147 P.3

S 75°15 E
Lovering St.

454.52

12 LOVERING St.

MEDWAY

Survey B

18 Jan. 1951 13

168

920.31
0.11
920.20

103+20.55

460.32
0.05
460.27

Lovering St.

R.P.

53173

460.27

576°E

920.20

50°02'

spl 12° oak

28.69

179°23-50
178°10-40
179°23-33
(4.50/3)

32.01

spl 4-8° oak

14°15-40

69°39-20

spl 12° Pine 43.55 spl

Holliston

sec N.B. 171
P. 3

702.90
0.08
702.82

112+40.75

576°E

920.20

702.82

23.09

spl 12° Pine

48.71

spl. P.O.T.

21.07

spl 20° M

115°52-20

D.H. in
stone wall

132°47-30

32.58

spl N.B. 171 P. 3

39.51

spl 24° E/m

135°27-40

119+43.57

517.56

55.84

90°18-20

D.H. in
stone wall

30°29'

174°15-10

43°14-20

31.80

6 B Rim

X Cut

sec N.B. 171
P. 3

st

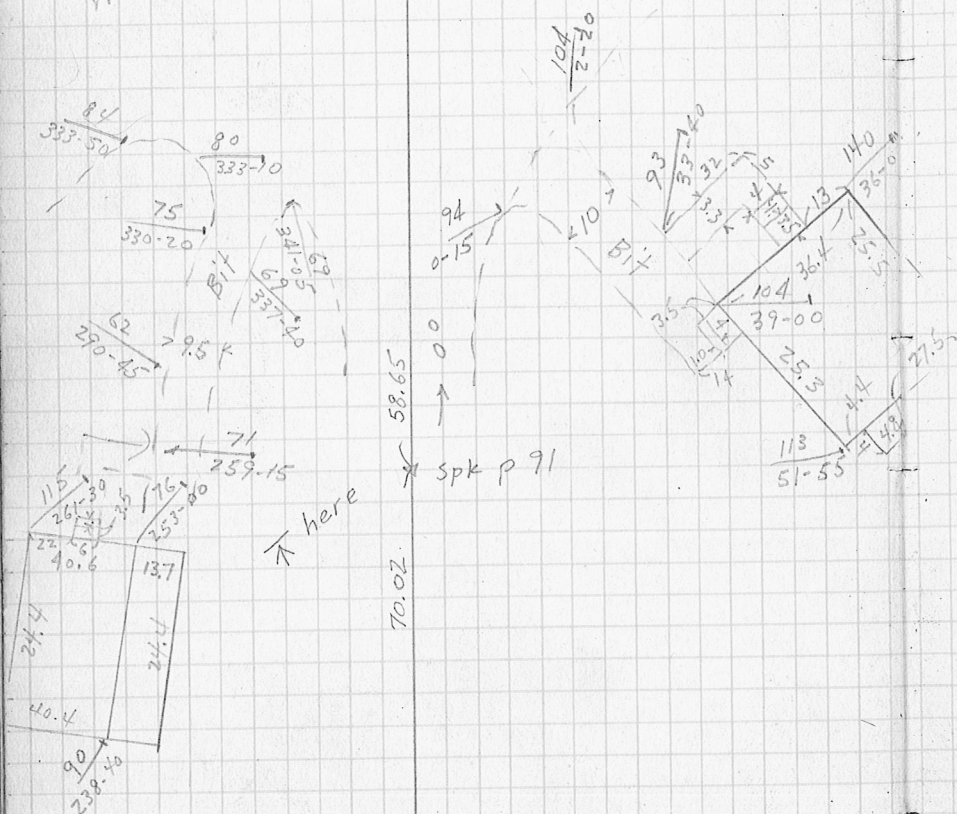
$$\frac{14}{168}$$

MEDWAY

June 18, 1962 15

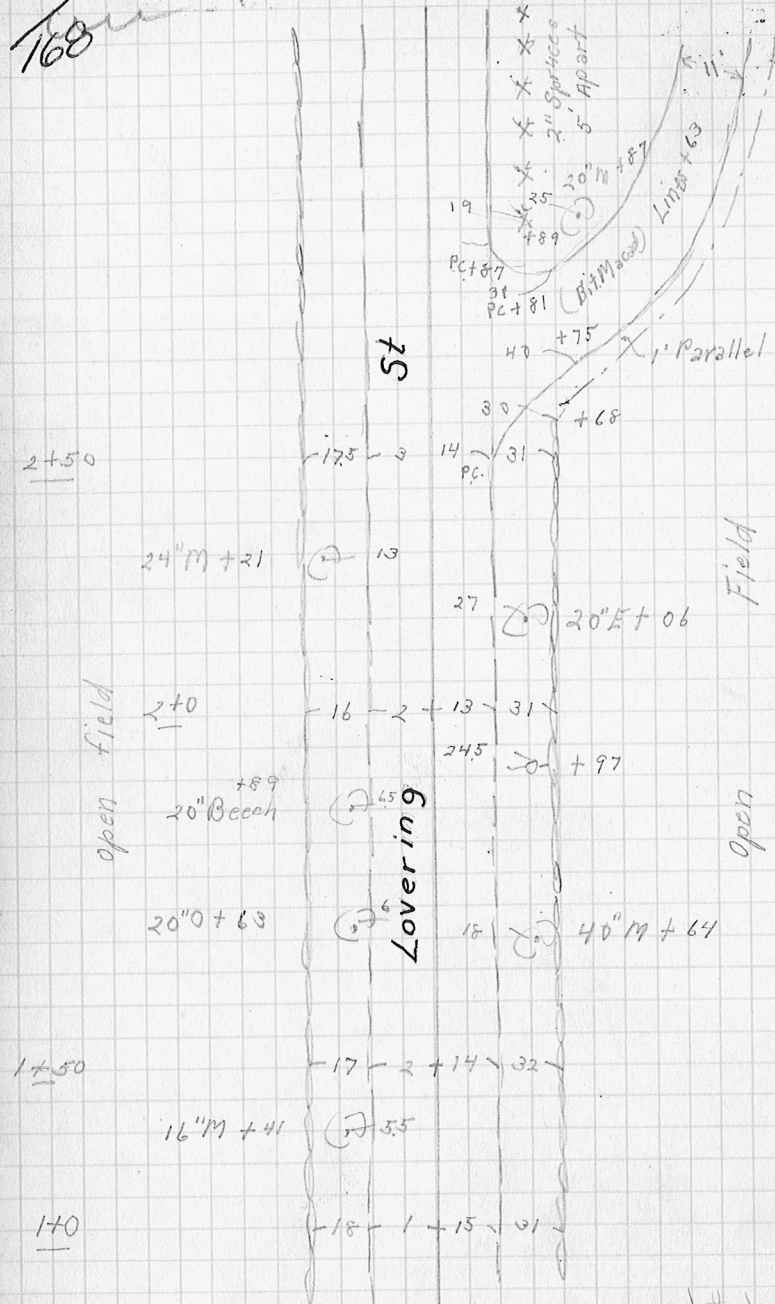
ST.

WINTHROP



Plotted

168



(See Summer St Plot)

Jan 22, 1951

Bitter Cold

Fekkes
Bowser
Strum

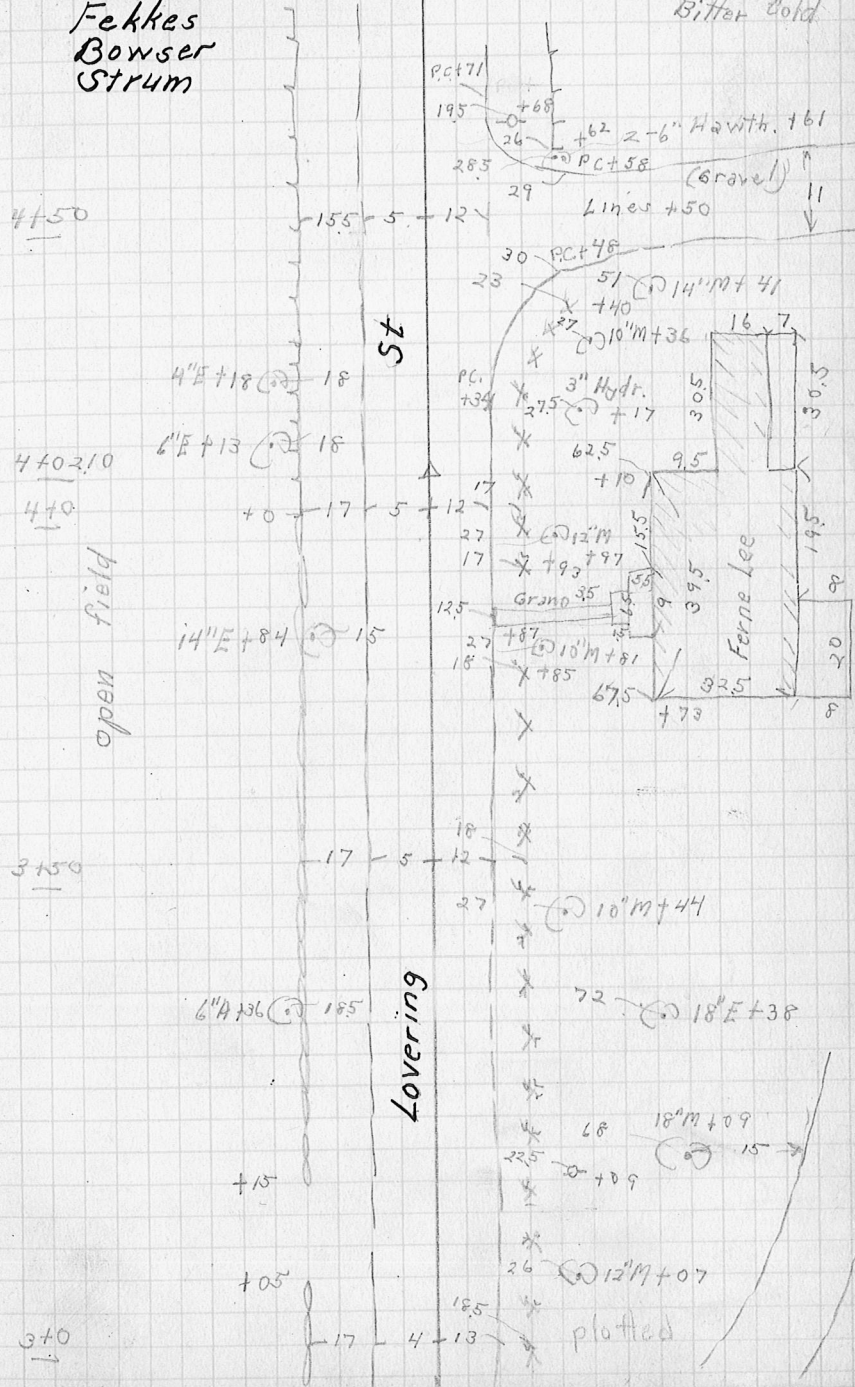
4+50

4+02.10

4+10

3+50

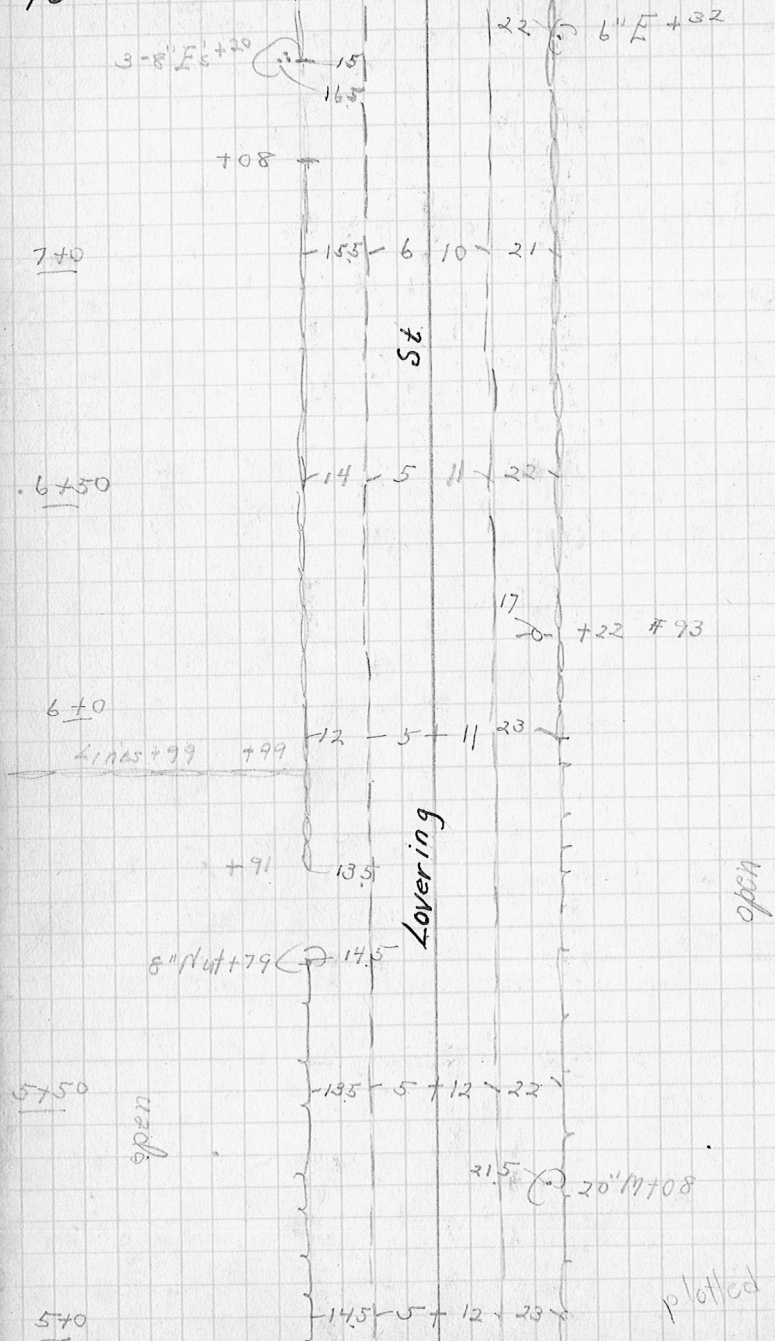
3+0



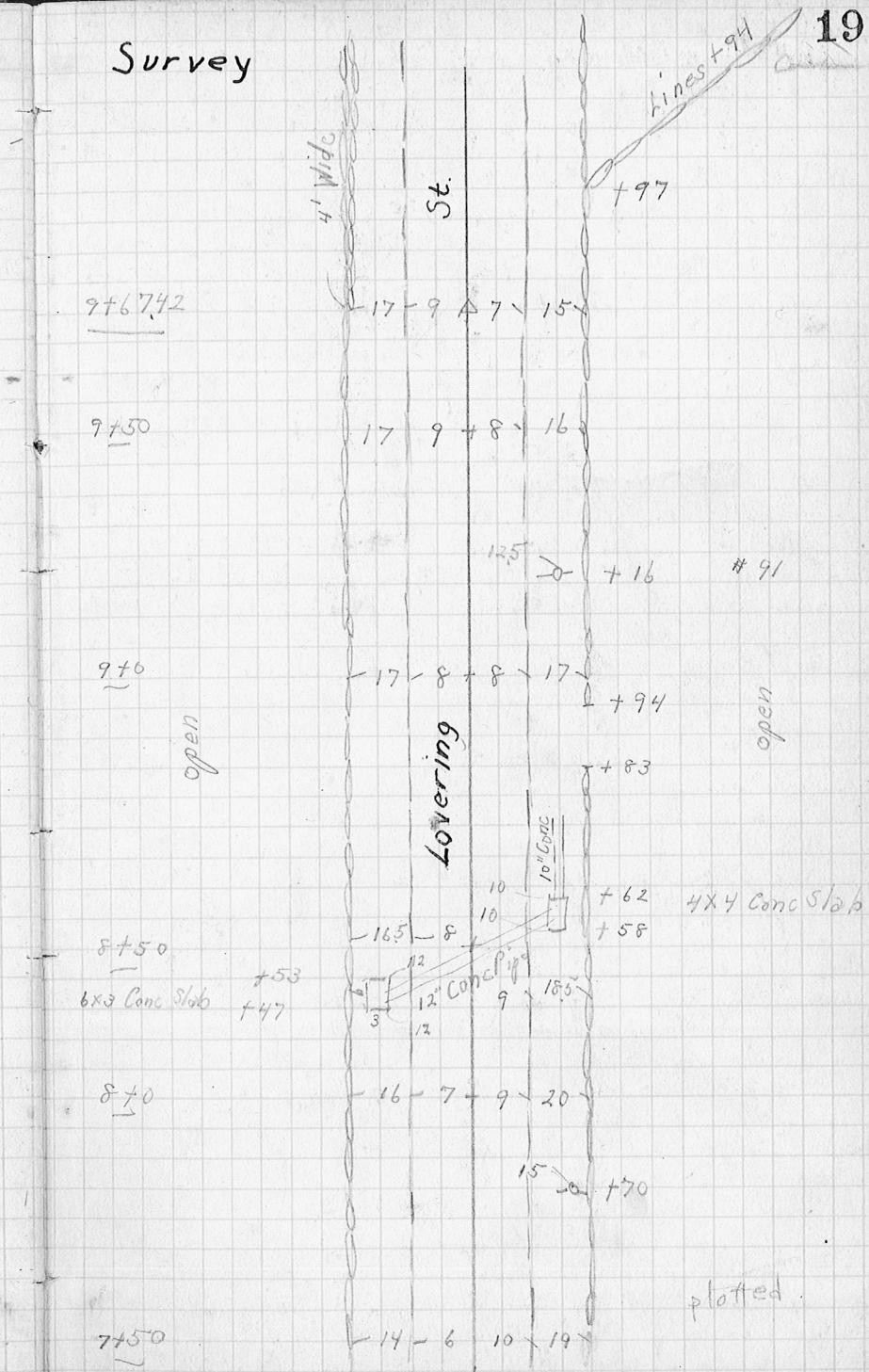
plotted

18/168

Lovering St. Medway



Survey



20 Loring

Medway

6

+76 conc slab 3x6

+70

3x5.5

conc slab over drain

+66

+61

16

15.5

12+50

24-14-3-16

36 10" Ap + 34

St.

7

+13 #89

12+0

23-14-3-16

37 12" Ap + 74

11+50

22-12-5-16

19 6" E + 42

4" wide

11+0

open

21-12-6-17

37 14" Ap + 12

orchard

Loring

10

+61

47/90

10+50

18.5-10-7-17

37 12" Ap + 50

11

End 10" Conc Pipe + 38

+08

10+0

+99

17-10-7-17.5

plotted

Survey

15+0

14+50

14+0

open

13+50

Lines + 24 + 16

+06

13+0

St.

Loring

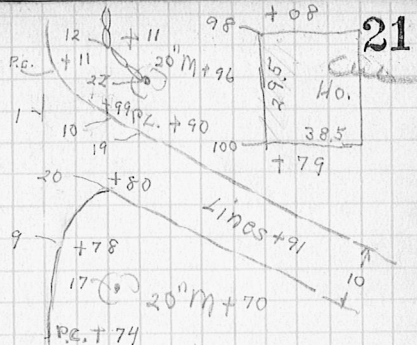
21-15-1

21.5-15-1

22-15-1

23-16-1

24-14-2-16



6 -0 +56

17 10" M + 37

17 12" M + 98

17 14" N 47 + 63

450 + 64

PC + 57

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

16 PC + 48

17 PC + 48

67 14" Ap + 28

37 14" Ap + 25

plotted

65 12" Ap + 72

open

22

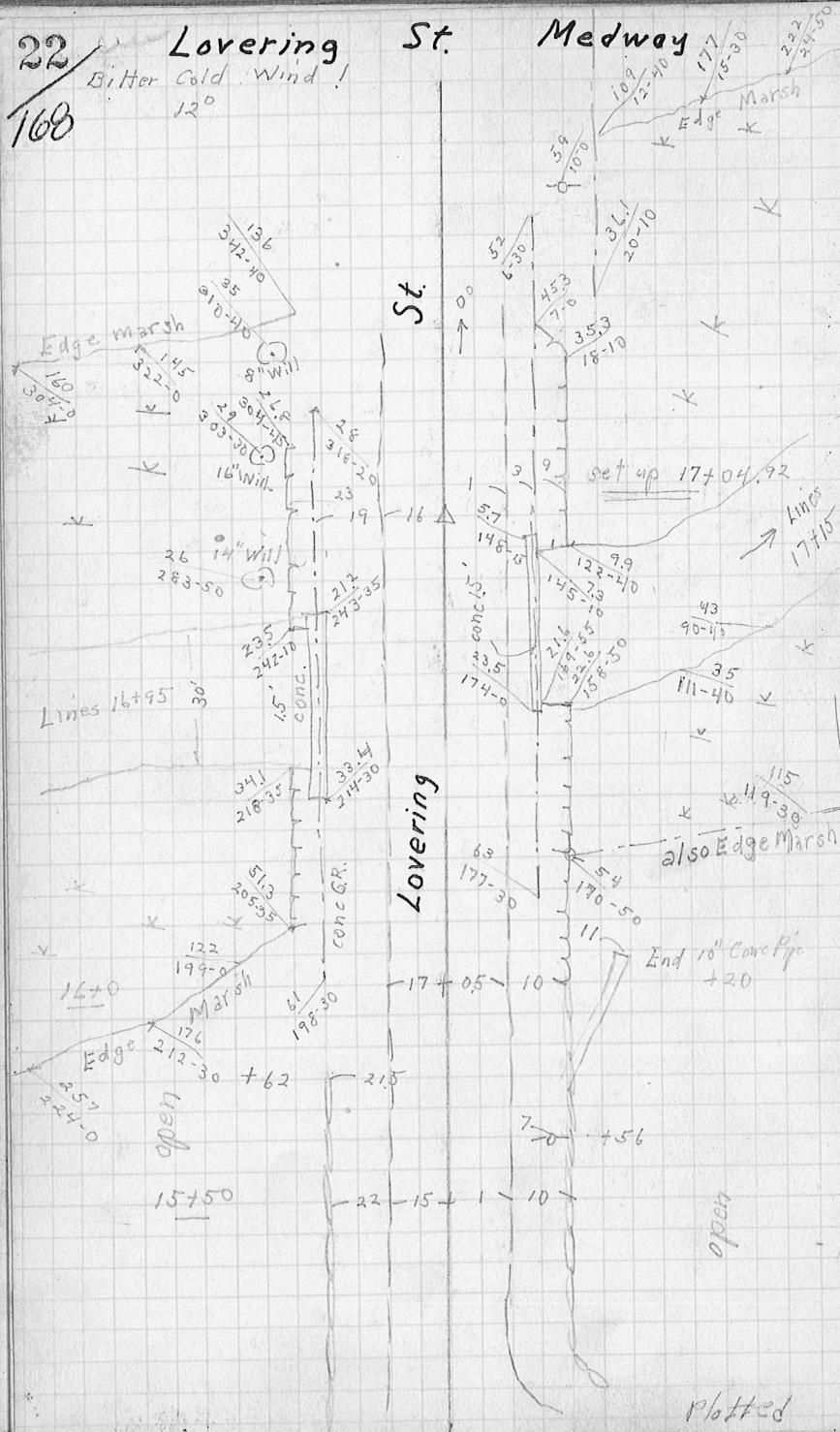
Lovering St.

Medway

Bitter Cold Wind!

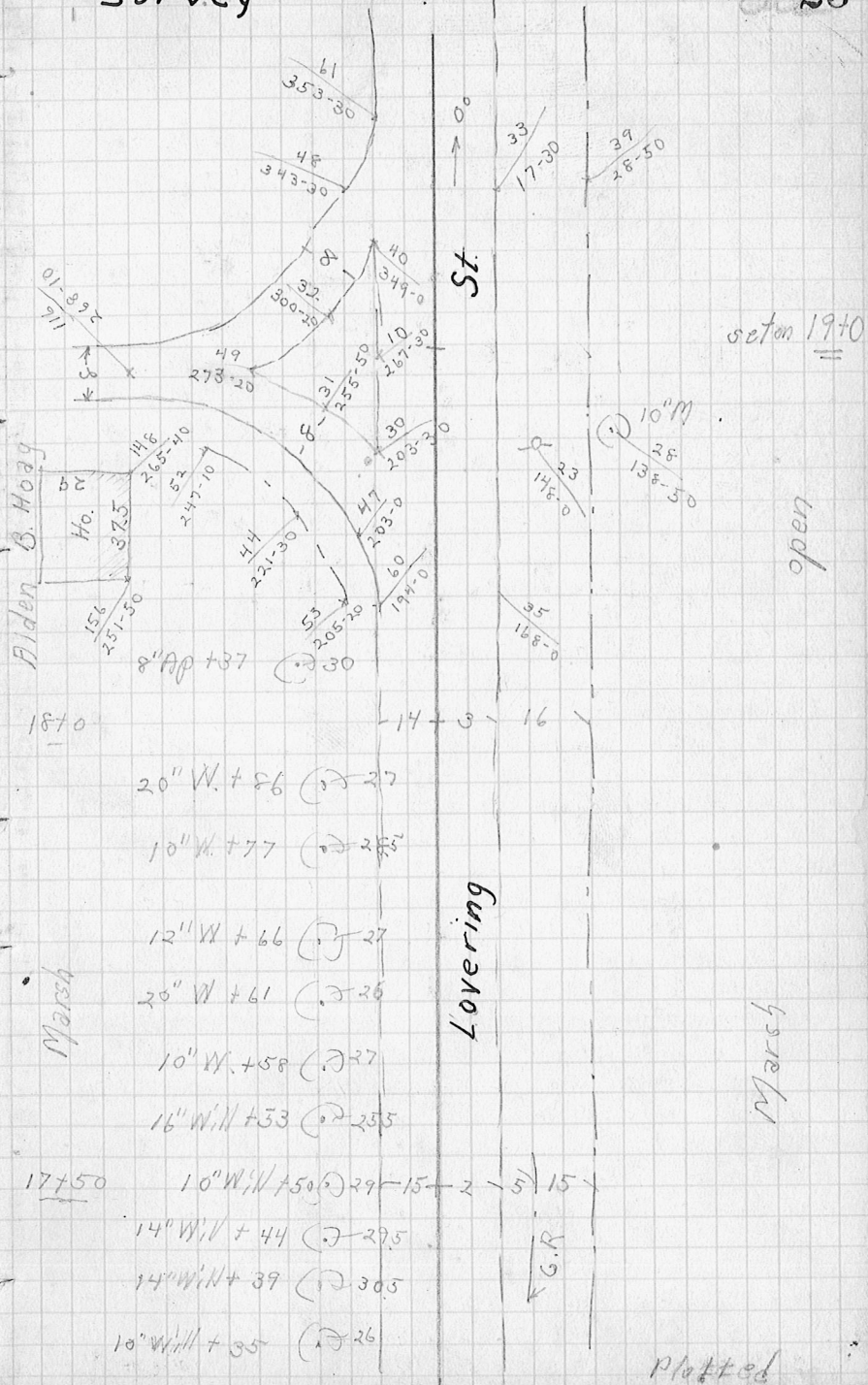
12°

168



Survey

23



28/160

Lovering St. Medway

31+58.88

31+50

31+0

30+50

30+0

29+50

29+0

St.

Lovering

Plotted

cut.

open field

Survey

Masonry Fieldstone

Wall 15 wide

29

Lines +72

33+50

20"A+48

33+0

30"A+85

47/70 +79

20"A+75

14"A+60

32+50

14"A+39

32+0

St.

Lovering

Plotted

14 3-22" A +69

PC+46

85 +43

8 PC

+25

+20 PC

+04

4

4

25

20"A+99

3

20"A+85

115

+63

72.5

+65

31

74

14.5

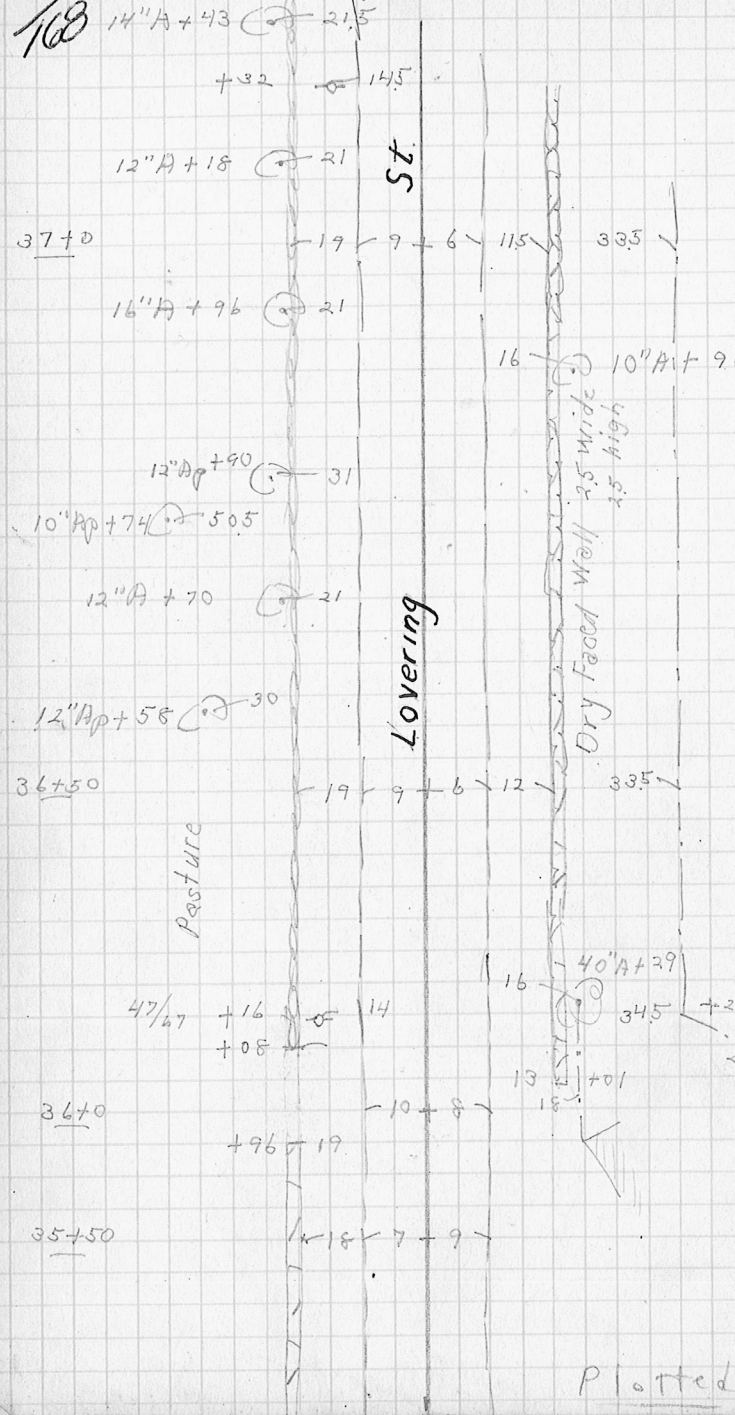
5.5

Shel

92

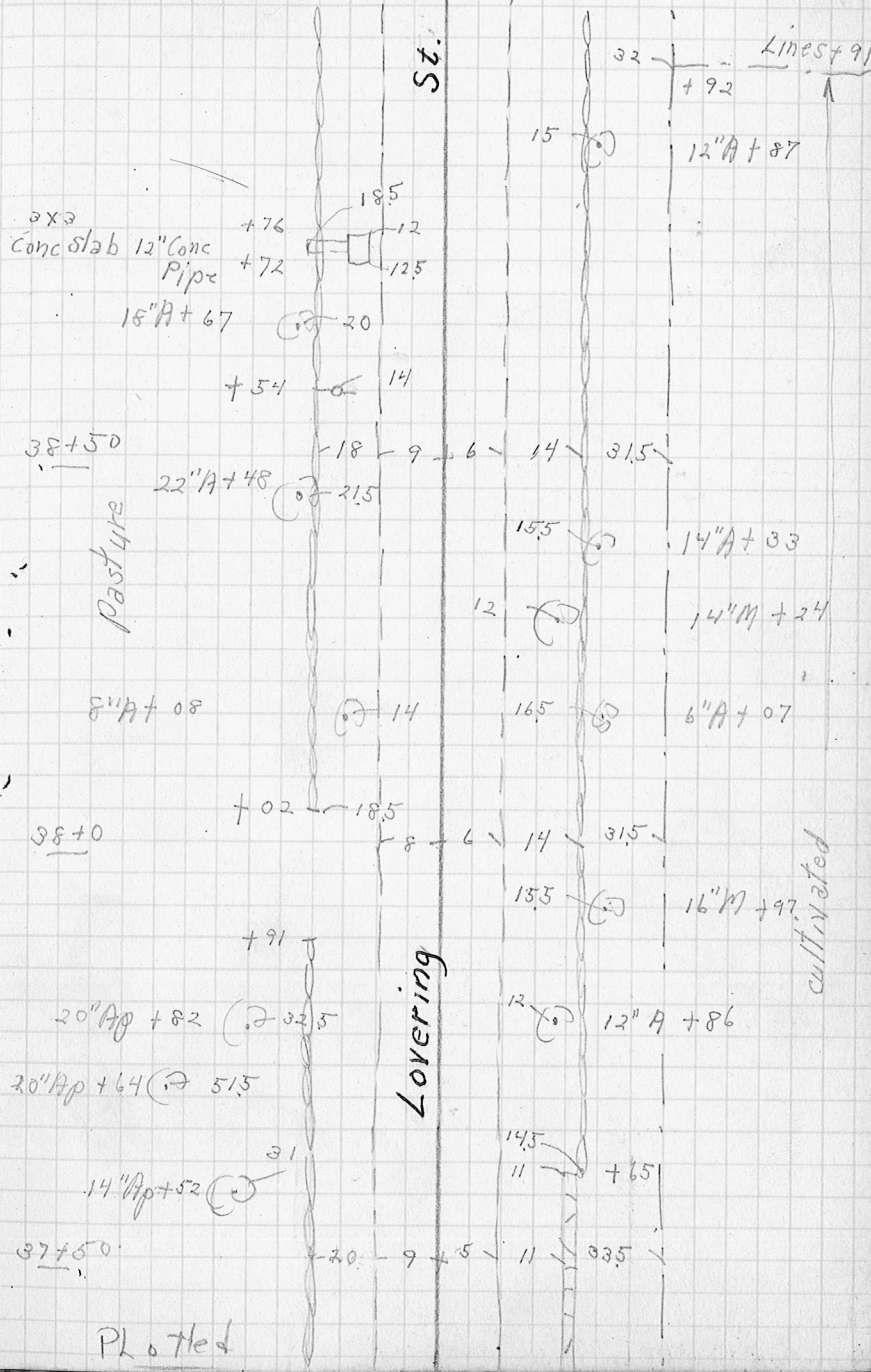
cultivated

32/100 *Lovering St. Medway.*



Survey

33



34
168

Lovering St. Medway High Tension

40+50

Pasture

19-9+6-14

54.5

+67

51.5

4

+50

St.

15 +41
34

+42

40+17.07

18-9+7-14-34

8" Bir + 04

20.5

40+0

18-9+6-14-33.5

14.5

18" M + 96

47/64

+74

13

10" A + 70

16

3x3 conc slab + 62

12" Conc.

16 +66

12.5

16

16 +58

open field

39+50

18-9+6-15-33

8

12" A + 49

14" A + 40

15

2-8" A's + 33

16

12" A + 08

16.5

10" M + 06

20

14" A + 0

19.5

39+0

18-9+6-13-32

15

14" E + 04

Plotted

Survey

35

+16

14

42+0

20-9+6-14

St.

73.5

+92

High Tension

69

+78

41+50

19-9+6-14

14

+47

+38

21

14.5

+22

17

+18

12" Conc

15.3

+14

+15

20

+06

19

18-9+6-13

+97

+92

14

+85

+85

+76

Lovering

open field

plotted

36

Lovering St.

Medway 44+0

168

92.4 33
+96 18-8-6
Lines +03

12" M +78 (2) 21

20" M +53 (2) 21

43+50

20" M +41 (2) 20

+39

open

+31
+28
+35

12" M +4 +03 (2) 15

43+0

Lovering

+63

Lines +78

42+50

St.

22" P +66

37 (2) 12" A +61

Dry Faced Masonry

33.5 (2) 20" A +36

12" Conc.

+25

Lines +78

14" M +97

12" A +90

+59

open

Plotted

Survey

37

set up 45+50

16" E +49 (2) 25.5 18.5-8-7

16" E +47 (2) 24

8" E +18 (2) 22

16" +01 (2) 21

45+0 set up

open

+59

44+50

14" M +44 (2) 14

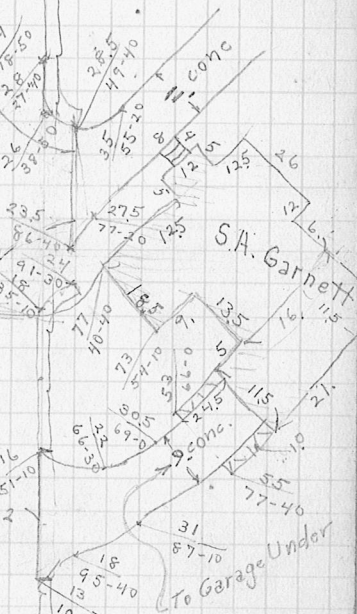
8" M +22 (2) 22

16" M +03 (2) 16

St.

Lovering

Dry Faced



20" P +63

31 (2) 20" A +75

22" M +62

30" P +30

Plotted

38
168

Lovering St.

Medway

46+50

19-10-6-12-15

St.

14"E + 19

16

16"E + 09

21.5

46+70

19-9-6-13-16.5

40"M + 21

14"E + 92

20.5

10"M + 85

21

2-6"M + 83

20

+76

12

16"E + 60

22

12"E + 33

21

Lovering

plotted

Survey

52+21.74

39

open field

Lovering St.

Winthrop

St.

Lovering St.

open field

plotted

open field

Winthrop St.

open field

Note: 114° angle is
for this survey only and
is not Winthrop St
connection. That came
later.

168

2+0

Lines + 92

+02

16" M + 99

21 - 9 + 8 - 185

105

+78

14" M + 75

15

St.

16" E + 56

17

1+50

22 - 9 - 8 - 185

12" M + 42

16" E + 34

17

open

Winthrop

Dry Face Wall

open

20" E + 11

17.5

1+0

23 - 10 + 8 - 185

10" E + 89

17.5

16" M + 99

10" E + 69

18

16" M + 78

115 + 67

14" E + 61

19

16" M + 57

15.5

0+50

23 - 11 + 8 - 185

Lowering

A

47+06.00

Plotted

St.

4+0

18" M + 0

23

7 + 9 - 205

14

scrub woods

Wood

St.

Lines + 68

+68

3+50

14" M + 49

23

8 + 9 - 21

14

50" O + 44

64

Scrub

18" E + 22

+39

15

Winthrop

open

3+0

16" O + 96

20 - 9 + 9 - 21

11 + 98

15.5

195 + 63

20" O + 73

16

+52

2+50

205 - 9 + 8 - 192

+40

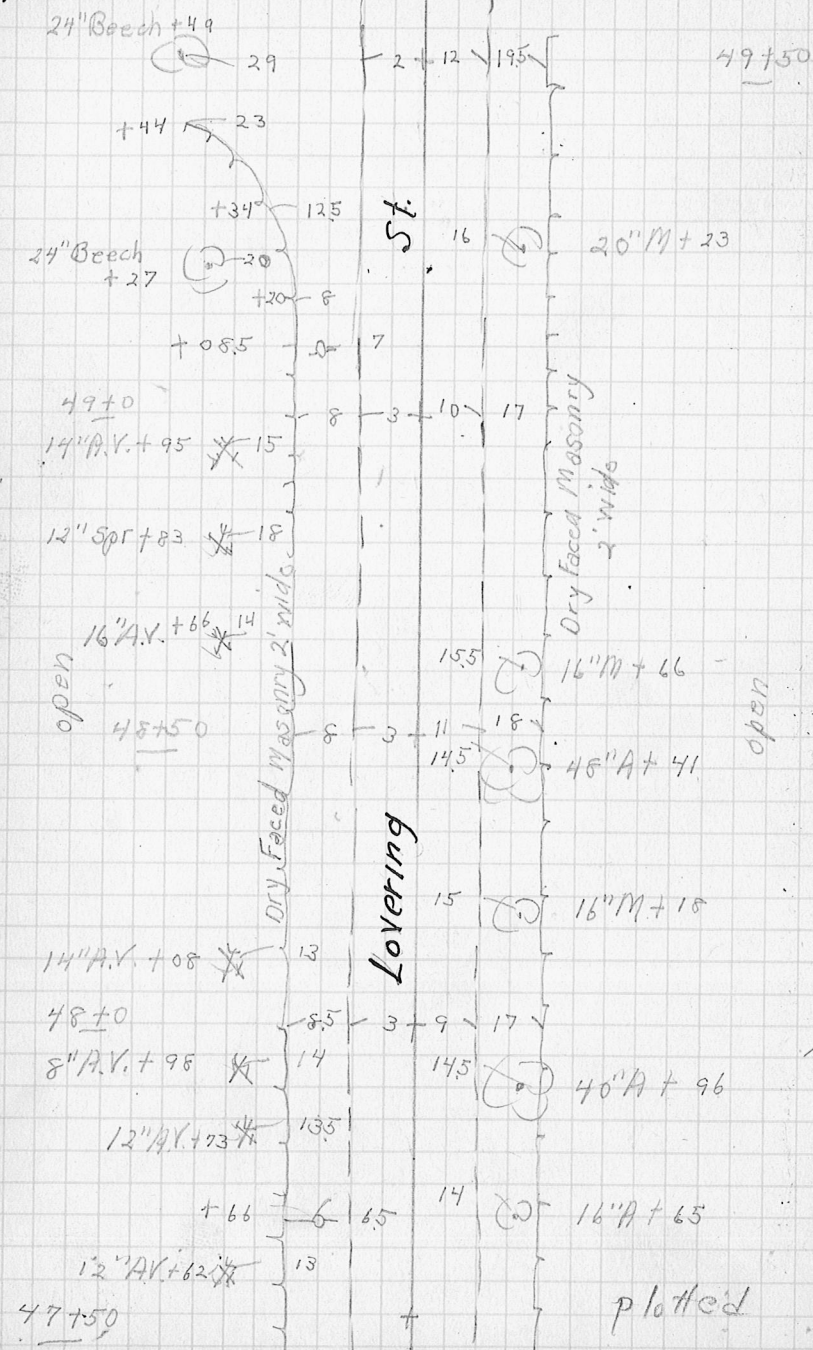
17

22" E + 34

Plotted

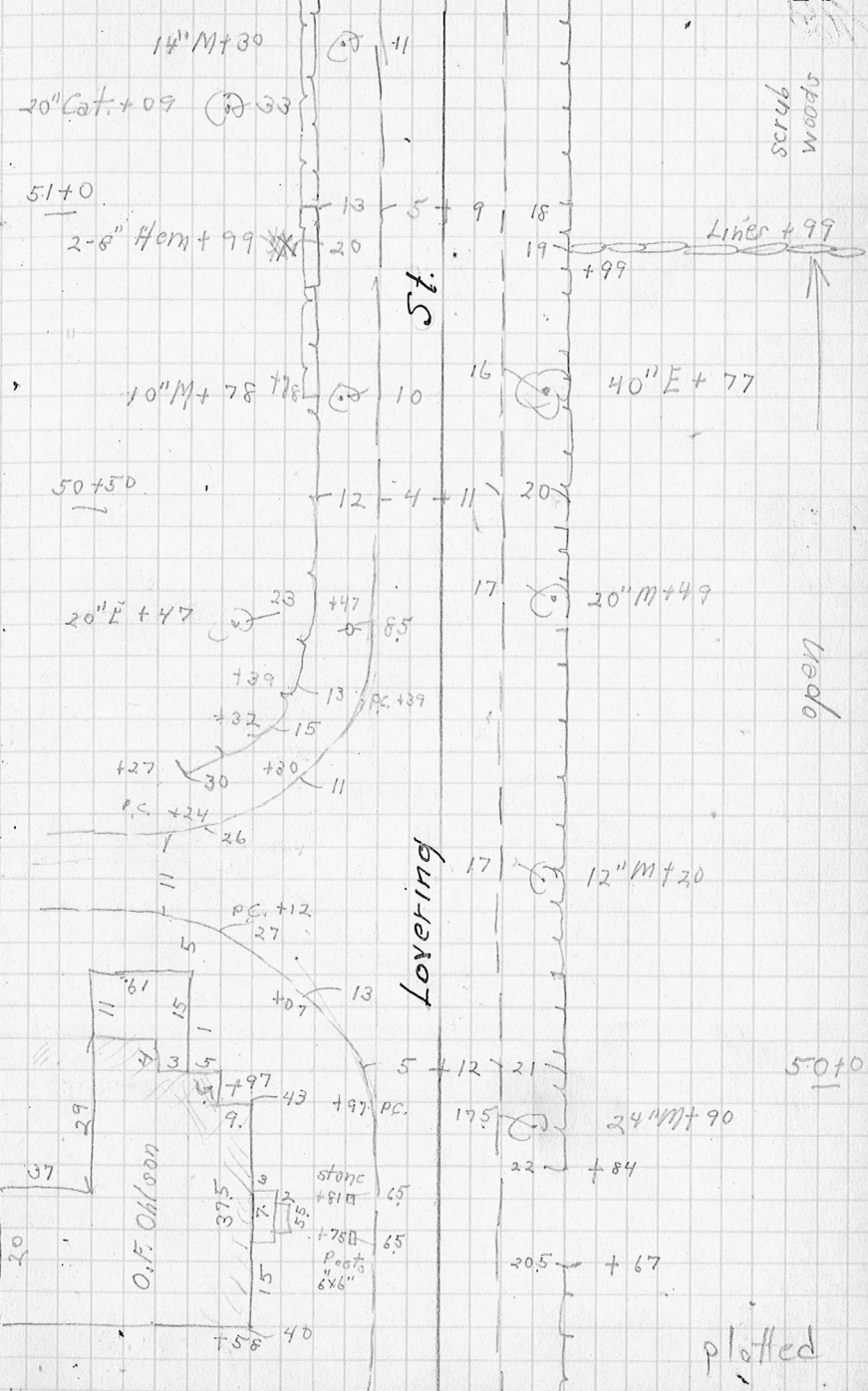
44 Lovering St. Medway

168

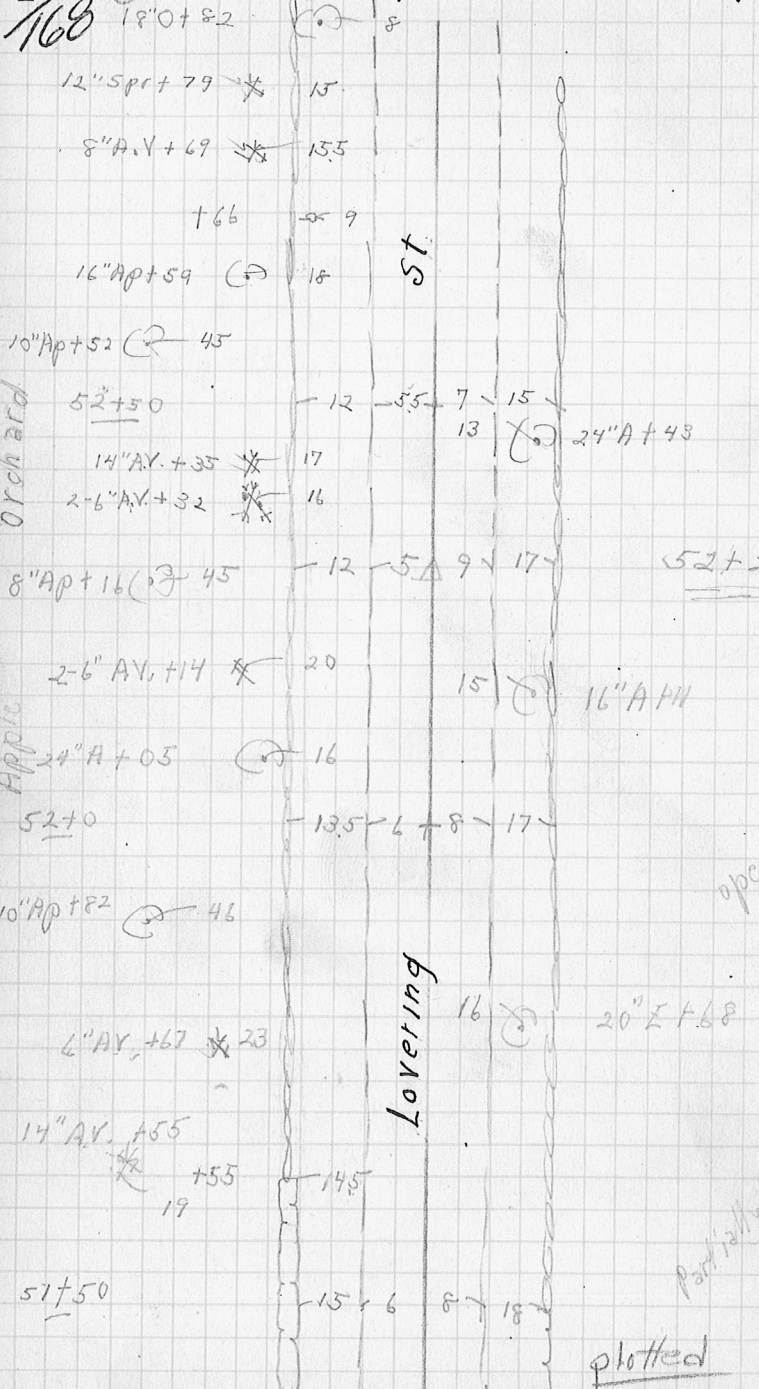


Survey +43

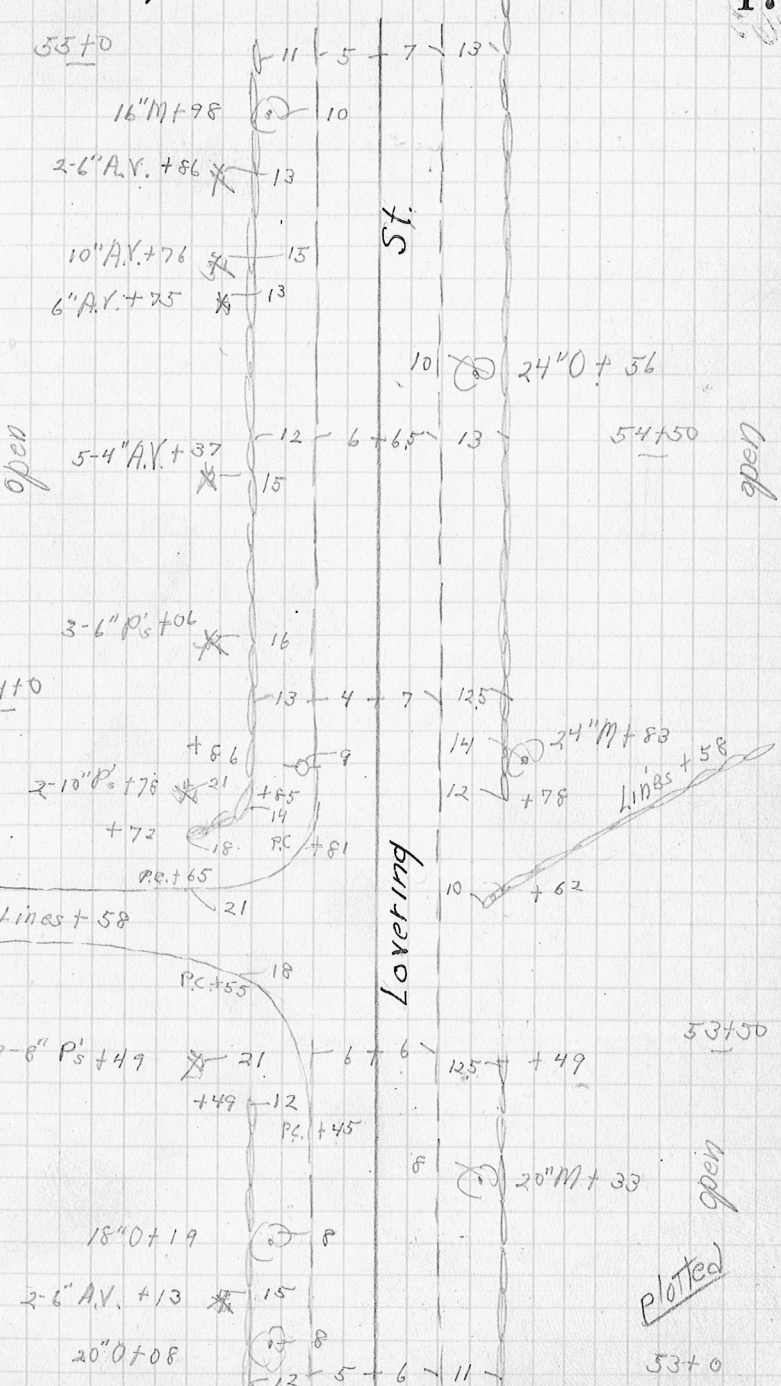
45



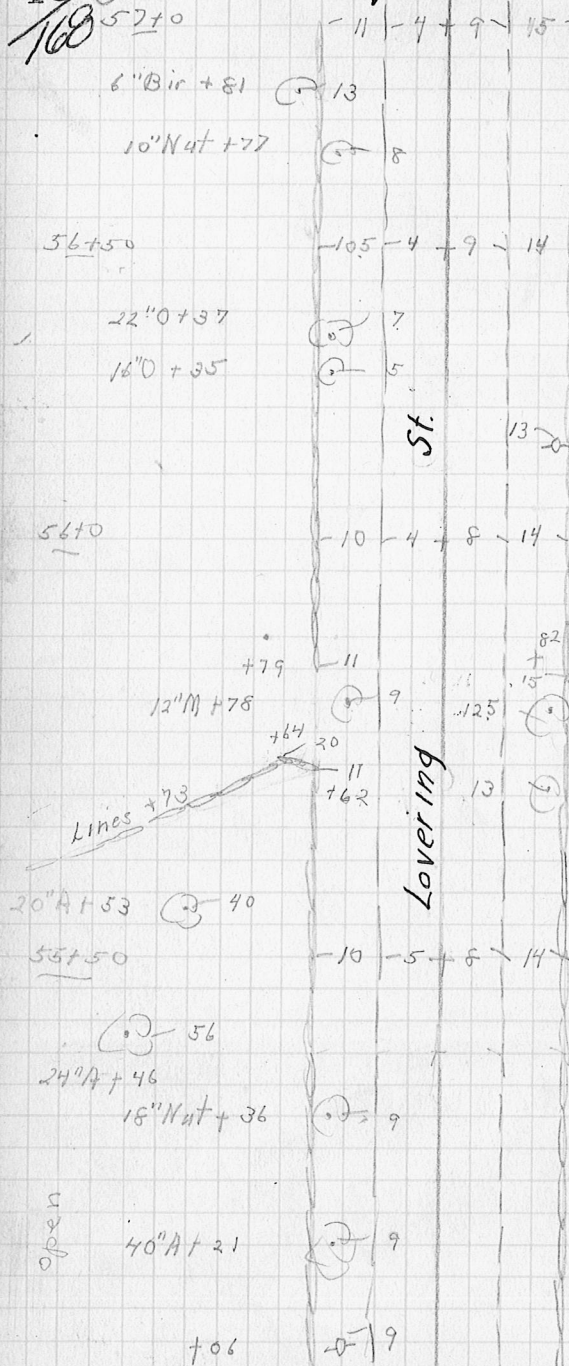
46/168 *Lovering St. Medway*



Survey



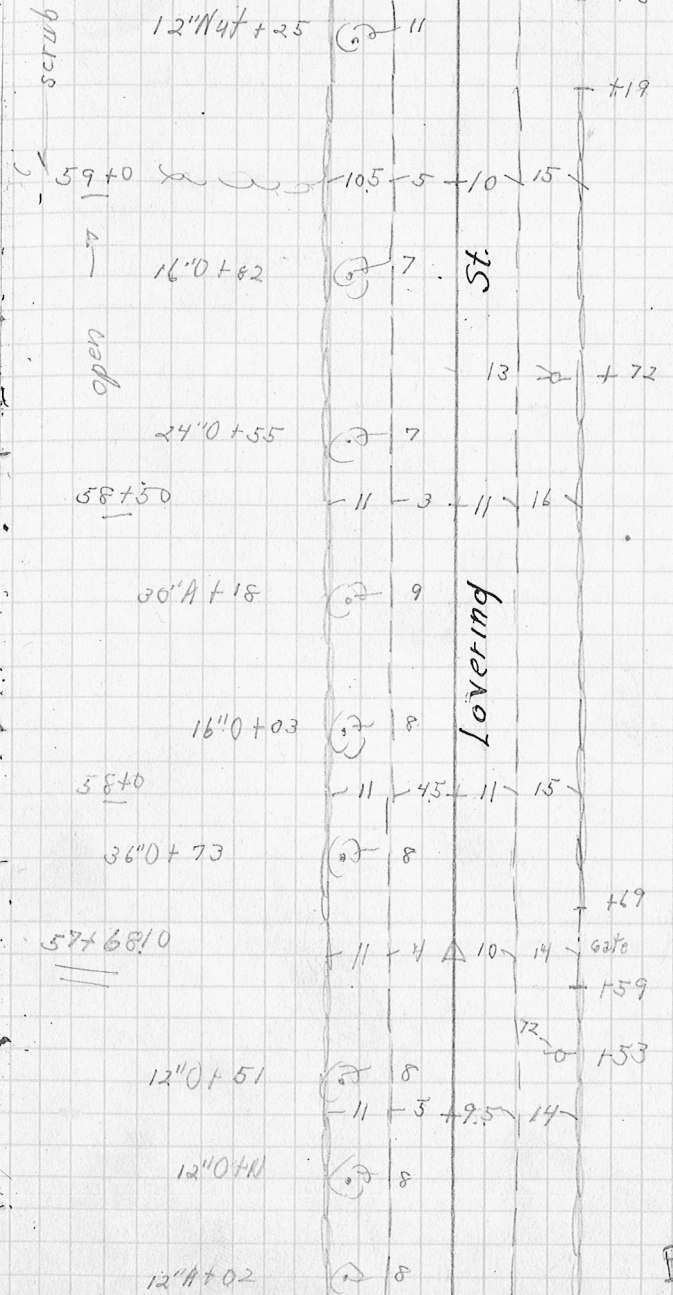
48 *in* Lovering St. Medway



Survey

49

scrub woods



50 Lovering St.

Medway

Survey

51

168

61+0

16-8-8-16

12

+01 18" Nut

12" O + 84

13

24" O + 57

12

60+50

15-7-8-17

woods

60+0

14-7-9-16

10.5

18" Nut + 33

woods

+97

Lines + 79

+75

13

+65

+55

59+50

11-5-9-14.5

18

10" O + 67

16.5

+64

14.5

+58

14

+40

30

Plotted

open

24" O + 51

62+50

16" O + 31

14" M + 02

62+0

14" Nut + 97

woods

14" O + 71

61+50

18" O + 46

20" M + 16

St.

Lovering

22

8" M + 74

35 8" M + 72

28 8" M + 66

12

18-9-6-14

14

15.5

8" M + 49

9

+42

34

+36

Lines + 42

12

14" Nut + 05

16-8-6-14

12

9

20" O + 76

9

12" Nut + 52

15-8-6-16

12

28

2-8" M + 30

11

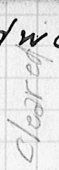
+20

Plotted

woods

52
168

53



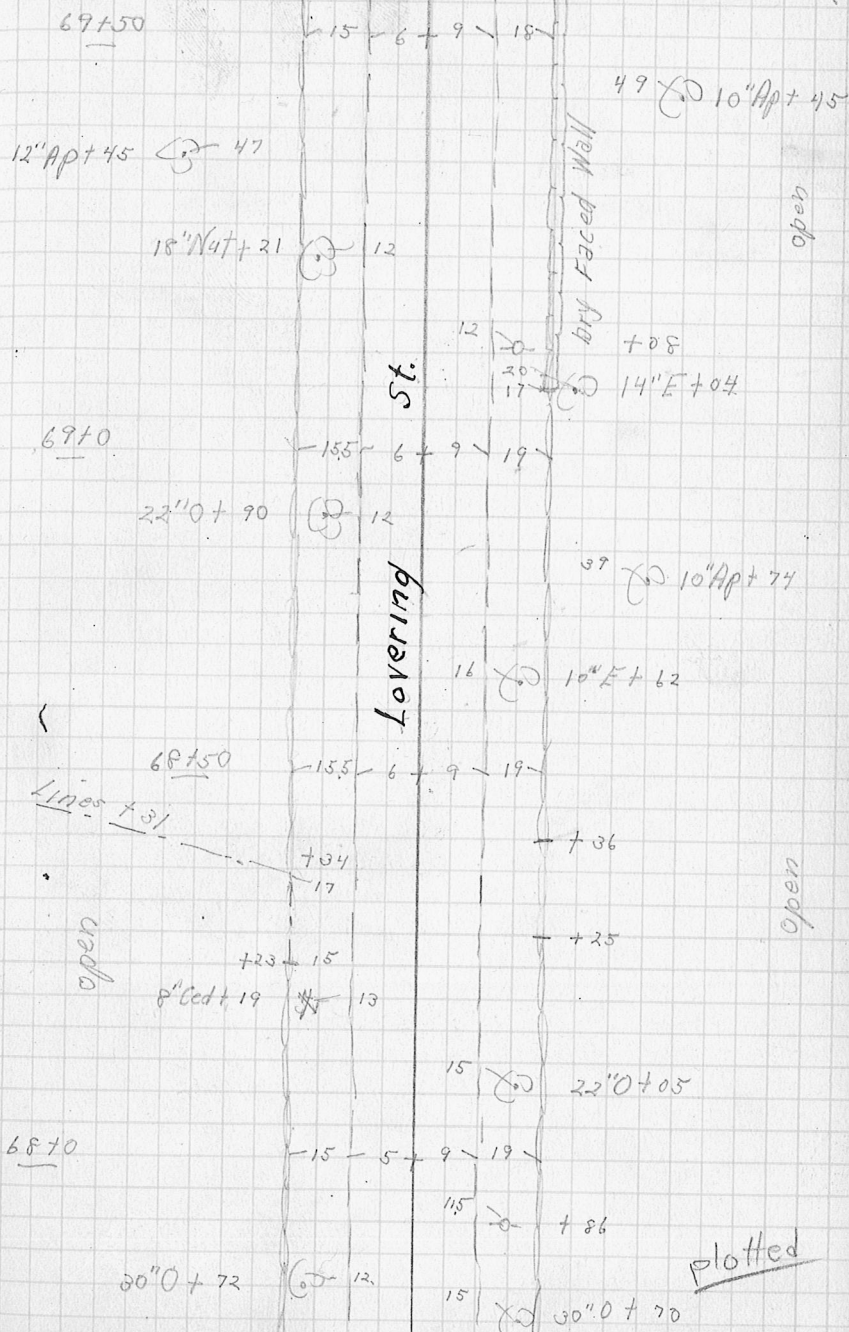
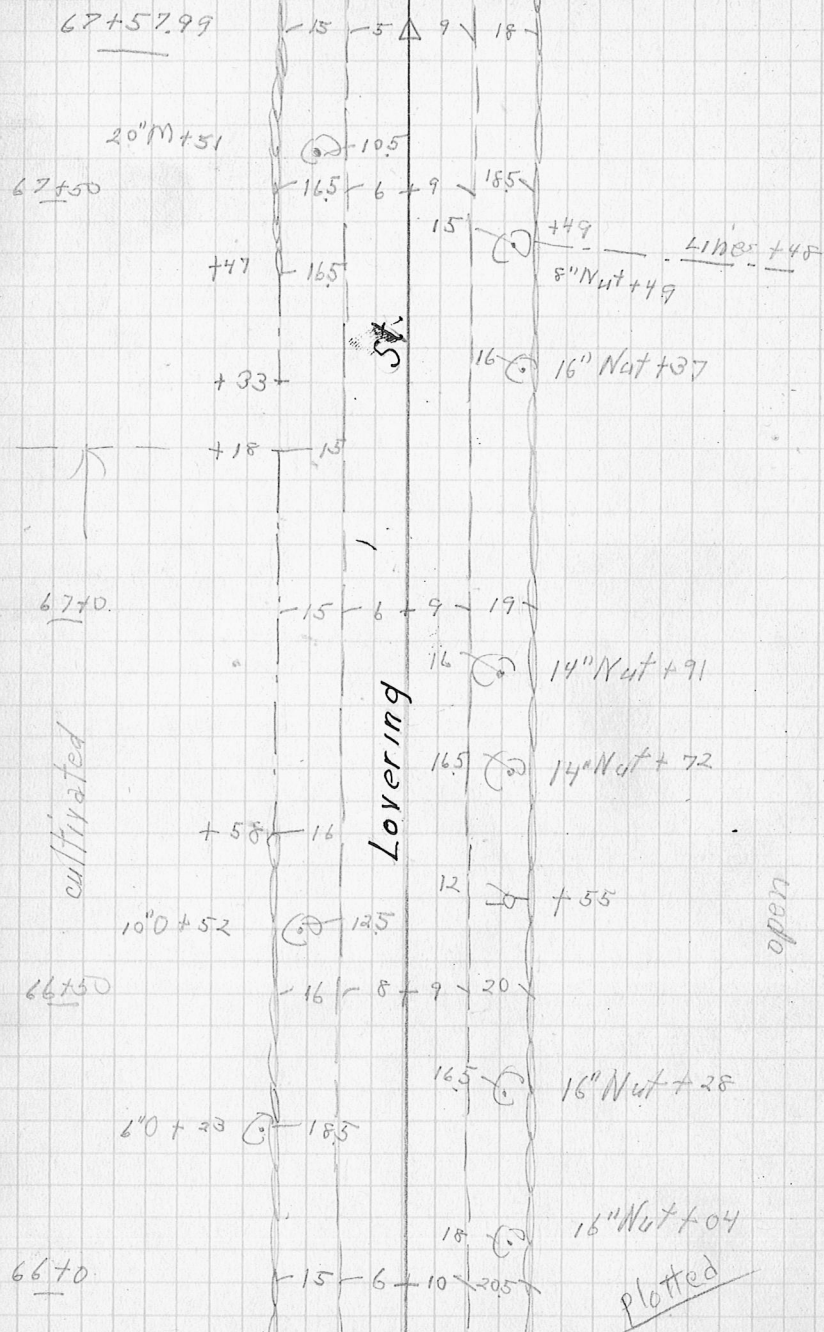
Plotted

54
168

Lovering St. Medway

Survey

55



56

Lovering St.

10" E + 01

Medway

168 + 0

+ 95 - 15

30" M + 35

set up 70 + 30

36" M + 23

70 + 0

16" Ap + 82 - 66

20" M + 51

Lovering St.

21

15

10

17

16

11

10

9

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4

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2

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-319

-320

-321

60/108

Lovering St. Medway

+34
culvert, conc slab over
3.5 sq.

80+0

16" Conc
21
12-2+135 24

+92
54
54
+87
6'x6'
well house
open

+92 10
St.

26 +71

+62

+61

79+50

79+0

Lines +77

open

+79

10
14

Lovering

+82 Lines +80

32 10" Nut +80

215 10" Nut +75

16 12" Nut +56

16" O +53

8

78+47.69

+47

24" O +32

9

+18

6

145 6" Nut +06

plotted

78+0

13-3 12 19

Survey

61

apple orchard

83+0

8-14-18-59
17-15

73 12" HP
330-45
47 352-30
45 346-40
2-12 1/2
77 304-0
3855
343-11
42 357-30
32 349-0
30 332-0
37 315-45

St.

wire fence
38 31-40

46 84-40
10" HP

Barn

38 42.5
14

81 255-20
78 213-30
49 280-45
22 297-40
11 301-50

38 19-30

82+50
setup

27 116-30
28 135-30

82+0

House
240 256-20
242-30

Pinecrest Farm

30" F +67

81+50

81+0

80+50

old wire fence

Lovering

+73

8" P +61

14" Tree +67

plotted

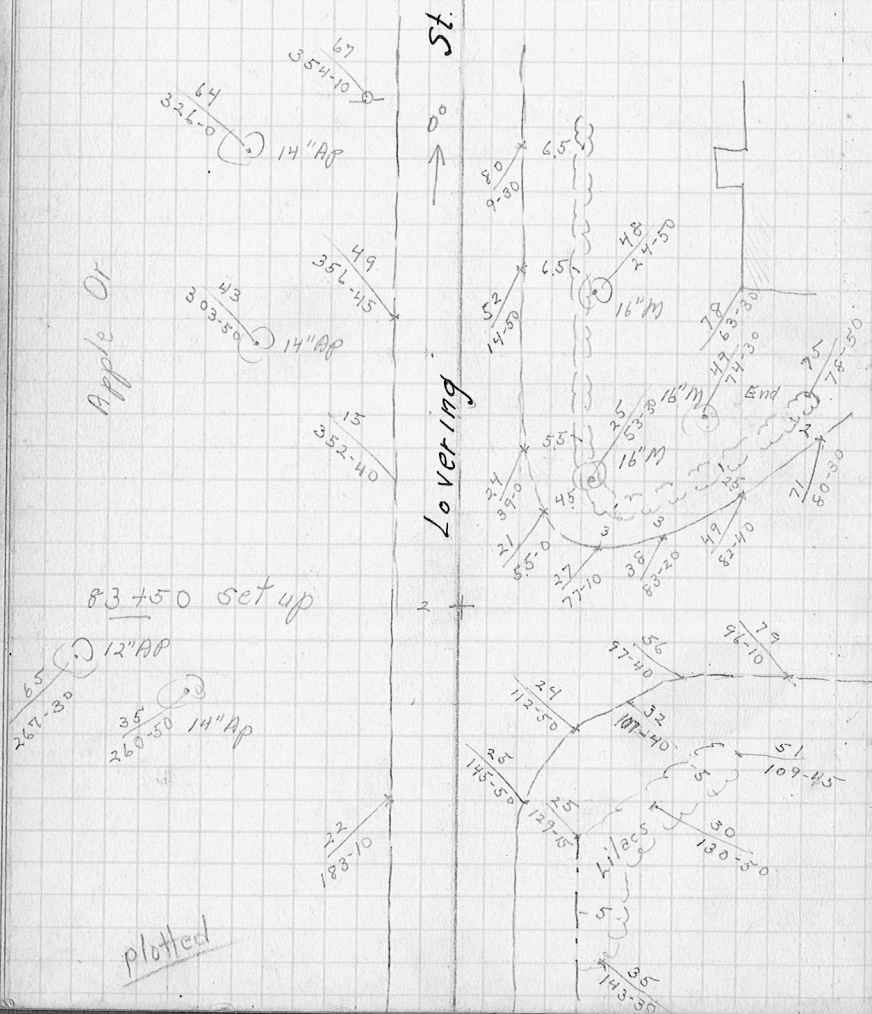
2-11-3+135 19

11-3+12-20

3-11-2+13-20

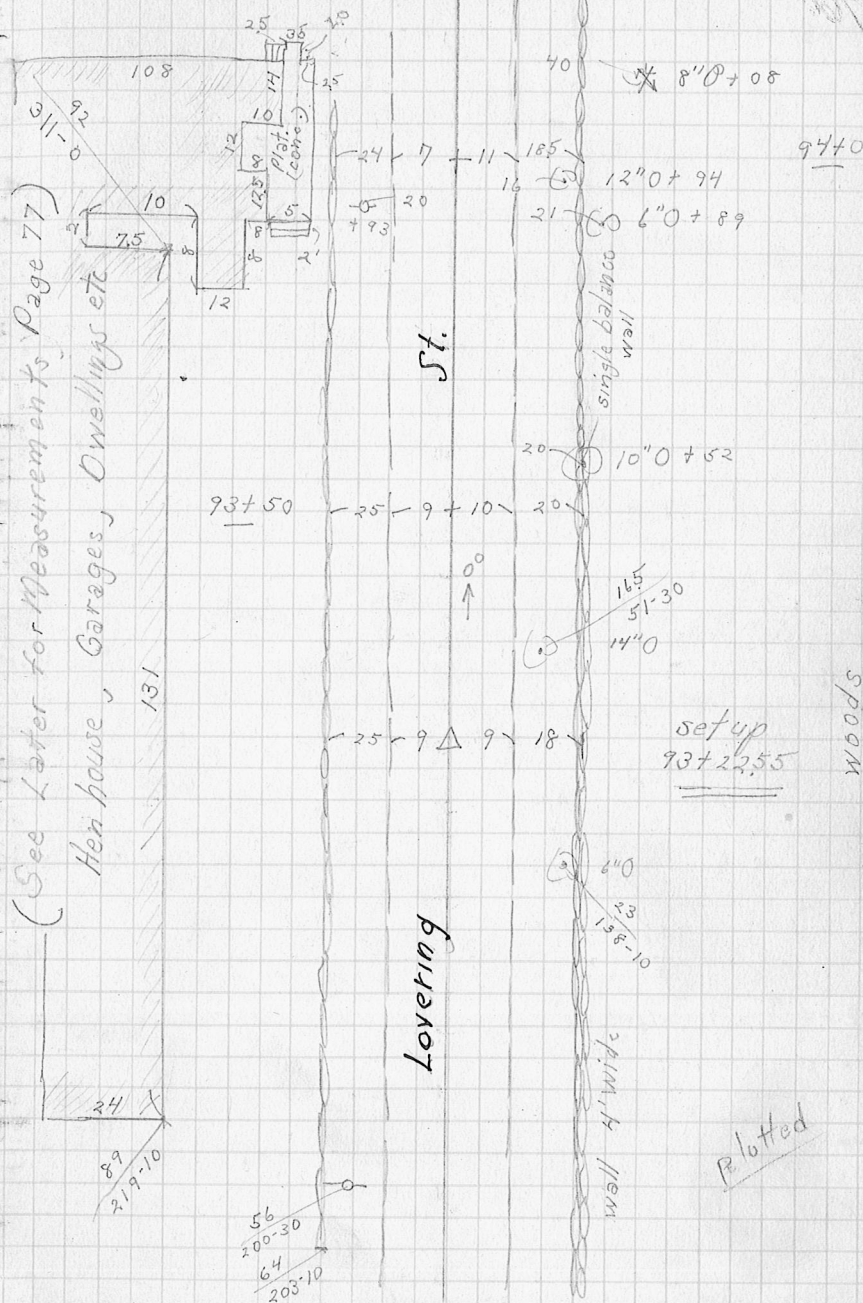
open

(See N.B. 167 Page for Survey to Pond + Maple Sts)



(See Later for Measurements Page 77)

Hen house, Garages, Dwellings etc



(See N.B. 167 for Survey from Pond St to here)

$95 + 50$

Woods.
Low & Swampy

75

puirao.7

woods

A. Brennan

Lovering

Partially cleared

Plotted

Plotted

16.5 X 6" N x 84

$$16 \times 8^0 m = 81$$

24 ~~12~~ 11"0 + 46

27 ~~X~~ 6"0 + 04

9540

16"0 + 61 (0.7) 49

Lines + 61 A 96750

16" 0 + 21/0 45

25) $\times 8'0442$

26 ~~12~~ 6" OMS

26 8" Oct 22.

24 ~~✓~~ 12" 0 + 19

$$+57 \quad -0 \quad | 18$$

Stone #52 □ - 19
(corner)

20.5

Gar. 11

01	01
----	----

47

27.

16"0 + 61 (0.7) 49

Lines + 61 A 96750

16" 0 + 21/0 45

16 ~~7~~ 6" M + 83

$$18 \cdot 2 + 58 = 72$$

8"0 16"0

23/06/2017

35 ~~20~~ 12"0 + 20

$$3/ \times 10^N 0 + 1$$

255X.0 6"m + 0

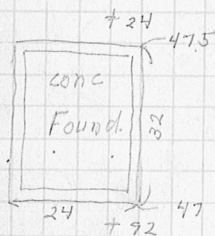
more to me

(2) 2-10 Oct 93

50 ~~(2)~~ 10" 7 20

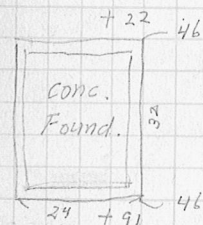
160

104+50 751 175

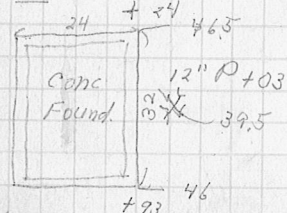


103+50

14" P + 35 41



102+50



Plotted

5t.

Lovering

18 3-8" O + 57

24 2-6" O + 96 104+0

305 4-6" O + 57

32 10" O + 40

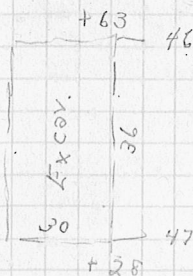
103+20.55

103+0

20 4-8" O + 94

21 10" O + 87

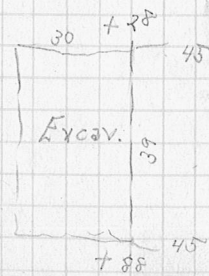
102+0



106+0

8" P + 74

105+50



Plotted

19 14" O + 65

23 6" Chy + 40

20 6" Chy + 46 106+50

30 8" Chy + 25

22.5 10" O + 16

14 10" M + 05

19 6" O + 75

27 6" P + 43 open

18.5 8" M + 41

27.5 10" P + 32

30 10" P + 28

24 2-6" P + 24

17 10" Liner + 06

21.5 6" O + 99

27 8" O + 96

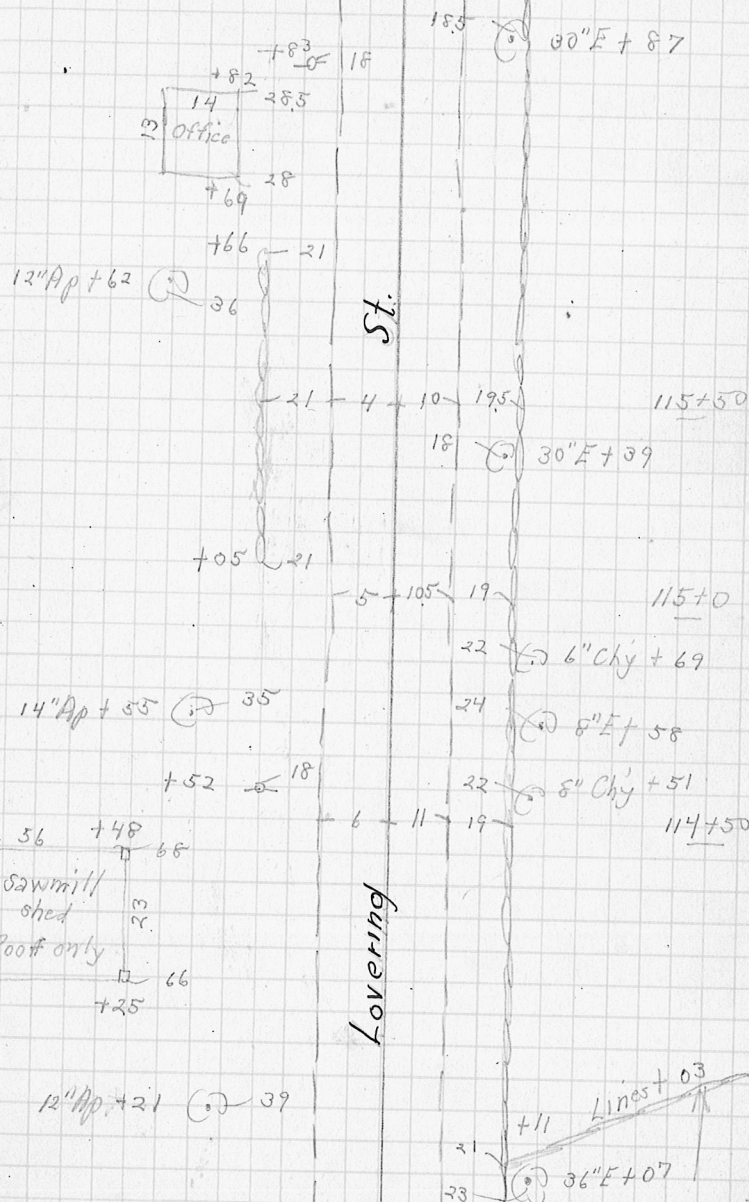
Lovering

Woods

105+0



Plotted



Plotted

open field

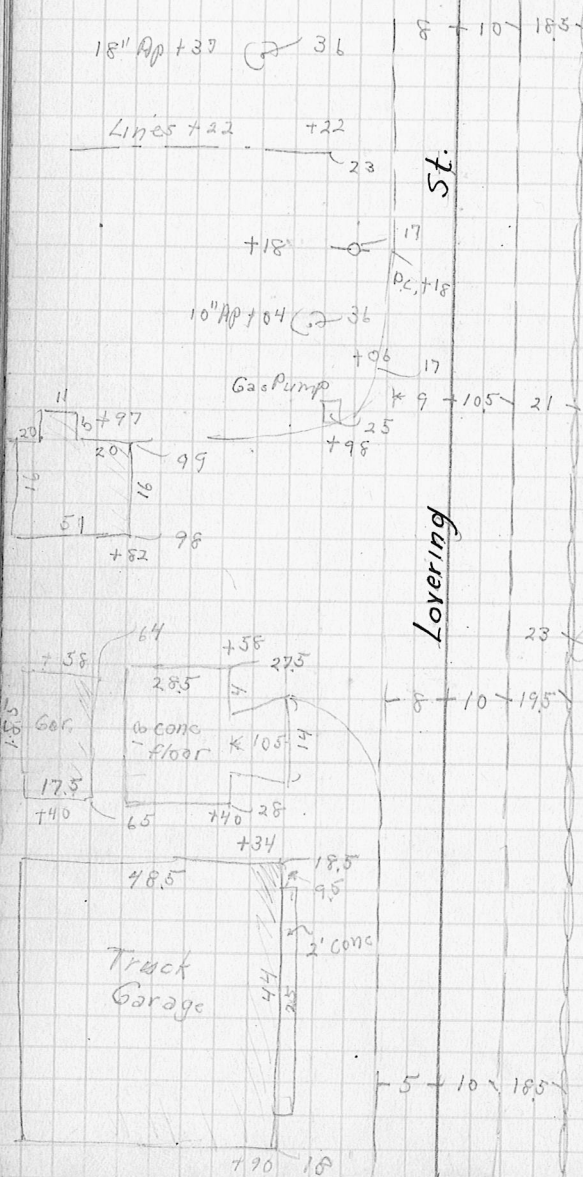
how
x
Sincerely

74 ~~168~~ Lövering St. Medway

Survey 119+43.57

Holliston St.

75



75.

Lovering

117 + 30

11740

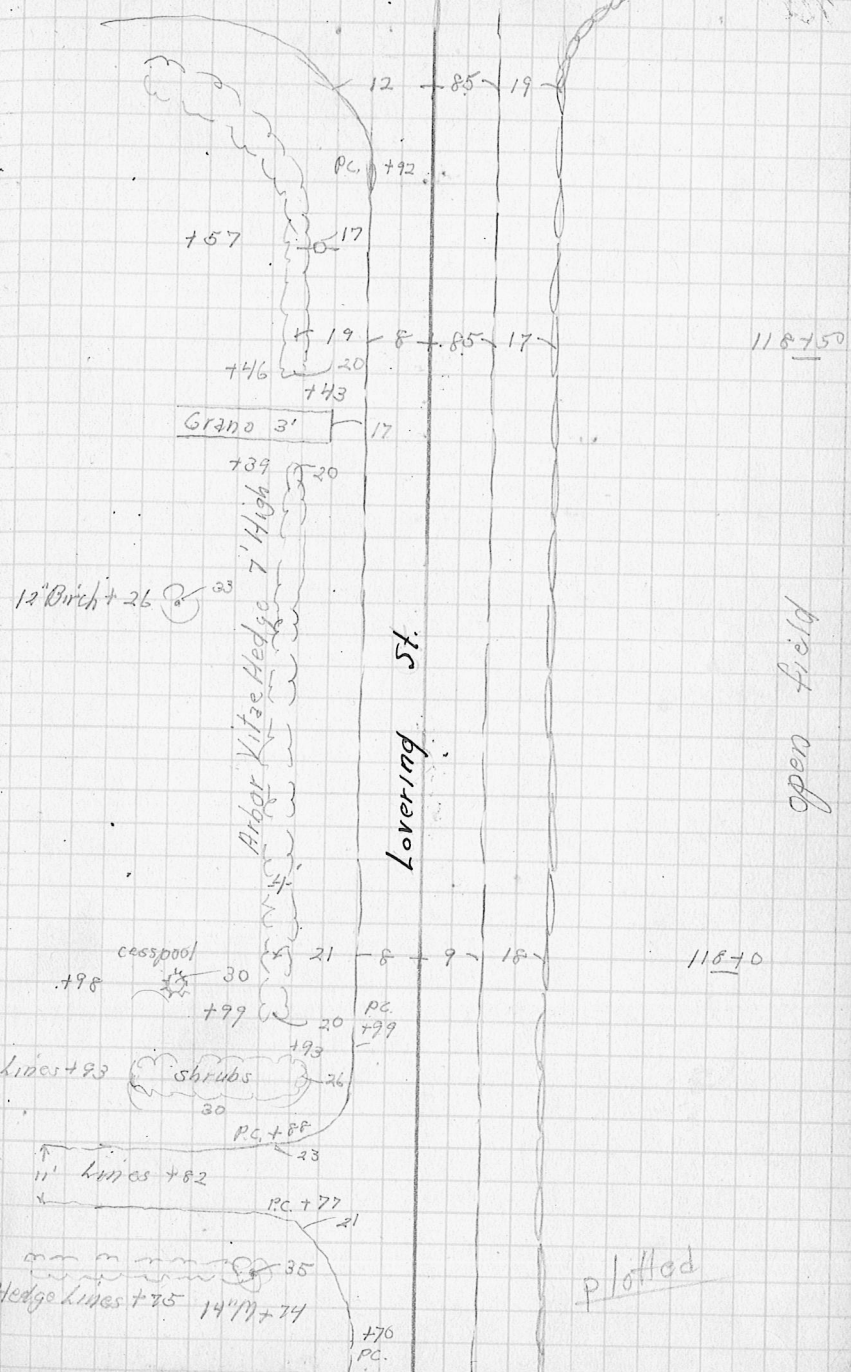
23 ~~KD~~ 2-6⁴ Chy + 56

 $1/6 + 50$

open field

11670

plotted



Lovering St.

open field

plotted

11840

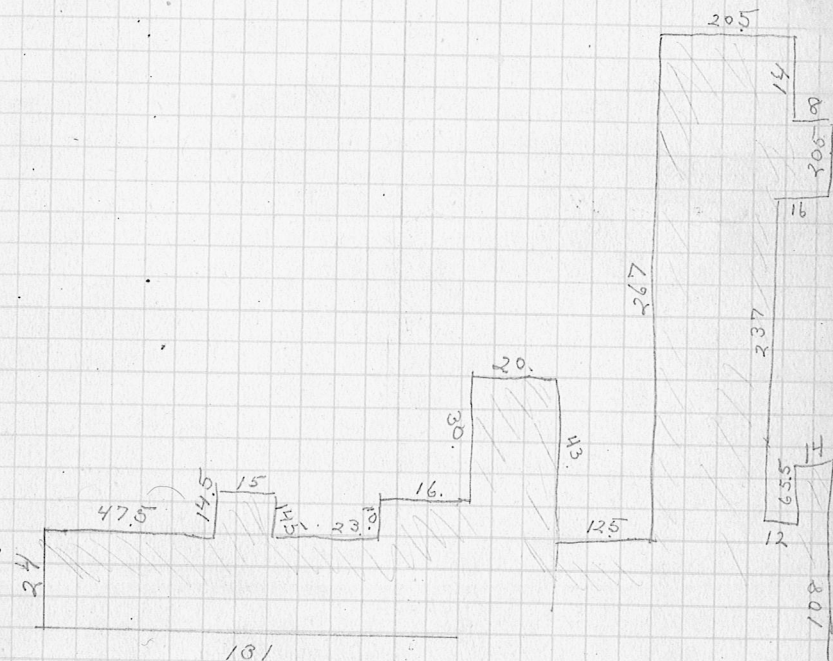
118750

78/168 Lovering St. $119 + 43.57 = 18 + 44.70$
Holliston St.

(See Page 63 for Building Front)



(See N.B. 171 P 24 Holliston St.)

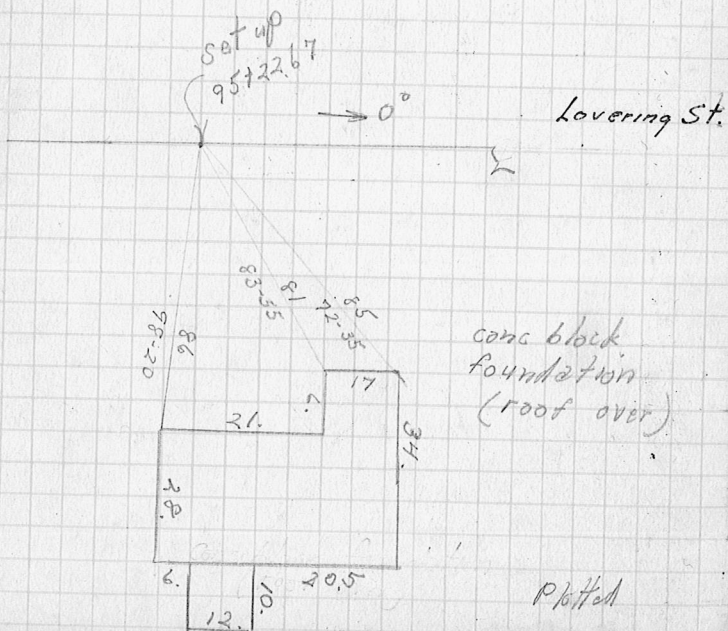
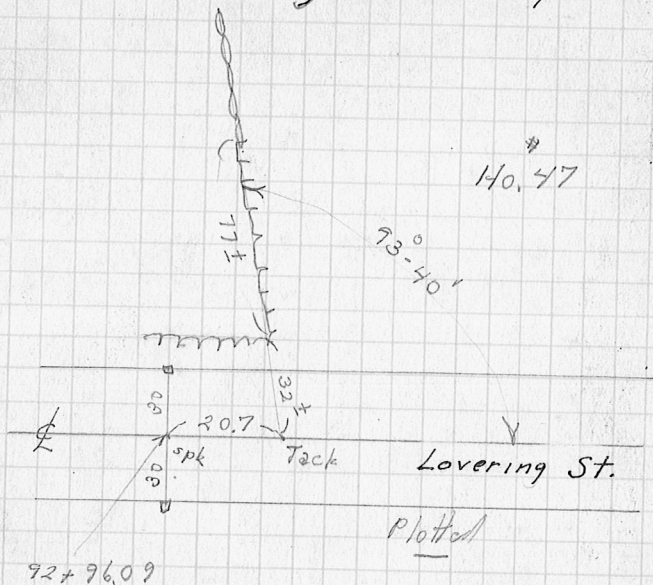


Lovering St.

Plotted

Page 63

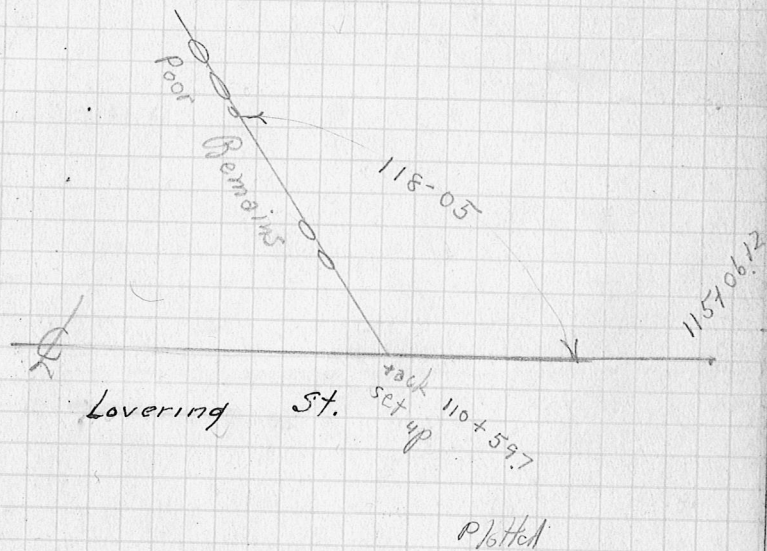
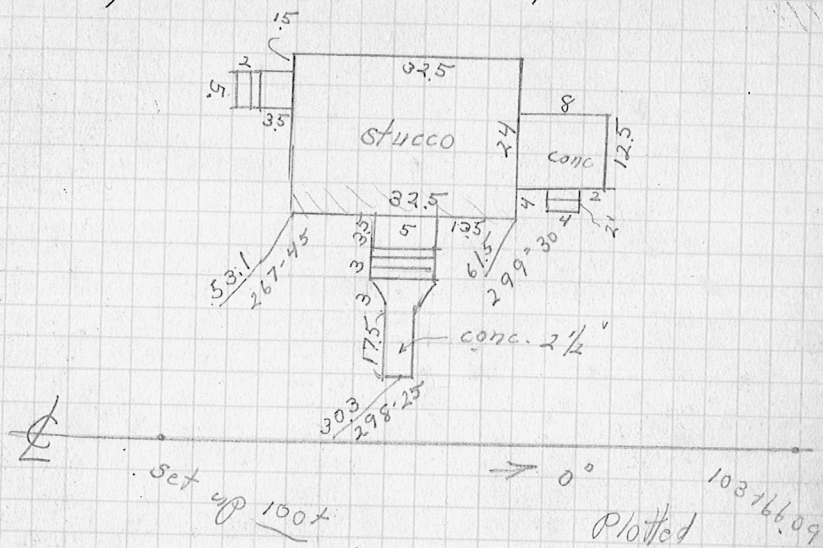
78
108 Additional Survey Lovering St.



Medway

June 16, 1953

79



80/ Lovering St.

Medway

Layout

May 1953 81

X=103720.55 spk P.12 A

160.56 307.65

TACK IN COR. TRIM BOARD
UP 0.6 GARAGE

77.46

179° 40.50
179° 02.30
179° 40.50

THIS ANGLE NOT CHECKED 1986

Bot. COR. 3rd Shingle UP #32

63.64

293.41
293.42

524.05
524.07

39.19
259.17
358.36
358.37

spk P.82

526.11 Calc
524.07 Meas.

St.

spk P.97

358.41 Calc
358.37 Meas.

Lovering

spk P.97

OLD TACK UNDER COR. Pg. 99 #33 (1986) #40 (1953)

D.H. Stone

140° 30'

84° 11.40
252-35
84° 11.40

Holliston

New &

147.00 spk N.B. 171 P.95

85° 30-20 X-Cut
256° 31' Rm. C.B.
85° 30-20

226.56

957.86

D.H. Hedge Outcrop

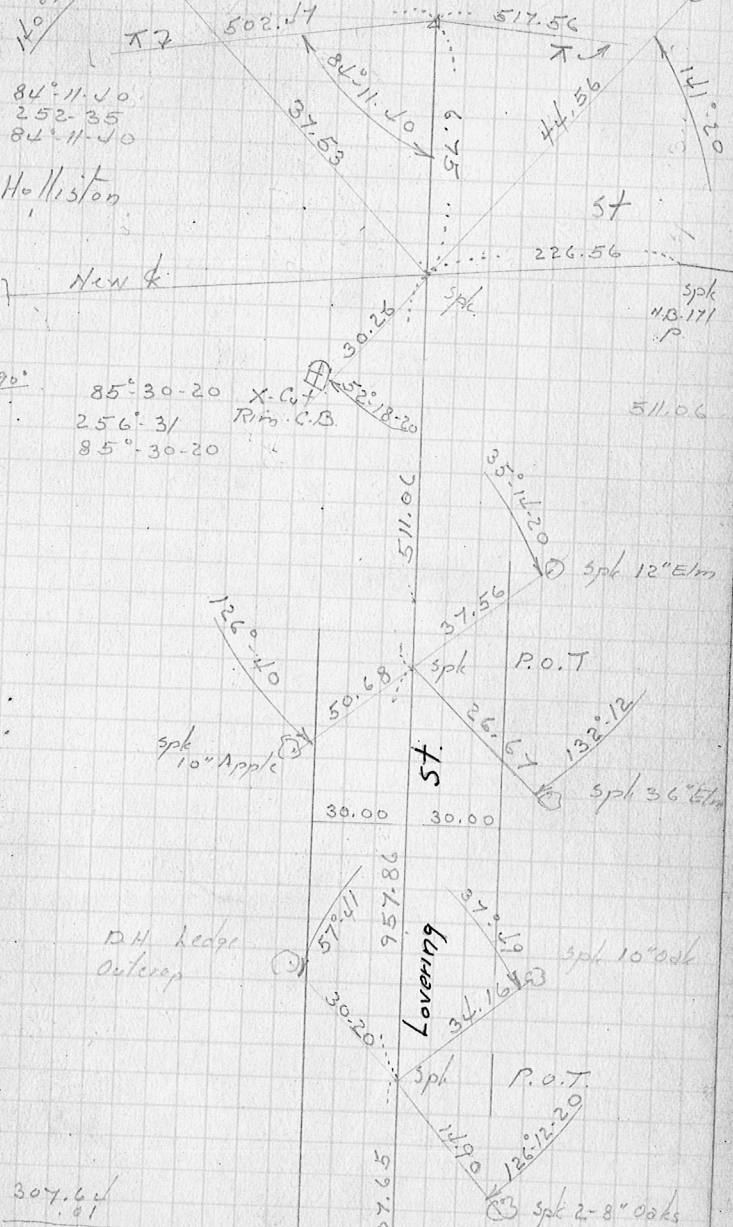
Lovering

spk

P.O.T.

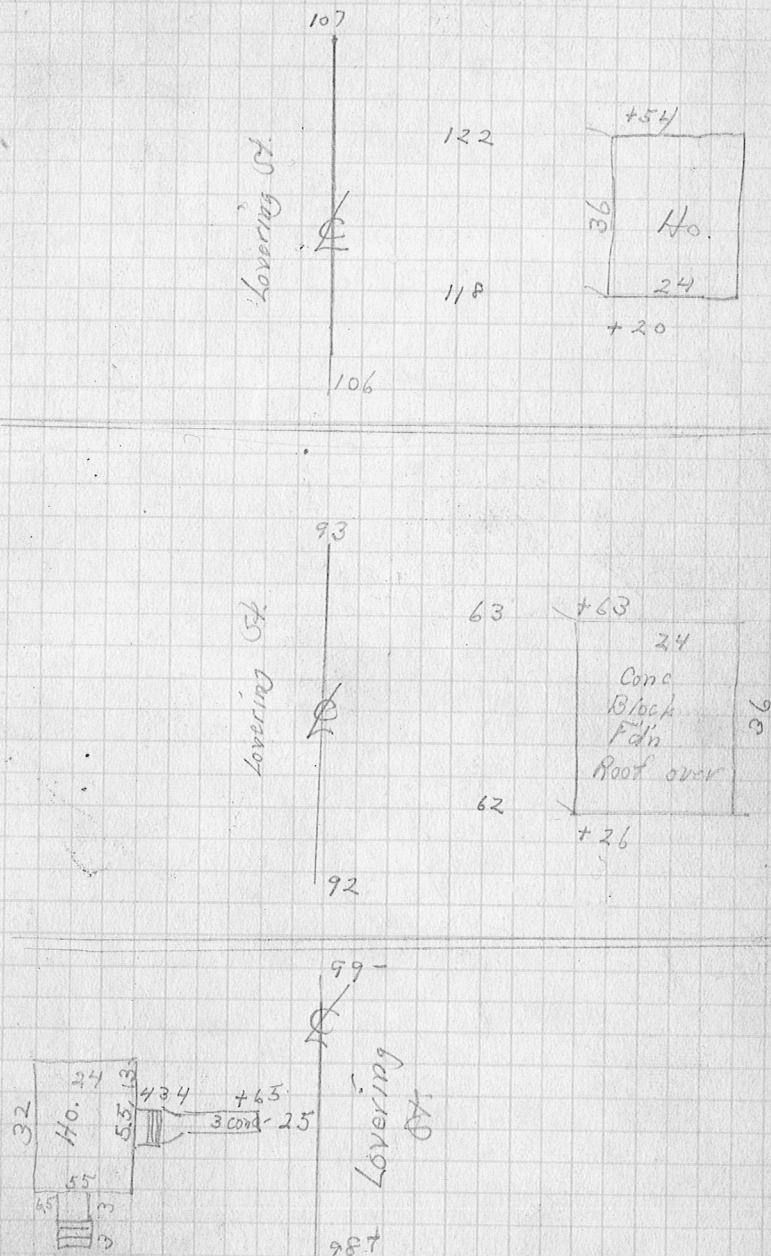
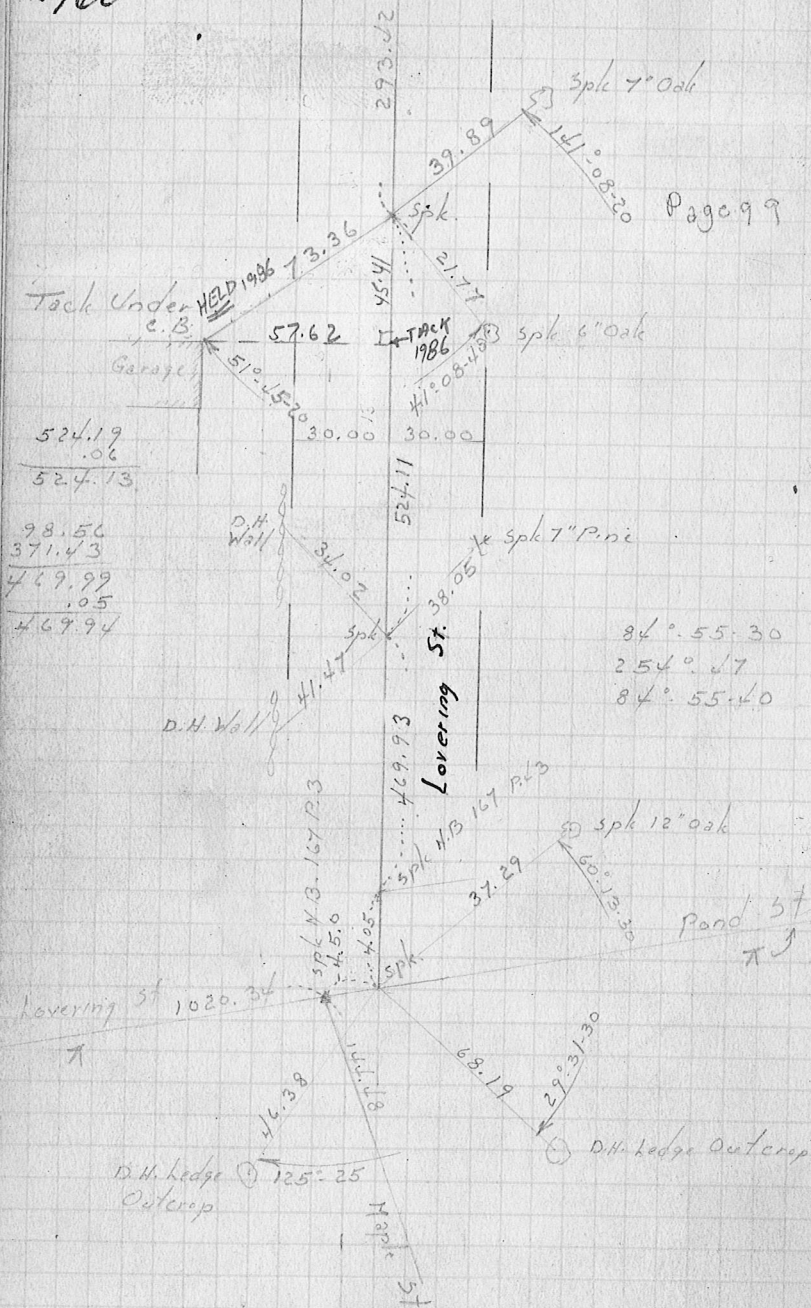
spk 2-8" oaks

307.64
307.65



82/168 Lovering St. Medway Layout. Feb 1952

New Houses Lovering St June 1954 83



168

Medway

Layout

Feb 1953 85
Meda, Tocci
Gino

RESTAKED FEB 1980

RE-STACKED Feb 1980
SEEN B127/152

Ties NB 127/153

May 1960 19.92

D. H. Lodge
Outcrop

Pin in lead in top stone

~~2.70~~ 2.67 (1964) OK 1980

d.h. in bedstone

~~4/26 24" M~~

D.11 Flush ledge

$$\Delta = 1^{\circ} - 12 - 30^{\circ} \text{ (o.k.)}$$

$\angle R = 80^\circ 30'$

$$\angle T = 84.68^\circ$$
~~D.H. Bedstone~~

~~out
New Tie spr
Clump 6" Elms~~

NB 127/152

1980 TIES

d.h.
bedstone

Print in Face
B.B.

1892

W. A. C. C.

Lovering St

$$\Delta = 89^{\circ} 27' 50''$$
$$\phi R = 88.61 \quad \checkmark$$
$$\delta T = 87.78 \quad \checkmark$$

88/Lovering St

780.30

168

A = 142-24-10
off R = 50.00
off T = 146.89

Medway

780.20
New Way

Old Way

See P. 110
100.5

10.82

S.B. Fnd (2001)

46.77

11.82

S.B. Fnd (2001)

4.59

1.82

U.P. #74

11.82

4.59

1.82

U.P. #74

11.82

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U.P. #74

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U.P. #74

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U.P. #74

11.82

4.59

1.82

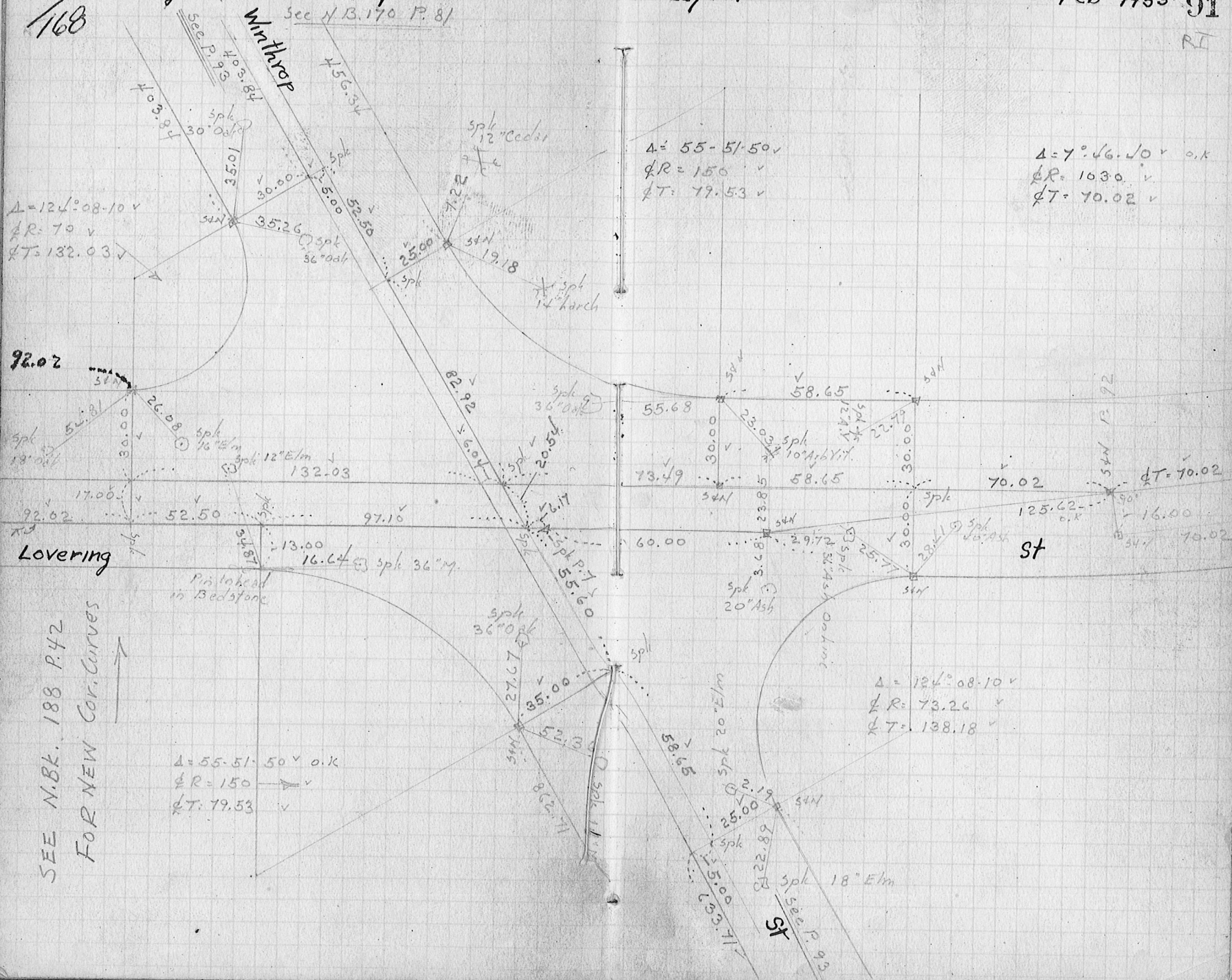
168

Medway
Sec 4 B. 170 P. 81

Layout

Feb 1953 91

PL



94/Lovering St
168

$$\begin{array}{r} 99.37 \\ 244.83 \\ \hline 344.20 \\ .02 \\ \hline 344.18 \end{array} \qquad \begin{array}{r} 478.34 \\ 478.02 \\ \hline 478.32 \\ 468.62 \\ \hline 9.70 \end{array}$$

98.32
 442.50
 542.90
 100.40 Calc from π
 100.10 Meas

57.47

See CB. 87P110

Medway

$$\begin{array}{r} 90.37 \\ 85.49 \\ 33.58 \\ \hline 238.70 \\ 448.14 \\ \hline 448.10 \end{array}$$

Layout

$$\begin{array}{r} 475.89 \\ 448.10 \\ \hline 27.79 \end{array}$$

Mar. 1953 95

Medea Tucci

Peteros

Root 8" Stamp
RE

TIES 192/114

425.00

✓
425.00

00

24.97 Meas

TIES

425.00

604 06

SEENB 192/112
RESTAKED 1980

sketch of Intersection for Ties

Large spk

3pl 36" Oak

475.89

See P. 92.

$$\begin{array}{r} 542.90 \\ 98.32 \\ \hline 641.22 \end{array}$$
$$\begin{array}{r} 36.80 \\ 81.52 \\ \hline 98.32 \end{array}$$

98 Lovering St

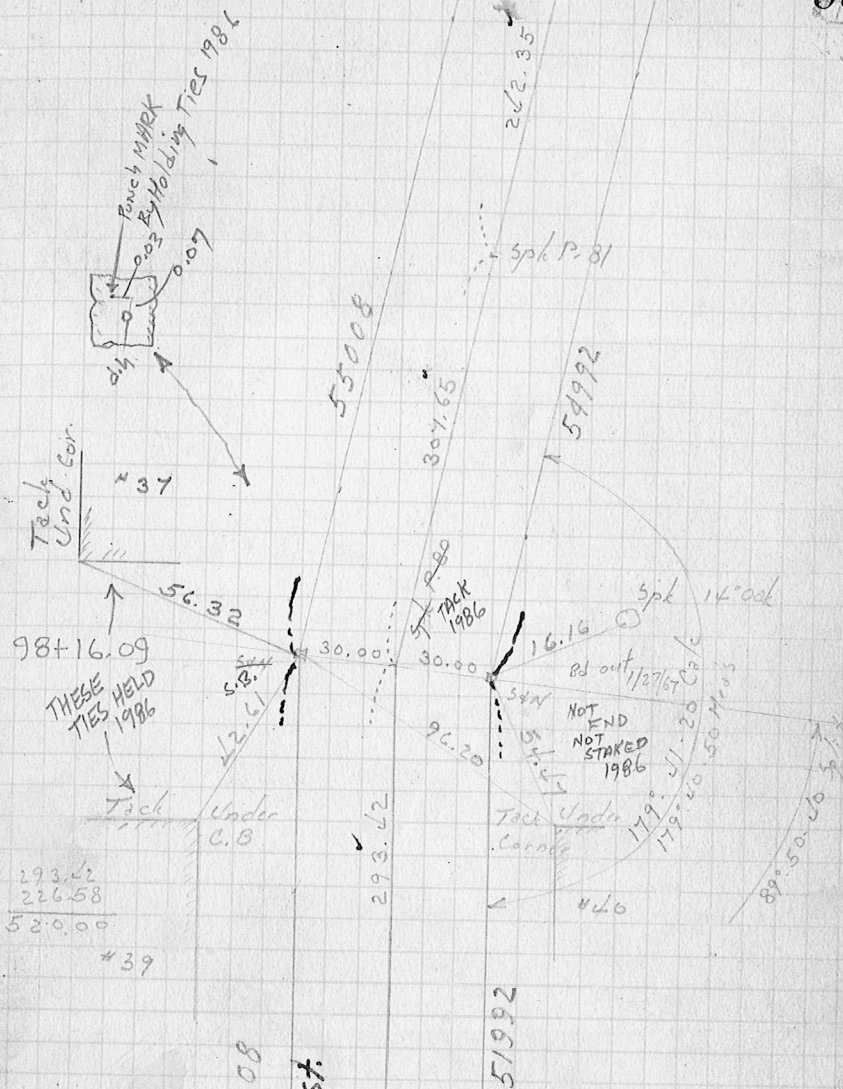
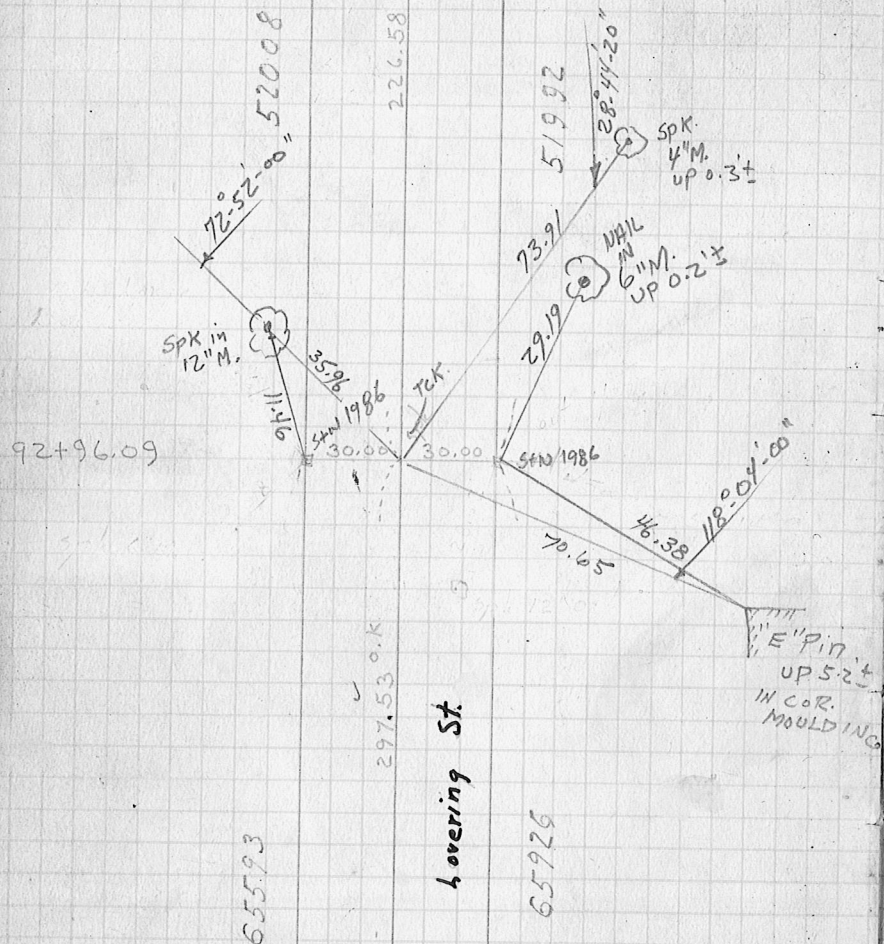
168

324.11
226.58
297.53

Medway

Layout

99



Lovering St

Lovering St

Call 357.46

358.37

377.50
226.58
520.00

Spk P. 82

Spk P. 82

293.42
226.58
520.00

#39

293.42

52008

51992

65926

65593

181.17

100, Lovering
168

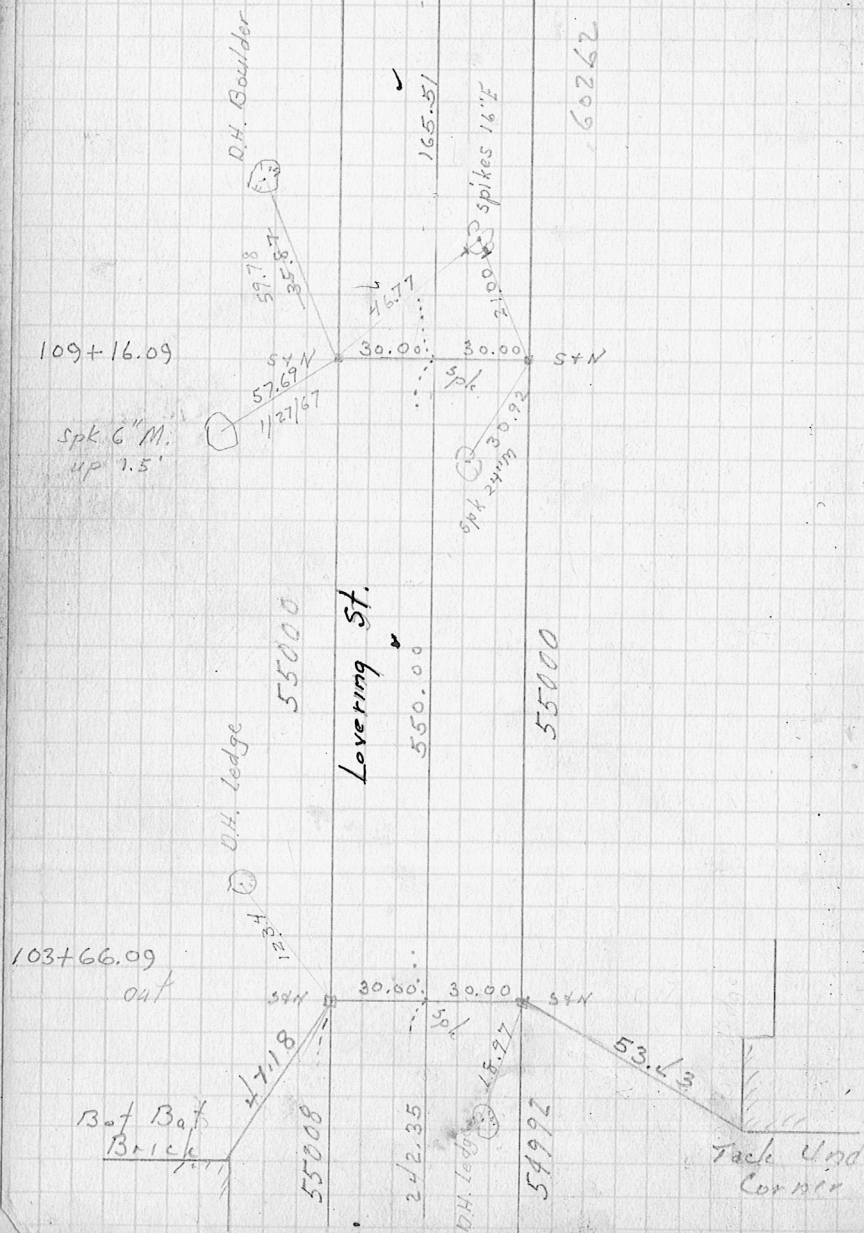
St.

Pg 102

Medway

Layout

May 1953 101



Intersection of Lovering St.
with Edison High Tension Line

Medway

Aug 28, 1953.

(See Page 88 for Layout)

(See E.E.I. Print in Envelope 344)

Old Lovering St.

Proposed

Cut-off

1548.17

$\phi T = 276.87$

D.H. in Ledge

42-04-30.2
126-14
42-04-40

Conc Bd
(Lead Plug)

Edison High Tension

Conc Bd (Lead Plug)

$\phi P.I. StN$

$\phi T = 276.87$

StN

14.42

spk

Lovering St.

42.24

24.07

D.H. in Ledge
also π tie

106

168

Sept. 18, 1953

Spk 10¹¹ A

0/d
DH. top wall

Partridge St.

D.H. conc
walk
(old tie)

Lovering St.

Additional Detail Lowering St.

107

July 26, 1955

$$92 + 96.09$$

set up 95-

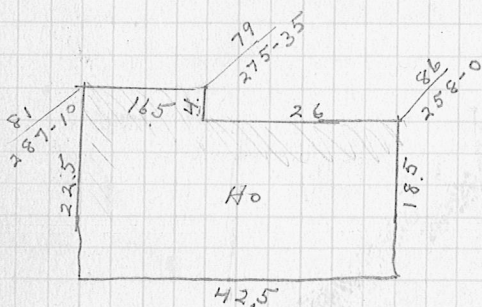
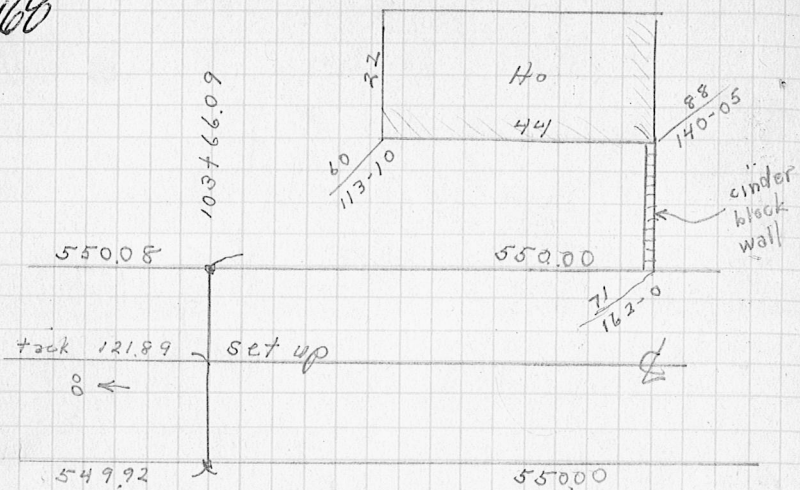
Plotted

Gar with No 37

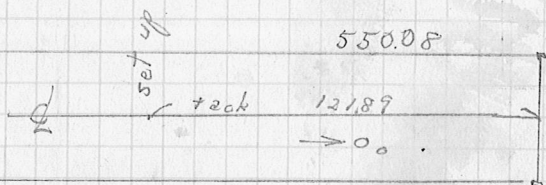
608 4

Angle
set up
 $98 + 16.09$

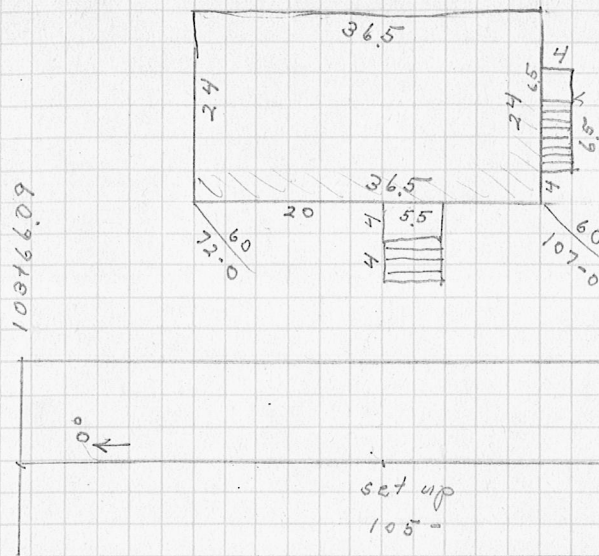
Plotted



Plotted



Plotted



Plotted

110/168
Lovering St.

Medway Layout

Oct 1953 111



112

Lovering St. Medway

Partridge

St.

spl 12" Pear Layout

Oct. 1963 113

168

Vert. spl
24" E/m(1964)
21.87
22.97
22.97
(1964)(1964)
24.48
24.59

spl 20" Ash

spl 20" Ash
10.41
10.41
10.41

32.55

See P. 111
For Tiesspl P. 6
N = 34° 37' 48"spl
2.79
54Nspl
2.20
54Nspl
1.90
54Nspl
1.04
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54Nspl
1.26
54N $\Delta = 44^\circ 17' - 10' \checkmark$ o.k.
 $\angle R = 80.00 \checkmark$
 $\angle T = 32.55 \checkmark$

#128

METAL
C.B.S.B. Fnd
(2001)

41.15

SPK #69
O.V.P.(2001)
S.B. Fnd

20.00

47.18
Old WaySee P. 110
173.12

54N See P. 110

 $\Delta = 84^\circ 10' - 40' \checkmark$ Turned
 $\angle R = 50.00 \checkmark$
 $\angle T = 45.16 \checkmark$

30H ledge

spl 18" Apple

37.01

D.H.
Bedstone

54N

20.00

54N

7.00

spl

13.00

54N

39.58

Stone Steps
To Barnspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" AshLovering St.
Old Way

46.16

19.32

30.12

30.12

7.00

54N

13.00

54N

39.58

spl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
36" Ashspl
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36" Ashspl
36" Ash $\Delta = 51^\circ 32' - 10' \checkmark$ o.k.
 $\angle R = 16.0 \checkmark$
 $\angle T = 77.24 \checkmark$

116
168

Lowering St. Medway

+5.47

279.61 ✓
N

117

X Sections

March 1953

274.14 Chisel Sq. ledge @ Summer St.
N.B. 167 19.56 + N.B. 102 19.132

-2.07

277.54 ✓ D.H. Cor. Walls NB 167/56 (277.54)

0+00 Lowering St. 2.1 277.5

	Top	@Wall	E	E.T.W	E	@Wall	Top												
0+50	70	60	42	25	24	23	12	13	0	10	19	23	24.5	26	44	60	70		
	5.3	5.0	4.9	4.6	1.9	4.0	4.9	4.4	4.0	4.2	5.4	4.8	2.3	4.5	4.9	5.1	5.2		
	274.3	274.6	274.7	275.0	277.7	275.6	274.7	275.2	275.6	275.4	274.2	274.8	277.3	275.1	274.7	274.5	274.4		
						Top	@Wall	E	E.T.W	E	@Wall	Top							
1+0	60	50	30	23	22	21	15	9	7	0	2	10	20	25	27	30	50	60	
	6.1	6.2	6.0	5.7	3.0	5.5	6.5	4.6	4.8	4.6	4.6	4.7	6.0	5.8	4.6	6.1	6.1	6.3	
	273.5	273.4	273.6	273.9	276.6	274.1	273.1	275.0	274.8	275.0	275.0	274.9	273.6	273.8	275.0	273.5	273.5	273.3	
						Top	@Wall	E	E.T.W	E	@Wall	Top							
1+50	50	30	21	19	17	14	7	4	0	2	11	24	27	30	32	36	40	50	
	6.5	6.2	6.1	4.8	6.0	7.0	5.1	5.4	5.4	5.4	5.4	6.4	6.2	5.1	6.4	7.4	7.0	6.9	
	273.1	273.4	273.5	274.8	273.6	272.6	274.5	274.2	274.2	274.2	274.2	273.2	273.4	274.5	273.2	272.2	272.6	272.7	
						Top	@Wall	E	E.T.W	E	@Wall	Top							
2+0	60	50	30	20	18	16	11	4	0	3	12	21	27	30	32	36	40	50	
	7.1	7.0	6.5	6.3	5.3	7.5	7.3	6.3	6.3	6.2	6.4	7.2	6.8	6.1	7.2	7.5	7.4		
	272.5	272.6	273.1	273.3	274.3	272.1	272.3	273.3	273.3	273.4	273.2	272.4	272.8	273.5	272.4	272.1	272.2		
						Top	@Wall	E	E.T.W	E.Tar	Remains								
2+50	60	50	30	17	16	15	9	3	0	5	22	30	50	60					
	7.7	7.6	7.3	7.2	5.6	7.1	7.9	7.1	7.1	7.0	7.3	7.0	7.8	7.8					
	271.9	272.0	272.3	272.4	274.0	272.5	271.7	272.5	272.5	272.6	272.3	272.6	271.8	271.8					
						E.T.W.	E												
2+50 Tar Drive Rt. Ask.	0	5	11	30	7.1	7.0	7.2	7.1	50	75	100								
	272.5	272.6	272.4	272.5	272.1	271.9	271.6												

+2.61

275.21 ✓
N

-7.01

272.60 ✓

T.P. Stone

	E	E.T.W	E																
3+0	60	50	30	17	10	5	1	0	6	14	30	50	60						
	4.2	4.2	4.1	3.7	4.1	3.2	3.8	3.8	3.7	3.7	3.7	3.9	4.2						
	271.0	271.0	271.1	271.5	271.1	272.0	271.4	271.4	271.5	271.5	271.3	271.3	271.0						

checked G.V.C.

	60	50	30	15	Topo	0	@Wall	
3450	<u>5.3</u>	<u>5.2</u>	<u>5.1</u>	<u>4.7</u>	<u>14</u>	0	<u>12</u>	<u>8</u>
	5.3	5.2	5.1	4.7	31	8	4.8	5.7
269.9	270.0	270.1	270.5	272.1		270.4	269.5	270.6
				E	E.T.W	E@Walk	Walk	
				<u>0</u>	<u>8</u>	<u>17</u>	<u>17</u>	
3475 Conc. Walk Rt.				5.6	5.4	5.4	5.23	
				267.6	269.8	269.8	269.98	
3475 68' Rt. Sill House				2.91	272.30			

3+80 64' Rt. B.M. L.O.C. Conc. P₂/form -3.15 272.06 ✓

	60	50	30	14	Top	12	8	3
440	6.1	6.4	6.4	6.3	5.7	5.8	8.0	6.5
	269.1	268.8	268.8	268.9	267.5	267.4	267.2	268.7
				E	E.T.W	E		
440 Tor Drive Rt.			0	2	7	18	30	50
			7.1	9.3	9.0	8.9	8.5	7.6
	266.1	265.9	266.2	266.3	266.7	267.6		

	$\frac{60}{8.9}$	$\frac{50}{8.9}$	$\frac{30}{8.9}$	$\frac{8}{8.6}$	} $\frac{8}{10.9}$	$\frac{6}{11.0}$
4.50	266.3	266.3	266.3	266.6		264.3

$$+ 1,46 \quad 269.67 \checkmark$$

	$\frac{60}{7.1}$	$\frac{50}{7.0}$	$\frac{30}{6.6}$	$\frac{15}{6.4}$	$\frac{Top}{7}$	} @ Wall	$\frac{7}{8.3}$	$\frac{4}{7.6}$	$\frac{0}{7.5}$
540	262.6	262.7	263.1	263.3	263.5		261.4	262.1	262.2

	60	50	30	Top 5	@ Wall	0
5+50	10.6	10.6	10.3	9.6	11.5	10.1
	259.1	259.1	257.4	260.1	258.2	259.6

$$+ 0.79 \quad 263.21$$

	Top		PW		
670	$\frac{60}{6.5}$	$\frac{50}{6.6}$	$\frac{30}{6.4}$	$\frac{6}{5.9}$	
	256.7	256.6	256.6	257.3	
				258.8	
					256.9

E	E.T.W	E			
<u>0</u>	<u>8</u>	<u>15</u>	<u>30</u>	<u>50</u>	<u>60</u>
5.0	4.8	4.9	4.7	4.3	4.1
270.2	270.4	270.3	270.5	270.9	271.1

30	50	62	62	64
5.05	4.63	4.21	3.85	3.20
270.16	270.58	271.00	271.36	272.01

(272.04) N.B. 157/56

E	ET, W	E			
$\frac{0}{7.0}$	$\frac{8}{6.5}$	$\frac{16}{6.5}$	$\frac{30}{6.1}$	$\frac{50}{5.5}$	$\frac{60}{4.7}$
268.2	268.7	268.7	269.1	269.7	270.5

$$\begin{array}{r} 75 \\ \hline 6.4 \\ 268.8 \end{array} \quad \begin{array}{r} 100 \\ \hline 5.9 \\ 269.3 \end{array}$$

<u>0</u>	<u>2</u>	<u>9</u>	<u>26</u>	<u>30</u>	<u>32</u>	<u>35</u>	<u>50</u>	<u>60</u>
10.0	9.9	9.8	9.8	8.9	7.5	8.7	9.4	8.8
265.2	265.3	265.4	265.4	266.3	267.7	266.5	265.8	266.4

- 7.00 268.21 ✓ T.P. Stone on Wall

F	PTW	F	CHall	Top			
<u>2</u>	<u>9</u>	<u>18</u>	<u>29</u>	{ <u>30</u>	<u>33</u>	<u>50</u>	<u>60</u>
7.7	7.5	7.7	7.3	{ 5.2	6.2	6.3	6.2
262.0	262.2	262.0	262.4	264.5	263.3	263.4	263.5

E	E.T.W	E	E	E	E	E	E
2	10	18	24	28	30	31	50
10.2	10.1	10.4	10.9	10.6	8.0	9.8	10.0
259.5	259.6	259.3	258.8	259.1	261.7	259.9	259.7

- 7.25 262.42 ✓ T.P. Vert Spk in stump 5740 28'R.

	E	± T.W.	F	@ Wall	Top										
0	3	11	19	25	29	8	30	37	50	60					
6.0	6.0	5.8	6.1	6.7	6.0	8	4.0	6.1	6.8	6.8					
257.2	257.2	257.4	257.1	256.5	257.2	257.2	257.1	256.4	256.4	256.4					

Checked G. W. C.

120
R1/168

	60	50	30	8	Top	@Wall	
6/50	8.6	8.9	8.9	7.7	6.7	8.1	8.1
	254.6	254.3	254.3	255.5	256.5	255.1	255.1

	60	50	30	21	0
7/50	10.3	10.5	10.7	10.9	9.6
	252.9	252.7	252.5	252.3	253.6

+ 1.65 256.01 ✓

	60	50	30	6	Top	@Wall	
7/50	4.1	4.3	4.5	4.1	2.5	4.2	3.9
	251.9	251.7	251.5	251.9	253.5	251.8	252.1

	60	50	30	17	7	Top	@Wall	
8/50	4.7	5.0	5.2	5.3	4.3	3.8	4.8	4.9
	251.3	251.0	250.8	250.7	251.7	252.2	251.2	251.1

8436 3' Lt. Drop Inlet.
 Conc. Cap Stone
 Rough Stone Inlet
 Inv. 12" Conc. Pipe

8446 23' Rt. Drop Inlet
 Conc. Cap Stone
 Rough Stone Inlet
 (Other End Conc. Pipe Above) Inv. 12" Corr. Iron Pipe
 Inv. 10" Conc. Pipe

	60	50	30	15	11	8	Top	@Wall	
8450	6.0	6.4	6.0	5.4	5.6	4.6	4.2	5.5	5.8
	250.0	249.6	250.0	250.6	250.4	251.4	251.8	250.5	250.2

8464 126' Lt. B.M. Chisel Sq. ledge outcrop

	60	50	30	15	8	Top	@Wall	
9/50	8.0	7.8	7.7	7.4	6.6	5.6	6.7	7.7
	248.0	248.2	248.3	248.6	247.4	250.4	247.3	248.3

121

E	±T.W.	E	@Wall	Top	30	50	60
3	11	19	28	29	30	50	60
8.0	7.7	7.9	8.7	7.0	8.3	9.2	9.3
255.2	255.5	255.3	254.5	256.2	254.9	254.0	253.9

E	±T.W.	E	@Wall	Top	30	50	60
3	11	19	27	29	30	50	60
9.5	9.3	9.4	10.3	8.7	10.1	11.3	11.8
253.7	253.9	253.8	252.9	254.5	253.1	251.9	251.4

- 8.85

254.36 ✓ T.P. Stone in Wall

E	±T.W.	E	@Wall	Top	30	50	60
2	11	19	27	38	30	50	60
3.5	3.2	3.5	4.3	22	4.1	5.4	5.6
252.5	252.8	252.5	251.7	253.8	251.9	250.6	250.4

E	±T.W.	E	@Wall	Top	30	50	60
3	11	19	29	30	31	50	60
4.9	4.6	4.9	5.4	3.3	5.5	6.3	6.5
251.1	251.4	251.1	250.6	252.7	250.5	249.7	249.5

5.88 250.13
 7.01 249.00
 8.20 247.81

6.28 249.73
 7.22 248.79
 8.75 247.26
 8.75 247.26

E	±T.W.	E	@Wall	Top	30	50	60
3	11	19	27	29	30	50	60
6.2	5.9	6.2	6.2	3.9	5.7	6.8	7.0
249.8	250.1	249.8	249.8	252.1	250.3	249.2	249.0

- 4.28 251.73 ✓ (251.73)

E	±T.W.	E	@Wall	Top	30	35	50	60
3	11	19	27	29	30	35	50	60
8.8	8.6	8.9	7.7	5.0	7.1	7.6	6.9	6.9
247.2	247.4	247.1	248.3	251.0	248.9	248.4	249.1	249.1

Checked G.N.C.

	60	45	30	15	7	Top	@Wall	
9+50	13.5	12.6	11.5	10.5	9.8	8.6	10.2	11.7
	242.5	243.4	244.5	245.5	246.2	247.4	245.8	244.3

+ 0.19

247.44
K

	60	50	30	29	11	8	Top	@Wall	
10+0	8.2	8.1	8.7	7.8	7.7	7.0	6.6	6.8	7.0
	239.2	239.3	238.7	239.6	239.7	240.4	244.8	240.6	240.4

10+26 24' Rt. Inv. 10" Conc. Pipe 10.28 237.16

	60	50	30	9	6	Top	@Wall	E
10+50	7.6	9.8	10.0	7.7	8.0	9.2	9.2	9.5
	237.8	237.6	237.4	237.7	239.4	238.2	238.2	237.9

	60	50	30	10	7	Top	@Wall	E
11+0	11.5	11.7	11.6	11.7	9.4	11.3	11.0	11.2
	235.9	235.7	235.8	235.7	238.0	236.1	236.4	236.2

219 240.05
K

237.86

	60	50	30	10	7.5	Top	@Wall	E
11+7	6.8	6.4	5.9	5.2	3.3	4.6	3.4	5.5
	233.3	233.7	234.2	234.9	236.0	235.5	234.7	234.6

568

237.84
K

7.89 232.16

	60	50	30	11	9	Top	@Wall	E
12-0	5.5	5.2	5.0	4.0	2.0	4.1	4.6	4.6
	232.3	232.6	232.8	233.8	235.8	233.7	233.2	233.2

	60	50	30	11	9	Top	@Wall	E
12+0	6.7	6.6	6.3	5.4	4.2	5.7	5.9	5.9
	231.1	231.2	231.5	232.4	233.6	232.1	231.9	

E	@T.W.	E	@Wall	Top					
2	11	19	24	26	28	29	30	50	60
12.3	12.4	12.4	11.6	10.4	8.3	9.5	9.4	9.1	9.0
243.7	243.6	243.6	244.4	245.6	247.7	246.5	246.6	246.9	247.0

- 8.76

247.25 T.P. Stone on Wall

E	@T.W.	E	@Wall	Top					
3	10	19	23	28	29	30	50	60	
7.3	7.1	7.1	6.7	5.9	3.5	5.5	5.1	3.6	
240.1	240.3	240.3	240.7	241.5	243.9	241.9	242.3	243.8	

@T.W.	E	@Wall	Top						
11	19	23	25	26	29	30	32	50	60
9.3	9.4	9.5	10.9	9.8	9.3	7.1	9.6	9.5	8.6
238.1	238.0	237.9	236.5	237.6	238.1	240.3	237.8	237.9	238.8

@T.W.	E	@Wall	Top						
10	20	23	24	26	30	32	33	50	60
11.1	11.2	11.8	12.3	11.4	10.9	9.1	11.1	11.0	11.1
236.3	236.2	235.6	235.1	236.0	236.5	238.3	236.3	236.4	236.3

- 9.58

237.86 T.P. Stone in Wall still - Rt.
checked G.N.C.

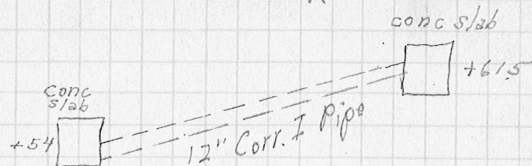
@T.W.	E	@Wall	Top						
10	20	23	24	26	30	31	33	50	60
5.3	5.5	5.7	6.5	5.0	4.6	3.1	4.6	5.1	5.3
234.8	234.6	234.4	233.6	235.1	235.5	237.0	235.5	235.0	234.8

T.P. conc 8/ab

@T.W.	E	@Wall	Top						
10	18	21	23	36	29	30	31	50	60
4.4	4.5	4.9	5.3	4.0	3.6	1.4	3.6	4.3	4.4
233.4	233.3	232.9	232.5	233.8	234.2	236.4	234.2	233.5	233.4

@T.W.	E	@Wall	Top						
9	17	21	22	23	29	30	31	50	60
5.6	5.9	6.5	7.0	5.8	5.4	3.4	4.6	6.0	6.1
232.2	231.9	231.3	230.8	232.0	232.4	234.4	233.2	231.8	231.7

2/17/53 A.T.



12+54	2' Lt. Flow	8.22	229.62
12+61.5	21' Rt	8.52	229.32
12+54	Top Conc Slab	5.86	231.98
12+65	" " "	5.80	232.04

13-	60	50	30	10	1	0	E
	7.3	6.9	6.7	7.1	6.7	6.7	
	230.5	230.9	231.1	230.7	231.1	231.1	

13+33	± Dirt Drive Rt. askew.	0	7	15	ΔTW	E
		7.7	7.6	7.8		
		230.1	230.2	230.0		

13+	60	50	30	11	10	top	@ wall	E	
	9.5	9.1	9.1	7.9	7.2			8	0
	228.3	228.7	228.7	229.9	230.6			7.8	8.4
		114		232.16				8.2	8.2
								230.0	229.4
								6.82	231.02

14-	60	50	30	11	10	Top	@ wall	E	
	4.7	4.5	4.4	3.5	2.0			8	4
	227.5	227.7	227.8	228.7	230.2			4.1	4.5
								4.4	4.4
								228.1	227.7
								227.8	227.8

14+	60	50	30	13	11	top	@ wall	E	
	6.9	6.4	6.4	5.7	4.0			9	5
	225.3	225.8	225.8	226.5	228.2			6.6	6.9
								6.8	6.8
								225.6	226.3
								225.4	225.4

14+87	± Dirt Drive Rt. askew.	0	3	ΔTW	E
		8.9	8.7		
		223.3	223.5		

14+84 Rt. 105 Sill Ho. 258 229.58

14+84 Rt. 105 check BM L.O.C. stone plot

744 8m

ΔTW.	E	@ wall	Top						
7	16	28	29	30	50	60			
6.6	6.9	6.8	4.6	6.1	6.8	6.9			
231.2	230.9	231.0	233.2	231.7	231.0	230.9			

30	50	60	100
7.6	7.4	7.5	8.0
230.2	230.4	230.3	229.8

ΔTW.	E						
5	13	20	30	50	60		
8.1	8.3	7.7	7.4	7.6	7.8		
229.7	229.5	230.1	230.4	230.2	230.0		

T.O. Boulder

ΔTW.	E						
5	12	30	50	60			
4.2	4.3	3.9	4.0	3.7			
228.0	227.9	228.3	228.2	228.5			

ΔTW.	E						
3	11	30	50	60			
6.8	6.8	5.5	5.3	5.1			
225.4	225.4	226.7	226.9	227.1			

ΔTW.	E						
11	30	50	60	100			
8.6	7.5	5.8	5.4	4.1			
223.6	224.7	226.4	226.8	228.1			

126/168

15-	60	50	30	14	13	8	10	6	0
	9.6	7.1	8.6	7.8	7.1	8	9.4	10.0	9.7
	222.6	223.1	223.6	224.4	225.1		222.8	222.2	222.5
	2.53		223.83		10.86		221.30		

15+	60	50	30	17	15	8	14	9	1	0
	8.9	8.1	6.8	5.5	4.5	8	4.5	4.2	3.9	3.9
	214.9	215.7	217.0	218.3	219.3		219.3	219.6	219.9	219.9

16-	60	50	30	20	12	3	0			
	11.5	11.4	9.3	5.5	5.2	5.1	5.2			
	212.3	212.4	214.5	218.3	218.6	218.7	218.6			

16+	33	30	27	20	20	14	6			
	11.7	11.0	8.8	7.6	5.8	5.8	5.7			
	212.1	212.8	215.0	216.2	218.0	218.0	218.1			

16+80 Bridge Opening

Bot Brook	Waterland	Bot Conc.	on Conc.	@ conc	E	ETW				
19	19	19	18	18	15	8	2			
14.8	11.66	8.21	5.32	5.2	5.9	5.8	6.0			
209.0	212.17	215.62	218.51	218.2	217.9	218.0	217.8			

17-	32	30	23	23	17	8				
	11.6	10.7	7.4	6.0	6.0	5.9				
	212.2	213.1	216.4	217.8	217.8	217.9	217.7	217.8		

16+86.5 Lt. 20 check chis. End 325 218.58

4.41 222.96 218.53

17+	60	50	35	30	28	18	8			
	11.0	10.6	10.2	7.1	5.7	5.3	5.3			
	212.0	212.4	212.8	215.9	217.3	217.7	217.7			

18-	60	40	34	30	18	8				
	9.9	8.2	5.5	5.3	5.1	5.2				
	213.1	214.8	217.5	217.7	217.9	217.8	217.6	218.1	213.0	211.8

18+28	60	50	30	25	11	0				
	9.8	8.2	4.1	4.4	4.6	5.2				
	222.2	220.3	219.8	218.9	218.6	218.4	217.8			

Dirt Drive Lt askew.

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ETW.	E									
2	7	15	17	30	50	60				
9.7	10.1	7.8	8.9	7.9	7.3	7.5				
222.5	222.1	222.4	223.3	224.3	224.9	224.7				

T.O. in wall

E	@ Rem									
7	13	0	15	18	30	50	60			
4.0	4.4	0	4.2	4.8	4.4	4.4	4.1			
219.8	219.4		219.6	219.0	219.4	219.4	219.7			

E	@ wall	top								
4	12	13	14	30	50	60				
5.4	5.9	5.6	7.6	8.8	8.6	8.2				
218.4	217.9	218.2	216.2	215.0	215.2	215.6				

E	@ Conc.	On Conc	Bot Conc.	In Marsh						
0	1	5	10	10	30	50	60			
6.0	5.9	5.4	6.5	9.9	11.5	11.8	12.1			
217.8	217.9	218.4	217.3	213.9	212.3	212.0	211.7			

@ Conc.	On Conc	Bot Conc.	Bot Brook				
1	3	3	4	4			
6.0	5.4	5.25	8.21	11.66	14.0		
217.8	218.4	218.58	215.62	212.17	209.8		

E	top	In water					
0	3	9	9				
6.1	6.0	6.3	13.3				
217.7	217.8	217.5	210.5				

See BK 188 P. 32
for Profile brook

(218.55) chis

E	Marsh						
0	4	16	30	30	60		
5.6	5.4	10.7	11.4	10.9	11.1		
217.4	217.6	212.3	211.6	212.1	211.9		

E	ETW	E					
0	6	14	30	50	60		
5.4	4.9	10.0	11.2	11.0	11.3		
217.6	218.1	213.0	211.8	212.0	211.7		

E	ETW	E					
0	2.7	3.2	4.1	4.4	4.6	5.2	
222.2	220.3	219.8	218.9	218.6	218.4	217.8	

DHE

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222.96 ✓

E @ 2 Drive E.T.W. E

18+	60	50	30	18	10	0
	3.0	4.0	3.8	4.4	4.3	4.7
	220.0	219.0	219.2	218.6	218.7	218.3

19-	60	50	30	17	9	0
	0.9	1.2	2.2	3.6	3.4	3.8
	222.1	221.8	220.8	219.4	219.6	219.2

4.77

227.39 ✓

0.34

222.62 ✓

Jct 2 drives

19+45 ± Dirt Drive Lt. askew.

8.8

5.3

221.9

19+	60	50	33	30	23	19	10	0
	1.4	1.2	1.0	2.9	5.8	6.1	5.7	6.0
	226.0	226.2	226.4	224.5	221.6	221.3	221.7	221.4

20-	60	50	30	25	18	10	1	0
	1.4	1.1	1.0	2.3	3.3	3.2	3.4	3.4
	226.0	226.3	226.4	225.1	224.1	224.2	224.0	224.0

20+	60	50	30	20	10	2	0
	2.6	2.5	2.0	2.1	1.9	2.3	2.2
	224.8	224.9	225.4	225.3	225.5	225.1	225.2

20+55 ± Dirt Drive Lt. sqd.

End

100

2.6

224.8

4.48

230.94 ✓

0.93

226.46 ✓

20+90

Lt. 8'sill Button's House

0.75 227.19

21-	60	50	30	25	20	11	4	0
	5.8	5.1	4.0	4.8	5.1	4.9	5.1	4.8
	225.1	225.8	226.9	226.1	225.8	226.0	225.8	226.1

21+	60	50	32	30	21	12	4	0
	4.5	4.3	4.7	4.6	5.4	5.2	5.5	6.3
	226.4	226.6	226.7	228.1	226.3	225.5	225.7	225.4

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4	15	30	50	60
4.6	8.7	9.3	10.4	10.4
218.4	214.3	213.7	212.6	212.6

10	30	50	60
5.6	6.7	7.2	7.5
217.4	216.3	215.8	215.5

T.P. opt Pole *82 Lt

60	50	30	23	11	0
5.9	6.2	6.7	6.7	6.1	6.0
221.5	221.2	220.7	220.7	221.3	221.4

5	10	15	23	30	36	41	50	60
6.1	7.6	7.8	10.7	11.3	11.1	9.4	10.3	11.6
221.3	219.8	219.6	216.7	216.1	216.3	218.0	217.1	215.8

10	17	30	50	60
4.2	4.3	11.5	11.9	11.0
223.2	223.1	215.9	215.5	216.4

10	16	17	18	30	50	60
4.6	3.5	2.5	3.8	3.8	3.9	4.0
222.8	223.9	224.9	223.6	223.6	223.5	223.4

60	50	30	20	10	2	0
2.7	2.7	2.4	2.1	1.9	2.3	2.3
224.7	224.7	225.0	225.3	225.5	225.1	225.1

T.P. stone in wall

10	13	19	28	30	50	60
5.5	4.3	4.8	5.7	6.0	7.7	8.3
225.4	226.6	226.1	225.2	224.9	223.2	222.6

2	6	13	14	16	30	50	60
7.3	7.0	6.3	6.0	6.7	8.1	9.6	10.5
223.6	223.9	224.6	224.9	224.2	222.8	221.3	220.4

DHE ✓

130/68

230.94 ✓

T

WS
131

22-	60	50	30	E	ΔTW	E		5	8	@ wall	top	14	15	20	30	50	60
	5.3	5.1	5.4	5.6	5.6	5.8	6.5	7.9	7.3	6.2	5.8	6.3	7.4	8.6	11.1	12.2	
	225.6	225.8	225.5	225.3	225.3	225.1	224.4	223.0	223.6	224.7	225.1	224.6	223.5	222.3	219.8	218.7	
22+	60	50	30	top	@ wall	E	ΔTW	E	@ Rem.	top	14	15	30	50	60		
	5.2	4.9	4.9	4.5	6.1	6.4	6.2	6.6	7.0	9.7	9.0	10.0	11.9	12.3	12.4		
	225.7	226.0	226.0	226.4	224.8	224.5	224.7	224.3	223.9	221.2	221.9	220.9	219.0	218.6	218.5		

3.81

228.50 ✓
T

6.25 224.69

T.P. spk. Pole # 79 Lt.

23-	60	50	30	top	@ wall	E	ΔTW	E	@ Rem.	top	14	15	30	50	60		
	2.5	2.3	2.0	1.6	4.0	4.8	4.6	4.8	4.8	7.7	7.4	8.0	9.1	7.3	6.4		
	226.0	226.2	226.5	226.9	224.5	223.7	223.9	223.7	223.7	220.8	221.1	220.5	219.4	221.2	222.1		
			3.85	228.54 ✓		224.69 ✓											
				T													

T.P. above

23+	60	40	30	Top	@ wall	E	ΔTW	E	@ wall	top	13	14	30	40	60		
	4.0	4.0	3.8	3.1	3.0	3.3	1.3	6	0	5	8	11	13	14	30	40	60
	224.5	224.5	224.9	222.7	223.2	223.4	223.1	222.8	222.1	220.3	222.2	223.1	222.1	223.2	223.9	224.9	

23+68 Rt. 4 Flow 12" Conc Pipe 8.94 219.60

23+92 Lt. 28 " " " " 8.72 219.86

24-	60	40	3.4	Top	@ wall	E	ΔTW	E	@ wall	Top	13	14	30	40	60					
	7.0	7.0	7.0	3.3	3.2	3.0	2.3	1.3	6	0	8	12	5.6	7.2	6.6	5.4	6.5	5.9	5.5	4.3
	221.5	221.5	221.5	222.4	222.3	222.6	223.2	223.4	223.2	222.9	221.3	221.9	223.1	222.0	222.6	223.0	224.2			

24+	60	40	3.1 <th>Top</th> <th>@ wall</th> <th>E</th> <th>ΔTW</th> <th>E</th> <th>@ wall</th> <th>top</th> <th>12</th> <th>13</th> <th>14</th> <th>30</th> <th>40</th> <th>60</th>	Top	@ wall	E	ΔTW	E	@ wall	top	12	13	14	30	40	60
	3.1	2.6	2.5	3.1	3.0	2.4	1.5	6	0	5	12	13	14	30	40	60
	225.4	225.9	226.0	224.8	223.8	224.0	223.8	223.8	223.8	223.3	224.2	225.4	224.0	223.0	222.4	222.8

25-	60	50	3.8	top	@ wall	E	ΔTW	E	@ wall	top	11	13	14	30	40	60		
	1.5	0.8	0.5	2.2	3.4	3.0	2.5	1.5	7	0	6	8	11	13	14	30	40	60
	227.0	227.7	228.0	226.3	224.8	224.0	224.4	224.9	224.8	224.7	224.5	225.6	227.2	227.4	226.9	225.9	225.5	224.9

4.38

229.66 ✓
T

3.26

225.28 ✓

T.P. Boulder

DNE ✓

132/168

229.66 ✓
N

	60	40	35	30	E	ETW
	1.7	1.7	5.1	5.0	4.8	4.5
2280	228.0	228.6	224.6	229.7	229.9	225.2

	60	40	37	30	E	ETW
	1.6	1.5	6.1	7.0	6.5	6.3
2281	228.1	228.2	223.6	222.7	223.2	223.4

	60	40	30	E	ETW
	4.2	6.8	7.3	7.8	7.6
225.5	225.5	222.9	222.4	221.9	222.1

5.77 227.10 ✓
N 8.33 221.33 ✓

28+68 Lt. 210 3.39 223.71

26+89	Rt 3	Flow 14" V.C. Pipe	10.28	216.82
"		Top Stone Header	7.48	212.62
"	Rt 10	Brook	10.0	212.1
26+91	Lt. 35	Flow 12" Conc Pipe	9.78	217.32
"		Top Stone Header	6.70	220.4
"	Lt 10	In Marsh	9.8	212.3

				top	@ wall			ETW.
27-	60	50	37	34	33	30	26	17
	9.5	9.3	8.6	5.6	6.2	5.8	6.0	5.6
	217.6	217.8	218.5	221.5	220.9	221.3	221.1	221.5

	60	41	40	39	35	30	E	ETW
277	8.1	8.5	6.3	6.0	6.1	5.6	5.3	5.3
	218.0	218.6	220.8	221.1	221.0	221.5	221.8	

	70	62	61	53	44	34	30	20
	62	36	50	52	46	48	48	51
28-	220.9	223.5	222.1	221.9	222.5	222.3	222.3	222.

0.21 225.87 ✓
N 1.44 225.66

133

<u>7</u>	<u>0</u>	<u>5</u>	<u>8</u>	<u>10</u>	<u>30</u>	<u>40</u>	<u>60</u>
4.7	4.8	5.0	3.1	1.5	2.1	2.3	2.2
225.0	224.9	224.7	226.6	228.2	227.6	227.4	227.5

<u>E</u>			<u>@wall</u>	<u>top</u>					
<u>7</u>	<u>0</u>	<u>6</u>	<u>14</u>	<u>15</u>	<u>17</u>	<u>30</u>	<u>40</u>	<u>60</u>	
6.7	6.9	6.6	1.9	0.9	1.4	0.0	+0.2	+0.5	
223.0	222.8	223.1	227.8	228.8	228.3	229.7	229.9	230.2	

<u>E</u>			Bottom	Top					
<u>7</u>	<u>0</u>	<u>10</u>	<u>15</u> 0	<u>15</u>	<u>17</u>	30	40	60	
78	85	42	44 0	33	42	45	43	42	
221.9	221.2	225.5	225.3	226.4	225.5	225.2	225.4	225.5	

T.P. stone in street

Check chis □ N.B. 167 P. 56 (223.76)

<u>E</u>	<u>10</u>	<u>0</u>	<u>2</u>	<u>10</u>	<u>30</u>	<u>40</u>	<u>60</u>
5.9	7.7	9.2	9.9	11.0	11.1	11.3	
221.2	219.4	217.9	217.2	216.1	216.0	215.8	

<u>E</u>							
<u>17</u>	<u>5</u>	<u>0</u>	<u>10</u>	<u>30</u>	<u>40</u>	<u>60</u>	
55	80	9.0	9.0	9.5	10.6	10.8	
221.6	219.1	218.1	218.1	217.6	216.5	216.3	

	<u>10</u>	<u>top</u>	@wall	<u>0</u>	<u>10</u>	<u>30</u>	<u>40</u>	<u>60</u>
	4.4	3.1	4.8	6.1	7.2	8.3	9.0	9.3
222.7	224.0	222.3	221.0	219.9	218.8	218.1	217.8	

T.P. in stone wall

DHE ✓

134/100

	ET.M.	L	225.67	top	@ wall	
28+	83	74	62	52	49	30
	26	24	2.6	2.0	2.0	3.2
	223.3	223.5	223.3	223.9	223.9	222.6

29-	60	40	30	10	0	10	30	40	60
	5.5	6.3	6.8	7.8	8.0	8.2	8.7	9.2	9.6
	220.4	219.6	219.1	218.1	217.9	217.7	217.2	216.7	216.3

29+	60	40	30	10	0	10	30	40	60
	8.5	9.5	9.7	9.9	9.8	9.6	10.1	10.3	10.8
Field	217.4	216.4	216.2	216.0	216.1	216.3	215.8	215.6	215.1

30-	60	40	30	10	0	10	30	40	60
	9.3	9.9	9.9	10.2	10.2	10.4	10.6	10.5	10.6
	216.6	216.0	216.0	215.7	215.7	215.5	215.3	215.4	215.3

30+	60	40	30	10	0	10	30	40	60
	7.0	8.7	8.3	8.0	7.8	7.7	7.8	8.0	8.1
	216.9	217.2	217.6	217.9	218.1	218.2	218.1	217.9	217.8

10.44 228.99 7.32 218.55
 T.O. top & stk 30+

31-	60	40	30	10	0	10	30	40	60
	8.9	8.2	7.9	7.5	7.7	7.8	9.0	9.5	9.7
	220.1	220.8	221.1	221.5	221.3	221.2	220.0	219.5	219.3

31+	60	40	30	10	0	10	30	40	60
	4.9	3.7	3.3	3.1	3.7	4.4	6.2	6.9	7.9
	224.1	225.3	225.7	225.9	225.3	224.6	222.8	222.1	221.1

32-	60	40	30	10	0	10	30	40	60
	4.3	3.2	2.3	1.3	1.5	1.8	2.5	2.7	3.3
	224.7	225.8	226.7	227.5	227.5	227.2	226.5	226.3	225.7

32+	60	40	30	10	0	10	30	40	60
	2.6	2.2	1.8	1.2	1.1	1.0	0.8	1.2	1.3
	226.4	226.8	227.2	227.8	227.9	228.0	228.2	227.8	227.7

8.06 235.86 1.19 227.80
 T.O. top & stk 32-

33-	60	40	30	10	0	10	30	40	60
	7.3	7.2	7.1	6.6	6.3	6.2	6.2	6.8	7.1
	228.6	228.7	228.8	229.3	229.6	229.7	229.7	229.1	228.8

135

GAP

235.86 ✓

 π

33+

60	40	30	10
4.9	5.1	5.1	4.9
231.0	230.8	230.8	231.0

34-

60	40	30	10
4.3	4.3	4.3	4.4
231.6	231.6	231.6	231.5
		4.80	231.06

5.70

240.66 ✓

 π

234.96 BM

38+66 Lt 145

38+62 Lt 154

(New Sta)
(Changed 1962)

4.29

236.37 ✓

Ordered off field

chis □ Between High Tension Lines (N.G. within layout)

New B.M. chis □ on ledge in Pasture
by owner 34+ to 39- taken later

GAP

July 23, 1953.

140

236.36 ✓

 π

234.96 BM

above

34+

60	40	30	10	0	10	30	40	60
4.6	5.0	5.3	5.5	5.7	5.9	6.1	6.3	6.1
231.8	231.4	231.1	230.9	230.7	230.5	230.3	230.1	230.3

35-

60	40	30	10	0	10	30	40	60
4.7	5.3	5.7	5.5	5.7	5.6	5.7	5.6	5.7
231.7	231.1	230.7	230.9	230.7	230.8	230.7	230.8	230.7

35+

60	40	30	10	0	10	30	40	60
4.9	5.1	5.1	5.4	5.4	5.1	5.1	5.0	5.6
231.5	231.3	231.3	231.0	231.0	231.3	231.3	231.4	230.8

36-

60	40	30	10	0	10	30	40	60
5.0	5.2	5.3	5.8	5.9	5.9	5.8	6.0	7.0
231.4	231.2	231.1	230.6	230.5	230.5	230.6	229.6	229.4

36+

60	40	30	10	0	10	30	40	60
5.0	5.3	5.6	6.1	6.4	6.6	6.7	6.7	7.2
231.4	231.1	230.8	230.3	230.0	229.8	229.7	229.7	229.2

← Minah

138
110823696
A

37-

$$\begin{array}{r} 60 \\ 4.8 \\ \hline 231.6 \end{array}$$

$$\begin{array}{r} 40 \\ 5.9 \\ \hline 230.5 \end{array}$$

$$\begin{array}{r} 30 \\ 6.4 \\ \hline 230.0 \end{array}$$

$$\begin{array}{r} 10 \\ 6.5 \\ \hline 229.9 \end{array}$$

$$\begin{array}{r} 0 \\ 6.8 \\ \hline 229.6 \end{array}$$

$$\begin{array}{r} 10 \\ 6.9 \\ \hline 229.5 \end{array}$$

$$\begin{array}{r} 30 \\ 7.2 \\ \hline 229.2 \end{array}$$

$$\begin{array}{r} 40 \\ 7.5 \\ \hline 228.9 \end{array}$$

$$\begin{array}{r} 60 \\ 7.6 \\ \hline 228.8 \end{array}$$

37+

$$\begin{array}{r} 60 \\ 4.2 \\ \hline 232.2 \end{array}$$

$$\begin{array}{r} 40 \\ 4.9 \\ \hline 231.5 \end{array}$$

$$\begin{array}{r} 30 \\ 5.2 \\ \hline 231.2 \end{array}$$

$$\begin{array}{r} 10 \\ 6.1 \\ \hline 230.3 \end{array}$$

$$\begin{array}{r} 0 \\ 6.8 \\ \hline 229.6 \end{array}$$

$$\begin{array}{r} 10 \\ 7.1 \\ \hline 229.3 \end{array}$$

$$\begin{array}{r} 30 \\ 7.2 \\ \hline 229.2 \end{array}$$

$$\begin{array}{r} 40 \\ 7.3 \\ \hline 229.1 \end{array}$$

$$\begin{array}{r} 60 \\ 7.8 \\ \hline 228.6 \end{array}$$

38-

$$\begin{array}{r} 60 \\ 0.8 \\ \hline 235.6 \end{array}$$

$$\begin{array}{r} 40 \\ 1.9 \\ \hline 234.5 \end{array}$$

$$\begin{array}{r} 30 \\ 2.0 \\ \hline 234.4 \end{array}$$

$$\begin{array}{r} 10 \\ 3.0 \\ \hline 233.4 \end{array}$$

$$\begin{array}{r} 0 \\ 3.7 \\ \hline 232.7 \end{array}$$

$$\begin{array}{r} 10 \\ 4.5 \\ \hline 231.9 \end{array}$$

$$\begin{array}{r} 30 \\ 5.2 \\ \hline 231.2 \end{array}$$

$$\begin{array}{r} 40 \\ 5.2 \\ \hline 231.2 \end{array}$$

$$\begin{array}{r} 60 \\ 5.9 \\ \hline 230.5 \end{array}$$

140 234.96

BM. (234.96)

← Minah

139

38+	ETW.	E	top	@				
65	56	49	48	47	40	30		
4.7	4.9	4.8	1.6	3.3	3.3	3.9		
236.6	236.4	236.5	239.7	238.0	238.0	237.4		

100	83	84	83	73
5.4	4.7	2.8	5.3	5.0
235.9	236.6	238.5	236.0	236.3

4.33

240.70
K

236.37 B.M.

39-	top	@ wall	E	ETW	E			
75	66	65	64	52	43	36	30	27
53	4.8	2.8	4.2	4.1	3.9	3.9	4.3	5.1
235.4	235.9	237.9	236.5	236.6	236.8	236.8	236.4	235.6

39+03	LT 24'	Flow 12" Conc Pipe	7.65
39+12	LT 57'	" " " "	7.50

39+	E	ETW	E			
60	46	40	34	30	26	18
6.8	6.0	4.3	4.4	4.4	4.3	4.6
233.9	234.7	236.4	236.3	236.3	236.4	236.1

40-	top	@ wall	E	ETW	E			
60	33	32	31	30	25	21	13	6
6.8	6.2	4.5	5.9	6.2	5.1	5.1	5.0	5.2
233.9	234.5	236.2	234.8	234.5	235.6	235.6	235.7	235.5

40+	top	@ wall	E	ETW	E			
60	40	30	20	19	18	14	10	3
6.0	6.0	6.2	6.3	4.5	6.5	5.8	5.6	5.5
234.7	234.7	234.5	234.4	236.2	234.2	234.9	235.1	235.2
5.04	240.59	5.15	235.55					

41-	top	@ wall	E					
60	40	30	20	12	11	10	6	4
5.7	6.5	6.8	6.8	6.7	4.6	7.7	7.2	6.0
234.9	234.1	233.8	233.8	233.9	236.0	232.9	233.4	234.6

41+11	LT 5	Flow 12" Conc Pipe	9.09
	"	Top Stone Header	6.8

41+07	RT 23	Flow 12" Conc Pipe	9.71
		Top of wall = header	5.3

30	10	0	10	20	30	40	60
4.8	5.5	6.4	7.2	8.1	8.9	9.9	10.3
236.5	235.8	234.9	234.1	233.2	232.4	231.4	231.0

above

top	@ Ret							
26	25	10	0	10	20	30	40	60
4.8	7.2	7.4	7.4	7.2	7.5	7.7	7.7	8.0
235.9	233.5	233.3	233.3	233.5	233.2	233.0	233.0	232.7

233.05	233.20
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top	@ wall							
12	11	10	0	10	20	30	40	60
4.8	3.7	5.8	6.3	6.2	6.2	6.5	6.4	7.4
235.9	237.0	234.9	234.4	234.5	234.5	234.2	234.3	233.3

@ wall	top	bot.						
0	1	2	3	10	20	30	40	60
5.3	5.4	3.7	6.4	6.9	7.1	7.5	8.0	8.6
235.4	235.3	237.0	234.3	233.8	233.6	233.2	232.7	232.1

E						
0	5	15	30	40	60	
5.6	5.8	7.6	8.7	9.1	10.0	
235.1	234.9	233.1	232.0	231.6	230.7	

top in wall

ETW	E	@ wall	top	Bot				
0	7	14	20	21	22	30	40	60
5.7	5.5	5.7	6.0	5.1	8.4	9.4	9.6	9.9
234.9	235.1	234.9	234.3	235.5	232.2	231.2	231.0	230.7

231.50	233.8
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230.88	235.3
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Checked D.E.

112/100

240.59
K

41+	60	40	30	20	10	6	top	@ wall
	5.5	6.6	6.8	6.9	6.9	6.7	5.4	4.7
	235.1	234.0	233.8	233.7	233.7	233.9	236.3	233.9

42-	60	40	30	20	10	3	top	@ wall
	5.9	5.8	5.4	5.2	4.7	5.0	2.0	4.6
	234.7	234.8	235.2	235.4	235.9	235.6	238.6	236.0

5.95

242.03

4.51

236.08

42+	60	40	30	20	10	2	top	@ wall
	5.1	4.7	4.9	4.9	5.0	5.1	1.8	4.7
	236.9	237.3	237.1	237.1	237.0	236.9	240.2	237.3

42+72 £ Conc Drive to Garage Under 0
40
238.0

43-	60	40	30	20	10	3	top	@ wall
	6.2	5.8	5.5	5.4	4.7	4.6	2.2	4.4
	235.8	236.2	236.5	236.6	237.3	237.4	239.8	237.6

43+25± Rt 71st Sill Garneff's Ho. 4.06

1.35

242.34

240.89 BM

43+21	d Conc Drive Rt. askew	0	9
		4.5	5.4
		237.7	236.8

43+	60	40	30	20	10	2	top	@ wall
	5.3	6.6	6.1	6.0	5.8	5.5	3.1	5.9
	236.7	235.6	236.1	236.2	236.4	236.7	239.1	236.8

2.53

243.42

240.89

0	E	4TW	E	@ wall	top
5.8	5.6	5.4	5.7	6.5	4.6
234.8	235.0	235.2	234.9	234.1	236.0

E	4TW	@ wall	top
8	14	23	39
4.9	4.9	5.1	5.6
235.7	235.7	235.5	235.0

T.P. stone in st.

E	4TW	E	@ wall	top
9	16	24	29	30
5.9	5.7	6.0	5.9	4.2
236.1	236.3	236.0	236.1	237.8

E	4TW	E	@ Conc Drive	@ Gar Door
9	18	37	30	32
5.6	5.5	5.7	6.1	6.1
236.4	236.5	236.3	235.9	235.9

E	4TW	E	@ Conc Drive	@ Gar Door
8	15	24	29	30
5.5	5.2	5.6	5.6	5.0
236.5	236.8	236.4	236.4	238.2

237.97

Hor Spk 36"0 @ Cor Winthrop St

4TW	E	@ Drive	on Drive
18	30	45	60
5.2	5.6	5.7	5.8
237.0	236.6	236.5	236.4

E	4TW	E	on conc.	on conc. drive
7	16	24	30	40
5.3	5.2	5.6	5.8	5.7
236.9	237.0	236.6	236.4	236.5

B.M. above

Checked D.H.E.

144/108

243.42 ✓
7

44-

40	30	20	10	2	top	@ wall
6.5	7.3	7.9	8.1	7.8	5.6	7.0
236.9	236.1	235.5	235.3	235.6	237.8	236.4

± T.V. Winthrop

110	94	79	top	@ wall	60
3.4	3.7	4.5	7.8	7.7	4.8
240.0	239.7	238.9	241.5	239.8	238.6

44+

9	8	7	3	top	@ wall
5.9	4.4	6.7	6.6	4.3	5.4
237.5	239.0	236.7	236.8	239.1	238.0

100	83	82	60	47	40	30	26
2.1	1.8	4.1	4.4	4.2	4.3	4.7	4.7
241.3	241.6	239.3	239.0	239.2	239.1	238.7	238.7

44+66.06 ± Winthrop & Lovering Sts.

@ wall	E	± T.W.
53	40	36
4.2	4.3	4.6
239.2	239.1	238.8

75	60	57	35
1.6	2.4	2.7	2.0
241.8	241.0	240.7	241.4

30	20	14	12	@ wall	E	0
2.9	3.5	4.4	2.7	4.4	4.9	4.9
240.5	239.9	239.0	240.7	239.0	238.5	238.5

75	60	40
1.8	1.9	2.7
241.6	241.5	240.7

45+07 Bot Bot Wall Rt side

E	10	20
5.0	4.9	5.4
238.4	238.5	238.0

45+07 Top

E	10	20
5.0	4.9	5.4
238.4	238.5	238.0

145

E	± T.W.	@ wall	Top	32	40	60
8	15	23	30	5.7	8.1	9.3
6.2	6.1	6.4	6.4	5.7	8.1	9.3
237.2	237.3	237.0	237.0	237.7	235.3	234.4

75
9.3
234.1

E	± T.W.	E	@ wall	top	32	40
4	14	24	30	3.1	7.6	8.7
5.6	5.8	6.2	6.8	5.9	7.6	8.7
237.8	237.6	237.2	236.6	237.5	235.8	234.7

60	75	100
9.4	9.8	9.8
234.0	233.6	233.5

10	± T.W. Lovering	E	@ wall	top	32	40
5.4	16	25	30	3.1	7.4	8.7
238.0	237.8	237.4	237.4	238.1	236.0	234.7

60	75	100
9.1	9.7	10.8
234.3	233.7	232.6

10	20	30	40	5	60
5.1	5.4	5.8	6.3	7.0	7.3
238.3	238.0	237.6	237.1	236.4	236.1

@ wall	top	74	83	100
6.8	7.0	7.8	9.3	9.8
236.1	237.5	235.6	234.1	233.6

E	@ wall	60	75	100	125
4.2	4.8	6.0	7.5	10.0	12.5
6.0	6.3	6.7	7.5	8.5	9.4
237.8	237.4	237.1	236.7	235.9	234.9

E	@ wall	60	75	100	125
4.2	4.8	6.0	7.5	10.0	12.5
6.0	6.3	6.7	7.5	8.5	9.4
237.8	237.4	240.2	239.3	239.4	238.1

checked D.H.E.

146
100

373

24462

240.89

B.M.

P. 144

147

45+

$$\begin{array}{r} 20 \\ 3.9 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} 10 \\ 3.3 \\ \hline 241.3 \end{array}$$

$$\begin{array}{r} 3 \\ 3.3 \\ \hline 241.3 \end{array}$$

$$\begin{array}{r} \text{top} \\ 2 \\ \hline 2.8 \\ \hline 241.8 \end{array}$$

$$\begin{array}{r} @ \text{Ret} \\ 1 \\ \hline 4.9 \\ \hline 239.7 \end{array}$$

$$\begin{array}{r} 0 \\ 4.9 \\ \hline 239.7 \end{array}$$

$$\begin{array}{r} E \\ 3 \\ \hline 5.3 \\ \hline 239.3 \end{array}$$

$$\begin{array}{r} 2 \text{ TW} \\ 10 \\ \hline 5.2 \\ \hline 239.4 \end{array}$$

$$\begin{array}{r} E \\ 17 \\ \hline 5.3 \\ \hline 239.3 \end{array}$$

$$\begin{array}{r} @ \text{Ret} \\ 2.2 \\ \hline 5.2 \\ \hline 239.4 \end{array}$$

$$\begin{array}{r} \text{top} \\ 2.3 \\ \hline 5.0 \\ \hline 241.6 \end{array}$$

$$\begin{array}{r} 2.5 \\ 5.4 \\ \hline 241.2 \end{array}$$

$$\begin{array}{r} 3.0 \\ 4.0 \\ \hline 240.6 \end{array}$$

$$\begin{array}{r} 7.5 \\ 2.5 \\ \hline 242.1 \\ \hline 6.13 \end{array}$$

$$\begin{array}{r} 6.0 \\ 2.6 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 3.9 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} 3.0 \\ 3.4 \\ \hline 241.2 \end{array}$$

240.82

T.P. spk in street. & P.C.

$$\begin{array}{r} 4.0 \\ 4.3 \\ \hline 240.3 \end{array}$$

$$\begin{array}{r} 6.0 \\ 3.9 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} 7.5 \\ 5.1 \\ \hline 239.5 \end{array}$$

46-

$$\begin{array}{r} 20 \\ 5.4 \\ \hline 241.6 \end{array}$$

$$\begin{array}{r} 17 \\ 5.1 \\ \hline 241.9 \end{array}$$

$$\begin{array}{r} 13 \\ 5.8 \\ \hline 241.2 \end{array}$$

$$\begin{array}{r} \text{top} \\ 11.5 \\ \hline 4.2 \\ \hline 242.8 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 10 \\ \hline 6.5 \\ \hline 240.5 \end{array}$$

$$\begin{array}{r} E \\ 6 \\ \hline 6.3 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} 0 \\ 6.3 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} 1 \\ 6.3 \\ \hline 240.7 \end{array}$$

$$\begin{array}{r} E \\ 8 \\ \hline 6.2 \\ \hline 240.8 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 15 \\ \hline 6.9 \\ \hline 240.1 \end{array}$$

$$\begin{array}{r} \text{top} \\ 16 \\ \hline 4.3 \\ \hline 242.7 \end{array}$$

$$\begin{array}{r} 17 \\ 6.9 \\ \hline 240.1 \end{array}$$

$$\begin{array}{r} 20 \\ 7.3 \\ \hline 239.7 \end{array}$$

$$\begin{array}{r} 30 \\ 8.0 \\ \hline 239.0 \end{array}$$

$$\begin{array}{r} 40 \\ 8.1 \\ \hline 238.9 \end{array}$$

$$\begin{array}{r} 60 \\ 9.1 \\ \hline 237.9 \end{array}$$

$$\begin{array}{r} 75 \\ 9.4 \\ \hline 237.6 \end{array}$$

$$\begin{array}{r} 2.5 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 6.0 \\ 5.2 \\ \hline 241.8 \end{array}$$

$$\begin{array}{r} 4.0 \\ 5.3 \\ \hline 241.7 \end{array}$$

$$\begin{array}{r} 3.0 \\ 5.3 \\ \hline 241.7 \end{array}$$

46+

$$\begin{array}{r} 21 \\ 4.5 \\ \hline 242.5 \end{array}$$

$$\begin{array}{r} 19 \\ 2.6 \\ \hline 244.4 \end{array}$$

$$\begin{array}{r} \text{top} \\ 18 \\ \hline 5.2 \\ \hline 241.8 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 13 \\ \hline 4.9 \\ \hline 242.1 \end{array}$$

$$\begin{array}{r} E \\ 6 \\ \hline 4.8 \\ \hline 242.2 \end{array}$$

$$\begin{array}{r} 0 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} E \\ 1 \\ \hline 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 5 \\ \hline 4.9 \\ \hline 242.1 \end{array}$$

$$\begin{array}{r} \text{top} \\ 8 \\ \hline 2.4 \\ \hline 244.6 \end{array}$$

$$\begin{array}{r} 11 \\ 3.4 \\ \hline 243.6 \end{array}$$

$$\begin{array}{r} 20 \\ 3.9 \\ \hline 243.1 \end{array}$$

$$\begin{array}{r} 30 \\ 4.0 \\ \hline 243.0 \end{array}$$

$$\begin{array}{r} 40 \\ 4.3 \\ \hline 242.7 \end{array}$$

$$\begin{array}{r} 60 \\ 4.5 \\ \hline 242.5 \end{array}$$

$$\begin{array}{r} 6.0 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 3.0 \\ 4.3 \\ \hline 242.7 \end{array}$$

$$\begin{array}{r} 6.0 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 5.0 \\ \hline 242.0 \end{array}$$

$$\begin{array}{r} 3.0 \\ 4.3 \\ \hline 242.7 \end{array}$$

$$\begin{array}{r} 2.0 \\ 4.3 \\ \hline 240.82 \end{array}$$

240.82

240.82

240.82

240.82

240.82

240.82

240.82

240.82

240.82

240.82

47-

$$\begin{array}{r} 6.0 \\ 5.5 \\ \hline 243.8 \end{array}$$

$$\begin{array}{r} 4.0 \\ 5.8 \\ \hline 243.5 \end{array}$$

$$\begin{array}{r} 3.0 \\ 5.4 \\ \hline 243.9 \end{array}$$

$$\begin{array}{r} 2.6 \\ 5.5 \\ \hline 243.8 \end{array}$$

$$\begin{array}{r} \text{top} \\ 2.7 \\ \hline 3.1 \\ \hline 246.2 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 2.2 \\ \hline 5.8 \\ \hline 243.5 \end{array}$$

$$\begin{array}{r} E \\ 1.8 \\ \hline 6.0 \\ \hline 243.3 \end{array}$$

$$\begin{array}{r} 11 \\ 5.7 \\ \hline 243.6 \end{array}$$

$$\begin{array}{r} E \\ 3 \\ \hline 5.8 \\ \hline 243.5 \end{array}$$

$$\begin{array}{r} @ \text{wall} \\ 0 \\ \hline 5.8 \\ \hline 243.5 \end{array}$$

$$\begin{array}{r} \text{top} \\ 4 \\ \hline 6.0 \\ \hline 243.3 \end{array}$$

$$\begin{array}{r} 5 \\ 3.6 \\ \hline 245.7 \end{array}$$

$$\begin{array}{r} 6 \\ 5.1 \\ \hline 244.2 \end{array}$$

$$\begin{array}{r} 20 \\ 3.9 \\ \hline 243.4 \end{array}$$

$$\begin{array}{r} 30 \\ 5.8 \\ \hline 243.5 \end{array}$$

$$\begin{array}{r} 40 \\ 5.9 \\ \hline 243.4 \end{array}$$

$$\begin{array}{r} 60 \\ 6.8 \\ \hline 242.5 \end{array}$$

@ Ho.

$$\begin{array}{r} 5.8.5 \\ 0.9 \\ \hline 248.4 \end{array}$$

$$\begin{array}{r} 4.0 \\ 1.7 \\ \hline 247.6 \end{array}$$

$$\begin{array}{r} 3.0 \\ 2.7 \\ \hline 246.6 \end{array}$$

$$\begin{array}{r} 2.0 \\ 4.9 \\ \hline 244.4 \end{array}$$

6 TW.

E

0

@ wall

top

4

10

30

40

$$\begin{array}{r} 13 \\ 4.7 \\ \hline 244.6 \end{array}$$

$$\begin{array}{r} 5 \\ 5.0 \\ \hline 244.3 \end{array}$$

$$\begin{array}{r} 0 \\ 6.0 \\ \hline 243.3 \end{array}$$

$$\begin{array}{r} 2 \\ 6.2 \\ \hline 243.1 \end{array}$$

$$\begin{array}{r} 3 \\ 4.6 \\ \hline 244.7 \end{array}$$

$$\begin{array}{r} 4 \\ 6.2 \\ \hline 243.1 \end{array}$$

$$\begin{array}{r} 10 \\ 7.0 \\ \hline 242.3 \end{array}$$

$$\begin{array}{r} 30 \\ 7.9 \\ \hline 241.4 \end{array}$$

$$\begin{array}{r} 40 \\ 8.1 \\ \hline 240.5 \end{array}$$

249.42

D.H.E.

47+50

L7 58.5 Sil Olsen's Ho. +0.17

148
1168

47+91 & Bit Maced Drive Lt. askew.

3.11 251.89 0.47 248.78
 $\bar{\pi}$

48- $\frac{60}{3.5}$ $\frac{40}{4.8}$ $\frac{30}{5.5}$ $\frac{22}{6.2}$
 2484 2471 2464 2457

48+ $\frac{60}{2.4}$ $\frac{40}{2.4}$ $\frac{37}{2.2}$ $\frac{33}{1.3}$ } @ wall $\frac{34}{4.5}$ $\frac{30}{4.5}$ $\frac{26}{4.9}$ $\frac{18}{4.9}$
 2495 2495 2497 2506 2474 2474 2470 2470
 4.87 253.65 248.78
 $\bar{\pi}$

49- $\frac{60}{5.1}$ $\frac{39}{4.5}$ $\frac{37.5}{1.4}$ } @ wall $\frac{36}{5.3}$ $\frac{32}{5.1}$ $\frac{30}{5.1}$ $\frac{28}{5.3}$ $\frac{21}{5.0}$
 2486 2492 2523 2484 2486 2486 2484 2487
 3.09 255.88 0.86 252.79
 $\bar{\pi}$

49+ $\frac{60}{8.3}$ $\frac{42}{5.6}$ $\frac{4.1}{2.6}$ } @ wall $\frac{40}{4.9}$ $\frac{35}{4.3}$ $\frac{31}{4.6}$ $\frac{30}{4.6}$ $\frac{24}{4.5}$
 2476 2503 2533 2510 2516 2513 2513 2514

50- $\frac{60}{6.6}$ $\frac{39}{3.0}$ $\frac{38}{1.0}$ } @ wall $\frac{37}{2.3}$ $\frac{31}{2.9}$ $\frac{30}{2.9}$ $\frac{24}{2.9}$ $\frac{12}{2.9}$
 2493 2529 2569 2536 2530 2530 2530 2530

6.41 260.08 2.21 253.67
 $\bar{\pi}$

50+ $\frac{60}{8.8}$ $\frac{40}{6.0}$ $\frac{37}{5.5}$ } @ wall $\frac{36}{5.3}$ $\frac{35}{5.4}$ $\frac{34}{5.8}$ $\frac{30}{7.7}$ $\frac{24}{7.7}$
 251.3 2541 2546 2568 2547 2543 2524 2524

51- $\frac{60}{9.5}$ $\frac{40}{6.9}$ $\frac{36}{6.4}$ } @ wall $\frac{35}{4.1}$ $\frac{34}{6.1}$ $\frac{32}{6.2}$ $\frac{30}{7.3}$ $\frac{27}{9.0}$
 2506 2532 2537 2560 2540 2539 2528 2511

149

$\frac{75}{0.1}$ $\frac{60}{0.8}$ $\frac{40}{2.3}$ $\frac{30}{3.0}$ $\frac{22}{3.7}$ $\frac{14}{3.8}$ $\frac{6}{4.2}$ $\frac{0}{5.2}$
 2492 2485 2470 2463 2456 2455 2451 2441
 T.P. Ring top granite post @ Ohlson (most rt)

$\frac{15}{6.2}$ $\frac{7}{6.6}$ $\frac{0}{7.5}$ } @ wall $\frac{1}{6.5}$ $\frac{2}{8.5}$ $\frac{10}{10.4}$ $\frac{30}{11.0}$ $\frac{40}{11.4}$ $\frac{60}{11.9}$
 2457 2453 2444 2454 2434 2415 2409 2405 2400
 $\frac{11}{5.2}$ $\frac{4}{6.4}$ $\frac{3}{5.7}$ } @ wall $\frac{1}{8.9}$ $\frac{0}{9.3}$ $\frac{5}{10.7}$ $\frac{20}{11.3}$ $\frac{30}{12.1}$ $\frac{40}{12.9}$ $\frac{60}{14.6}$
 2467 2455 2462 2430 2426 2412 2406 2398 2390 2373
 T.P. above DNE

$\frac{13}{5.3}$ $\frac{6}{6.1}$ $\frac{5}{4.5}$ } @ wall $\frac{4}{7.4}$ $\frac{0}{8.3}$ $\frac{10}{9.7}$ $\frac{20}{11.8}$ $\frac{30}{13.9}$ $\frac{40}{15.2}$ $\frac{60}{18.2}$
 2484 2476 2492 2463 2454 2440 2419 2398 2385 2355
 T.P. stone in street

$\frac{15}{4.7}$ $\frac{14}{5.7}$ $\frac{7}{3.4}$ $\frac{6}{3.0}$ } @ wall $\frac{0}{4.6}$ $\frac{0}{5.7}$ $\frac{10}{8.4}$ $\frac{30}{11.0}$ $\frac{30}{13.4}$ $\frac{40}{16.0}$ $\frac{60}{19.2}$
 2512 2522 2525 2529 2513 2502 2475 2449 2425 2399 2367

$\frac{15}{2.1}$ $\frac{9}{1.5}$ $\frac{8}{0.8}$ } @ wall $\frac{7}{2.1}$ $\frac{0}{2.9}$ $\frac{10}{4.1}$ $\frac{20}{5.7}$ $\frac{30}{8.1}$ $\frac{40}{10.6}$ $\frac{60}{15.1}$
 2538 2544 2551 2438 2530 2518 2502 2478 2453 2408

T.P. top of stk 50+07±

$\frac{18}{7.8}$ $\frac{15}{6.5}$ $\frac{12}{6.4}$ $\frac{10}{4.9}$ } @ wall $\frac{9}{6.1}$ $\frac{0}{6.0}$ $\frac{10}{5.6}$ $\frac{20}{7.0}$ $\frac{30}{9.0}$ $\frac{40}{12.0}$ $\frac{60}{15.8}$
 2523 2536 2537 2552 2540 2541 2545 2531 2503 2481 2443

$\frac{23}{7.2}$ $\frac{17}{9.3}$ $\frac{13}{7.4}$ $\frac{12}{6.4}$ } @ wall $\frac{10}{7.3}$ $\frac{0}{7.2}$ $\frac{10}{6.3}$ $\frac{20}{5.1}$ $\frac{30}{4.9}$ $\frac{40}{7.1}$ $\frac{60}{11.5}$
 2509 2508 2527 2537 2528 2529 2538 2550 2552 2530 2486

DNE

150
1168260.08
K

51+39 £ Dirt Drive Lt. skew.

4.28 254.73
K 9.63 250.45
K

51+

60	40	30	E	ΔTW
5.3	5.4	5.4	5.3	5.1
2494	2493	2493	2494	2496
449	254.94	✓	250.45	✓

100	75	60	40	30	E	ΔTW	E	10	0
10.6	10.4	10.8	10.8	10.4	10.3	10.4	10.8	11.0	
2495	2497	2493	2493	2497	2498	2497	2493	2491	

T.P. stone wall

52-

60	40	34	32	top	@ wall	E	ΔTW
6.6	7.2	6.7	5.2	3.1	3.0	2.8	2.5
2483	2477	2482	2497	2487	2489	2500	2496

E	10	0	top	@ cross wall	top	5	7	20	30	40	60
5.4	6.4	7.0	3.0	6.0	6.6	7.3	6.5	8.4			
2493	2483	2477	251.7	248.7	2481	2474	2482	2463			

T.P. above

52+

60	40	30	29	top	@ wall	E	ΔTW	E
5.2	5.5	5.3	3.3	2.8	2.4	1.8	1.2	
2497	2494	2496	2516	250.1	2500	2508	2499	

E	8	top	@ Ret.	5	0	10	20	30	40	60
5.4	5.2	4.9	7.4	8.6	8.9	9.5	9.7	9.8	9.8	
2495	2497	2500	2475	2463	2460	2454	2452	2451	2451	

check BM. chis. (251.94)

53+29 Rt. 86 541 257.35
K 251.94

BM above

53-

60	40	30	29	top	@ wall	E	ΔTW	E
5.6	5.7	5.5	3.6	2.8	2.4	2.2	1.5	9
251.8	251.7	2519	2538	2522	2524	2515	2514	2512

4	top	@ wall	1	0	10	20	30	40	60
5.9	4.6	6.4	6.5	7.3	7.6	7.7	7.8	8.0	
251.5	2528	251.0	2509	2501	2498	2497	2496	2494	

53+

60	40	30	20	top	@ wall	E	ΔTW	E
3.3	3.4	3.6	4.1	4.1	4.2			
254.1	2540	2538	2533	2533	2532			

1	top	@ wall	2	10	20	30	40	60
2.4	2.2	3.3	4.3	4.7	4.8	4.7	5.7	
2550	2552	2541	2531	2527	2526	2527	251.7	

T.P. Boulder

54-

60	40	30	25	top	@ wall	E	ΔTW
4.2	4.3	4.6	4.7	2.5	2.3	2.0	1.7
2583	2582	2579	2578	2600	2579	2575	2557

E	@ wall	top	1	2	10	20	30	40	60
6.7	5.4	3.8	6.2	7.4	7.6	8.1	8.4	8.1	
2556	2571	258.7	2563	2551	254.9	2544	2541	2544	

54+

60	40	30	23	top	@ wall	E	ΔTW
4.1	4.0	3.9	3.6	1.6	3.1	1.8	1.5
2584	2585	2586	2589	2609	2594	2591	2576

E	@ wall	top	2	4	10	20	30	40	60
5.0	3.8	1.2	4.7	5.8	7.5	8.1	8.7	9.1	
2575	2587	2613	2578	2567	2556	2544	253.8	2534	

DNE

152/68

262.49

153

55-

60	40	30	21	20	@ wall	E	2TW	E	@ wall	top	3	5	15	20
$\frac{60}{4.6}$	$\frac{40}{4.8}$	$\frac{30}{4.8}$	$\frac{21}{4.4}$	$\frac{20}{3.6}$	$\frac{19}{4.4}$	$\frac{15}{4.8}$	$\frac{8}{4.6}$	$\frac{1}{4.5}$	$\frac{0}{4.5}$	$\frac{2}{4.1}$	$\frac{3}{1.3}$	$\frac{5}{4.7}$	$\frac{15}{5.1}$	$\frac{20}{5.7}$
2579	2577	2577	2581	2589	2581	2577	2579	2580	2580	2584	261.2	2578	2574	2568

645

262.71

623

256.26

T.P. Ledge outcrop.

30

64

2561

40

72

2553

60

86

2539

55+

60	40	30	20	top	@ wall	2TW	E								
$\frac{60}{5.6}$	$\frac{40}{6.2}$	$\frac{30}{6.4}$	$\frac{20}{5.9}$	$\frac{19}{5.0}$	$\frac{18}{5.7}$	$\frac{13}{5.4}$	$\frac{6}{5.3}$	$\frac{0}{5.3}$	$\frac{1}{5.3}$	$\frac{4}{5.3}$	$\frac{6}{5.9}$	$\frac{20}{6.7}$	$\frac{30}{7.1}$	$\frac{40}{7.4}$	$\frac{60}{7.4}$
2571	2565	2563	2568	2577	2570	2573	2574	2574	2574	2574	2568	2560	2556	2553	2553

56-

60	40	30	20	19	top	@ wall	E	2TW	E	@ wall	top	8	12	30	40	60
$\frac{60}{5.0}$	$\frac{40}{5.5}$	$\frac{30}{6.0}$	$\frac{20}{5.9}$	$\frac{19}{3.8}$	$\frac{18}{5.4}$	$\frac{11}{5.7}$	$\frac{4}{5.6}$	$\frac{0}{5.7}$	$\frac{3}{5.8}$	$\frac{6}{5.3}$	$\frac{7}{3.9}$	$\frac{8}{6.6}$	$\frac{12}{7.1}$	$\frac{30}{7.7}$	$\frac{40}{7.5}$	$\frac{60}{7.3}$
2577	2572	2567	2568	2589	2573	2570	2571	2570	2569	2574	2588	2561	2556	2550	2552	2554

56+

60	40	30	17	16	top	@ wall	E	2TW	E	@ wall	top	11	15	30	40	60
$\frac{60}{5.2}$	$\frac{40}{4.7}$	$\frac{30}{5.0}$	$\frac{17}{5.3}$	$\frac{16}{3.9}$	$\frac{15}{5.3}$	$\frac{9}{4.1}$	$\frac{3}{6.0}$	$\frac{0}{6.0}$	$\frac{4}{6.2}$	$\frac{8}{5.6}$	$\frac{9}{4.6}$	$\frac{11}{6.9}$	$\frac{15}{7.6}$	$\frac{30}{8.2}$	$\frac{40}{8.9}$	$\frac{60}{8.9}$
2575	2580	2577	2574	2588	2574	2566	2567	2567	2565	2571	2581	2558	2551	2545	2538	2538

5.59

261.59

6.71

256.00

T.P. stone

57-

$\frac{60}{4.3}$	$\frac{40}{4.8}$	$\frac{30}{5.1}$	$\frac{16}{5.0}$	$\frac{15}{3.4}$	$\frac{14}{5.2}$	$\frac{9}{5.5}$	$\frac{2}{5.3}$	$\frac{0}{5.4}$	$\frac{5}{5.6}$	$\frac{7}{5.0}$	$\frac{9}{3.9}$	$\frac{11}{6.3}$	$\frac{20}{7.1}$	$\frac{30}{7.8}$	$\frac{40}{8.1}$	$\frac{60}{8.8}$
2573	2568	2565	2566	2582	2564	2561	2563	2562	2560	2566	2577	2553	2545	2538	2535	2528
		4.2	26042		25600		T.P. above									

4.42

260.42

256.00

T.P. above

57+

60	40	30	20	15	14	top	@ wall	E	2TW	E	@ wall	top	13	14	20	30	40	60
$\frac{60}{4.9}$	$\frac{40}{5.4}$	$\frac{30}{5.6}$	$\frac{20}{5.9}$	$\frac{15}{5.5}$	$\frac{14}{4.1}$	$\frac{13}{5.2}$	$\frac{9}{5.3}$	$\frac{0}{4.9}$	$\frac{7}{5.2}$	$\frac{12}{5.2}$	$\frac{13}{4.0}$	$\frac{14}{6.2}$	$\frac{20}{7.4}$	$\frac{30}{7.7}$	$\frac{40}{8.1}$	$\frac{60}{9.5}$		
2555	2550	2548	2545	2549	2563	2552	2551	2555	2552	2552	2564	2542	2530	2527	2523	2509		
		388		25288		25600		T.O. above										

3.88

259.88

256.00

T.P. above

58-

$\frac{60}{5.6}$	$\frac{40}{6.1}$	$\frac{30}{6.3}$	$\frac{20}{6.6}$	$\frac{15}{6.3}$	$\frac{14}{4.3}$	$\frac{13}{4.8}$	$\frac{8}{5.3}$	$\frac{0}{5.0}$	$\frac{7}{5.3}$	$\frac{14}{5.2}$	$\frac{15}{4.5}$	$\frac{16}{7.1}$	$\frac{20}{6.4}$	$\frac{30}{9.0}$	$\frac{40}{8.8}$	$\frac{60}{10.2}$
2543	2538	2536	2533	2538	2556	2551	2546	2549	2546	2547	2554	2528	2515	2509	2511	2497

58+

$\frac{60}{7.0}$	$\frac{40}{7.0}$	$\frac{30}{7.5}$	$\frac{20}{7.3}$	$\frac{15}{7.0}$	$\frac{14}{4.9}$	$\frac{13}{5.6}$	$\frac{7}{5.6}$	$\frac{0}{5.4}$	$\frac{8}{5.6}$	$\frac{14}{5.6}$	$\frac{15}{5.5}$	$\frac{16}{7.9}$	$\frac{20}{8.6}$	$\frac{30}{9.0}$	$\frac{40}{9.7}$	$\frac{60}{10.6}$
2529	2529	2524	2526	2529	2550	2543	2543	2545	2543	2543	2544	2520	2513	2509	2502	2493

4.96

259.37

5.47

254.41

T.P. in wall

DHE

59-	60	40	30	20	17	16	top	F	@wall	E	ΔTW	-	0	5	@wall	top	12	13	20	30	40	60
5.7	6.2	6.6	7.0	6.8	4.4	4.4	15	10	2	5.1	5.3	5.5	4.6	7.7	8.7	9.0	9.0	9.7				
253.7	2532	2528	2524	2526	2550	2538	2540	2544	2543	2541	2539	2548	251.7	250.7	250.4	250.4	2497					
		4.92			259.33																	

6.79 252.54 check B.M. chis D back Pole 46 (252.56)

7.08 259.64 252.56 BM above

59+				Bot.	top	@wall	E	ΔTW	E	@wall	top	Bot.					
60	40	30	23	22	{	21	15	8	1	0	7	8	9	14	30	40	60
6.2	6.7	7.1	7.2	4.8		5.7	5.6	5.3	5.4	5.4	5.8	5.0	7.4	8.9	9.2	9.4	10.1
253.4	2529	2525	2524	2548		2539	2540	2543	2542	2542	2538	2546	2522	250.7	250.4	250.2	2495

60-	60	40	30	29	28	22	ΔTW	E	1	top	Bot	10	20	30	40	60
6.6	7.4	7.5	5.7	5.5	5.6	5.3	15	8	5.8	0	1	8.2	8.9	9.4	9.5	9.8
2530	2522	2521	2539	2541	2540	2543	2541	2538	2534	2514	250.7	250.2	250.1	2498	2498	

60+14 Rt. 22 B.M. chis D 7.40 259.96 252.56

60+	60	44	43	42	36	30	27	19	14	top	@wall	10	20	30	40	60
7.8	7.8	5.1	5.1	5.5	5.4	5.3	5.7	6.6	5.6	8.4	8.9	9.3	9.6	9.9	10.2	10.7
2522	2522	2549	2549	2545	2546	2547	2543	2534	2544	251.6	251.1	250.7	250.4	250.1	249.8	2493
		4.77		260.42	4.31	255.65										

T.P. stone in st.

61-	70	Bot	top @ wall	E	2 W. E	top	@ wall									
	59	59	58	52	44	36	30	28	27	10	2	10	30	30	40	60
8.4	8.2	5.4	5.3	5.1	5.6	5.8	5.9	8.6	9.7	19.8	10.0	10.4	10.4	10.9	11.4	
2520	2522	2550	2551	2553	2548	2546	2545	251.8	250.7	250.6	250.4	250.0	250.0	2495	2490	
	6.06	261.71	255.65				T. P.	2600								

T.P. above

61+23 L+70 Flow 2-12" Conc. Pipe 10.64
Top Stone Header 7.2
61+27 L+38 Flow 2-12" Conc. Pipe 10.87
Top Stone Header 7.8

251.07
2545
250.84
2539

156/168

1.75 268.79[✓] 337 267.04[✓]

261.71 ✓
A

157

T.P. Boulder.

